Estimation of rainfall using METEOSAT TIR data for the Naivasha catchment

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By

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ABSTRACT

Areal rainfall computed by kriging from point data measured with the available rain gauge network over the Naivasha catchment were used to calibrate a satellite rainfall algorithm using TIR METEOSAT data, through TAMSAT method approach.

The TAMSAT technique uses infrared images and depends on the assumption that convective clouds are the main source of rain.

Cold Cloud Duration at different thresholds and gauge data from 1994 to 1998 were compared in this study, it was shown that CCD 30 is an optimum threshold which shows the highest level of agreement with the gauge data in this region.

The correlation between precipitation ground measurement and convective clouds derived from METEOSAT TIR data were computed for daily and decadal scales, the relation between precipitation and cold cloud field notably improved in decadal scale.

Some of the statistical techniques have been utilized for the determination of the best relationship between rainfall and satellite data.

The response of the runoff at the outlet of Malewa catchment to the event CCD and the kriged rainfall has been discussed briefly for two short periods during 1997 and 1998.

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List abbreviations

| ADMIT | Agricultural Drought Monitoring Interactive Technique |
|----------|---|
| BIAS | Bristol Inter Active Scheme |
| CCD 30 | Cold Cloud Duration at a temperature of -30°C |
| EUMETSAT | European METorological SATellite |
| FAO | Food and Agriculture Organisation (UN) |
| GOES | Geostationary Operational Environmental Satellites |
| GPI | Goes Precipitation Index |
| KR | Kriged rainfall |
| METEOSAT | METEOrological SATellite |
| NOAA | National Oceanic and Atmospheric Administration |
| NASA | National Aeronautics and Space Administration |
| PERMIT | Polar Orbiter Effective Rainfall Monitoring Interactive Technique |
| PR | TRMM Precipitation Radar |
| TAMSAT | Tropical Applications of Meteorology using SATellite |
| TMI | TRMM Microwave Imager |
| TIR | Thermal Infra-Red radiation |
| TRMM | Tropical Rainfall Measuring Mission |
| TSDIS | TRMM Data and Information System |
| VIRS | Visible and Infra-red Radiometer System |
| VIS | VISibleradiation |

CHAPTER 1

1. INTRODUCTION

1.1 Problem Definition

Because of the need for better management of the scarce water resource, we need better data on water budgets. Rainfall is of course the first major component of the water budget.

Rainfall occurs over time periods from minutes to days and weeks and over areas of a few kilometers to hundreds of kilometers. Hence to measure space/time averaged rainfall a dense net work of rain gauge is needed. However, the distribution density of rain gauges is often too low to cope with the extreme spatial and temporal variations of rainfall, especially in arid and semi-arid regions and through much of the tropics (Barrett and Martin, 1981).

See Fig 3.5, the spatial variation of decadal rainfall over the Naivasha catchment, the correlation between distance and rainfall is less than 50% after 5 km. (data obtained from Kenya Meteorology office). Further, rain gauge data are often inaccurate and /or untimely.

It is well known that rainfall observations from relatively isolated rain gauges are rarely representative of rainfall over wider areas. (The World Meteorological Organization, 1974) recommended the minimum gauge density of precipitation networks in various geographical regions. For temperate, Mediterranean, and tropical mountainous region $100 - 250 \text{km}^2$ per gauge is recommended (Ward, 1974). The over all rain gauge density in Naivasha catchment is 290 km² per gauge, but large parts have a much lower density.

Understanding rainfall in the tropics is important because of its influence on large-scale atmospheric dynamics and its relevance to human life (Barrett and Martin, 1981).

Real time rainfall data is needed to assess and monitor the water budget, to signal short falls in crop growth, and to provide warning for floods. In Africa the scarcity of ground based data means that the only feasible approach to real-time area estimation is the use of satellite imagery. Thus, satellite remote sensing could play a significant role in improving knowledge of rainfall distribution and quantification in areas like Naivasha.

Therefore this thesis is devoted to find a relation between METEOSAT thermal infrared imagery (CCD) based on temperature thresholding (to identify potential rain clouds) and actual rainfall over the Naivasha catchment.

1

1.2 Objective

The main objective of the research is

• To work out areal rainfall estimates using *TAMSAT* method as developed from the *GOES* precipitation index *(GPI)* which is widely used for climatological studies of global precipitation, for the Naivasha area.

• To analyze deviation of predicted and observed rainfall

• To study whether the result yields improved rainfall-runoff relationships in the Naivasha catchment.

1.3 Research Methodology

The Cold Cloud Duration (CCD) daily image taken by satellite over the whole African continent is used as an input data (supplied by TAMSAT group, University of Reading, Department of Meteorology), the following is based on their method.

First the entire area is divided in to grid square map (latitude, longitude), then the satellite images overlay with grid square map, the grid squares are identified as "gauge cells" (those containing the gauge stations) and "satellite cells" (those lacking stations)

Then a contingency table, which contains both satellite derived (CCD) and conventional data will be prepared to select an appropriate cold cloud top temperature threshold, to determine whether or not the cloud produced rain and the rainfall estimated from the period during which the cloud remained over a site, using the above "gauge cell".

By using Kriging the areal rainfall based on the rain gauge data is estimated for the corresponding period of CCD images.

After merging of CCD and gauge data, evaluation of the result will be analyzed by examining events, which deviate much from the expectations.

Regression analysis is used to define the relation between CCD and the kriged rainfall; the result is used to make a prediction of rainfall for the full catchment.

River gauging records are utilized to verify how well the discharge responses to the event CCD estimated rainfall and kriged rainfall.

1.4 Study area

The Lake Naivasha basin, stretching over an area of 3200 km², lies in the East African Rift Valley, about 100 km Northwest of Nairobi. Its geographical coordinates are $0^{0}00'$ to $1^{0}00'$ S and 36^{0} 00' to 36^{0} 45' E. Administratively, it is situated in the Naivasha division, Nakuru district, Rift Valley province of Kenya.

It receives an average of 1000 mm of rain per year and it exhibits smooth to very high relief. The area has two rainy season short rainy season (mid October to mid December) and long rainy season (March to June), During the rain season the major rain bearing system is the squall line: a convective system and moving from east to west.

The cumulonimbus clouds have a low cloud base and very high cloud tops. For this reason, on the METEOSAT image these clouds appear very cold in the thermal infrared and very bright in the visible domain. This offers a possibility to discriminate them from other clouds. (Ears and Rosema, 1988)

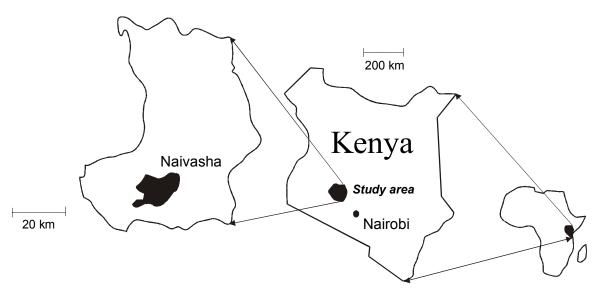


Figure 1.1 The study area in international, national, and regional contexts.

1.4.1 Meteosat data

Windowing of Study Area:

This is a method to define (windowing out) the above area from the whole African continent CCD image in METEOSAT projection. The Latitude-Longitude co-ordinate of the catchment is defined using the Atlas GIS. These co-ordinates convert to METEOSAT co-ordinates using the program LL2METXY (Rogerio, 1996).

Each degree Latitude is about 20 METEOSAT pixels, and the rectangular area covering entire Kenya is 200*200 METEOSAT pixels.

Windowing by convention and to give some margin for further trimming, following reprojection, a square region is defined in METEOSAT coordinates of 256x256 pixels.

This window is extracted from the original whole continent imagery and then re-projected to Latitude-Longitude co-ordinates to derive the original region.

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Hence the "Real-time window rectified daily CCD image", data which is based on half hour image is utilized for this study (1994 -1998).

1.4.2 Rain gauge network description

The network stations inside and around the catchment are composed of more than 200 manual recording raingauges. 11 raingauge stations within the catchment and an additional 19 stations in the area around the catchment with daily rainfall data for the period 1994 to 1998 are available, see Fig 1.3, out of 32101 available data 3647 data are missed.

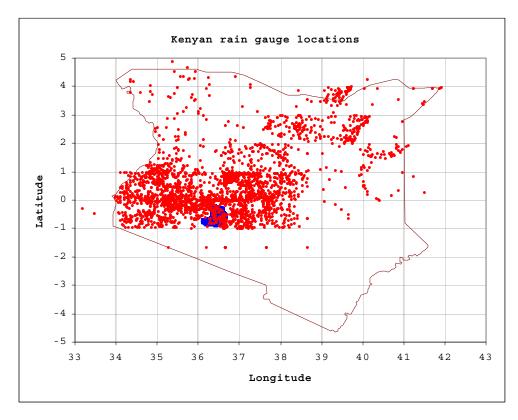


Figure 1.2 Map of Kenya with Naivasha catchment outline and rain gauge locations (source: Kenya meteorology department).

4

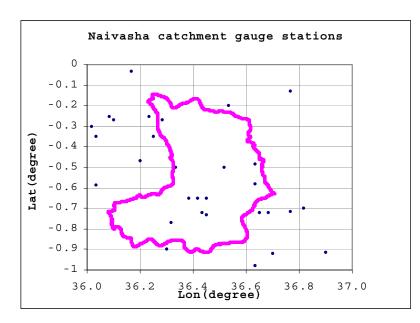


Figure 1. 3 Map showing Naivasha catchment and rainfall gauge stations which have recorded values for the year 1994 to 1998.

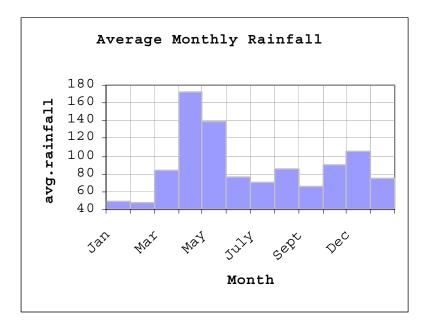


Figure 1.4 Graph, showing the average monthly rainfall pattern for the Naivasha catchment using the above 30 stations (1994 to 1998).

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CHAPTER 2

2. REVIEW OF TECHNIQUES IN QUANTITATIVE RAINFALL ESTIMATION

2.1 Measurement of rain with standard rain gauges

Even if the measurement of rainfall by rain gauges is fraught with some problems, that relatively simple instrumentation will long continue to provide the data against which rainfall assessments by other means must be adjusted.

The advantage of using rain gauges to monitor rainfall is (Grimes, Bonifacio and Loftie, 1998).

• *Comparability:* rainfall amounts can be compared through out a region or over a period of time if standardized gauges is used. Correction factors can be used to take account of differences in design.

• *Simplicity:* rain gauges are easily manufactured from local materials and do not require specialized maintenance. Observers can easily be trained.

The disadvantage using rain gauges are (Grimes, Bonifacio and Loftie,1998).

• *Point measurements:* rain gauges measure rainfall at a point but most often the information required is the rainfall average over a large area.

• *Distribution of gauges:* because gauges usually need to be read at once per day, gauge sites are often dictated by ease of access. This means that there are few gauges in uninhabited areas. Thus the distribution may not be representative of the area as a whole.

• *Time delay:* rain gauges are typically read at 6 AM to give the previous days rain. Data are rarely available in a central location on the same day and weeks or even months may elapse before sufficient data are assembled to give a meaningful overview.

Of the disadvantages, the first mentioned is the most significant. Particularly in the tropics, rainfall is often localized and a single gauge may only be representative of a very small area in its immediate vicinity, on a particular day.

As stated in (Barrett and Martin, 1981), (Woodley et al., 1974) found relatively small differences 5 to 10% in the measurements of heavy convective rainfall by pairs of co-located, unshielded rain gauges. (Rodda, 1971) stated similarly discouraging findings: catch deficiencies for rain collected in standard gauges were found to vary from 3% to 30% for annual totals and over a wider range for individual storms.

2.2 Areal rainfall estimation from Point data

The accuracy of areal rainfall estimation is depends on the spatial variability of precipitation; thus more gauges would be required in those area where rainfall is highly variable, Naivasha is of course one of the area where the rain fall is highly variable with space and time.

Many interpolation schemes have been proposed in the literature for the estimation of areal rainfall. The most familiar and simple scheme is the well-known Thissen polygons and the isohyetal methods, whereby the isohyets are often based on simple linear interpolation.

The statistical methods first require an examination of the spatial correlation structure of the data set, such as the analysis of the semi-variogram for the kriging method. This method is described in chapter three in more detail, since it is applied in this study.

The general form of the equation for interpolation at a point is:

Where: $\hat{Z}o$ is the estimated value of the process at any point with coordinates x_0, y_0 ;

- W_i the weight of the sampling point i
- Z_i the observed value of the attribute (or process) at a point i with coordinates x_i, y_i
- n the number of sampling points considered, i = 1,2,n.

The various interpolation technique differ only in evaluating the weight W.

Interpolation uses the principle that for the estimation of unknown values, the known values in the locality, surrounding or neighborhood is more relevance than those further away and weights may be given to the surrounding points.

Generally, a fairly large number of reference points (stations) are required, which restricts the application of the method. Even with an adequate density of the gauge network, the analysis of the spatial correlation structure may take so much time that one would be reluctant to use a stochastic (statistical) method when many rainfall pattern have to analyzed, for example for Studying daily rainfall patterns and runoff (Meijerink, de Brouwer, Mannaerts and Valenzuela, 1994).

2.3 Areal rainfall estimation using Satellite Remote Sensed data

(Griffth et al., 1978) recognized the transient evolution and extent of cloud-top temperature as a tool to infer convective activity. (Dugdale and Milford, 1986) developed the concept of cold cloud duration (CCD), using the thermal channel of Meteosat, to generate time series of cloud temperature for tropical altitudes, where most rainfall comes from large convective storms. They suggested that the duration above a threshold temperature value is representative of the amount of rain that is generated. Although there is an essential amount of empiricism included in this methodology, it helps to interpret rainfall intensities at unsampled locations between gauges in a network of rain gauges. As stated in (Bastiaanssen, 1998).

2.3.1 Satellite Remote Sensing Systems

It has become fashionable and convenient to differentiate between two groups of earth observation satellites, namely "Earth Resource" and "Environmental" satellites. In more general terms, the differences between the two groups arise from design capabilities for the frequency, and spatial resolution on the ground, of the data they provide. These capabilities are inversely related to each other largely because of data-flow constraints (Barrett and Martin, 1981). Since Earth Resource satellites provide a low temporal resolution (low imaging frequency) they only provide indirect rainfall through vegetation response (Meijerink, deBrouwer, Mannaerts and Valenzuela, 1994).

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Environmental satellites have commonly occupied two types of orbits, and may be grouped in (Barrett and Martin, 1981).

(A) Polar-orbiting, and

(B) Geostationary satellite families

Polar-orbiting Satellites

The satellites occupy relatively low-level orbits (usually between 500-1500 km above the surface of the earth), crossing the equator at high angles so that each orbit takes such a satellite close to the north and South Pole. These satellites are usually sun-synchronous, i.e. their orbits are so organized that, as the earth rotates on its polar axis, within the orbital ellipses, each new orbit results in the presentation of a new strip of the global target to the satellite in such away that the relationship between earth surface and sun angle is kept relatively constant.

The speed of the satellite is determined by its height above the earth. United States NOAA (National Oceanic and Atmospheric Administration) satellites, which are widely used for vegetation monitoring, orbit at a height of around 800km. This means they complete an orbit roughly every 90 minutes. The NOAA AVHRR (Advanced Very High-Resolution Radiometer) sensor scans the entire Earth's surface in about 12 hours. In this way most points on the Earth are viewed at least twice per day. Because of their low orbits, polar orbiters can give relatively high spatial resolution images.

Examples of polar orbiting satellite include NOAA, TIROS, ESSA, Molniya and Meteor (Russian), DMSP.

Geosynchronous satellites

The satellites are placed in to orbit at approximately 36000km in the plane of the equator, and advance in the same direction as the rotation of the Earth. This type of orbit is geosynchronous, the satellite keeping pace with the rotation of the earth on its polar axis, and geostationary in that it ensures that any satellite occupying it appears to be fixed or stationary above a given point on the surface. Such a satellite is able to record the same geographic field of view very frequently through the diurnal cycle, commonly at interval of 30 minutes.

Thus a geostationary satellite sees the same view of the full Earth disc all the time. Because a geosynchronous satellite has the same view of the Earth at all times; it is possible to build up a more detailed picture of how the scene is changing over time with in the field of view.

METEOSAT produces imagery every 30 minutes giving a total of 48 images per day. These factors are very important in estimating tropical rainfall. In contrast, a polar orbiting satellite, which may pass over the same spot at the same time only once or twice per day, will obtain a very biased view of the strong daily cycle of rainfall in the tropics.

Most convective storms build up in the late afternoon and evening so an overpass in the afternoon will exaggerate the rain, while an overpass in the morning will tend to underestimate it. For this reason, a geostationary satellite is much more useful than polar orbiters particularly when estimating rainfall on short time scales.

Examples include Applications Technology Satellite (ATS); The American Geostationary Operational Environmental Satellites (GOES-1, 2); GOES-10, an American satellite located over the Indian Ocean and controlled by ESA-European Space Agency satellite; METEOSAT (over west Africa controlled by ESA). The METOSAT satellite is positioned above 0° latitude, 0° longitude off the coast of West Africa. It is ideally positioned for looking at Africa); and a Japanese satellite, GMS-1, located over Borneo.

In this study METEOSAT is used to produce the image.

2.3.2 Satellite sensors and The Electromagnetic Spectrum

All sensor measure radiation in particular range of the electromagnetic spectrum. The electromagnetic spectrum is the term used to describe a whole family of types of radiation, which consist of electromagnetic wave motions.

Electromagnetic sensors and limitations

Sensors, which are sensitive to different wavelength bands in the electromagnetic spectrum, give us different information about the earth and its atmosphere. The wavelengths in common uses, which are relevant to rainfall estimation, are summarized below (Grimes, Bonifacio and Loftie, 1998).

(A) Visible sensor $(0.4 - 0.7 \mu m)$

A sensor in the visible region of the spectrum measures reflected sunlight, of clouds and earth surface.

Thicker clouds are more opaque, i.e. less sunlight passes through them than through thin clouds and more light is reflected back into space. This means that, seen from below, the base of the cloud is very dark, but seen from the satellite's point of view, the reflected light makes the cloud appear very bright. Therefore, it is supposed that as cloud thickness increases precipitation is more probable and its intensity is likely to be greater. Thinner clouds (which may be either at a low altitude or a high altitude) allow through more light and so reflect less. Therefore they appear less bright to the visible sensor on the satellite.

(B) Thermal Infra-Red (TIR) sensor $(10.5 - 12.5 \ \mu m)$

The temperature of the atmosphere decreases with height in a regular way throughout the troposphere (the bottom 10-15 km of the atmosphere) depending on weather conditions and the amount of the moisture present.

The emission of infrared radiation is less at lower temperature and greater at higher temperatures. The infrared sensor therefore acts as a remote thermometer, which can estimate the temperature of the cloud tops. *Cirrus* is also identified as very cold and lower, inactive cumulus show up at higher temperature of between 0° C to -20° C.

The infrared sensor can identify storm clouds by their low temperature although they may be confused with cirrus.

(C) Microwave sensor (5000 - 300000µm)

C.1. Passive sensor:

At wavelength of about 1.5 cm (15000 μ m), rainy areas show up very well over the oceans as bright against a dark background. Over the land, however, the background emission from the surface is very variable. The wetness of the surface as well as its roughness and the kind of vegetation all cause variations in the emitted radiation. Making quantitative estimates of rainfall against this continually changing background is a difficult task.

A further problem is that, because the micro wavelengths are so long, the energy available is quite small compared to the above wavelengths. Thus, the fields of view must be large to detect enough energy to record a signal; consequently, the spatial resolution in the microwave band is much coarser than in the other wavebands mentioned above. Hence, microwave sensor on a geostationary satellite would give images with a pixel size of several kilometers, which is far too coarse a scale for rainfall estimation.

C.2. Active sensor

TRMM sensor package:

The TRMM (Tropical Rainfall Measuring Mission) is designed to measure tropical rainfall from a low-inclination orbit using a suite of sensors, including the first spaceborn application of the precipitation radar. It covers the tropics between 35°N and 35°S. The primary rainfall instruments on TRMM are the precipitation radar (PR), the TRMM Microwave Imager (TMI) and the visible and Infrared Radiometer system (VIRS) (Kidd, 1998).

| | TMI | PR | VIRS |
|------------|---|--|---|
| Advantage | • Quantitative measure of rain wide swath | Quantitative measure of rain Better spatial resolution Rain type vertical profile of rain Can provide layer thickness works well over land | Best spatial resolution distinguish between convective and stratiform precipitation Transfer standard to geosynchronous to polar orbital |
| Limitation | Less quantitative over land for low rainfall Moderate spatial resolution | Narrow swath widthLargely untested in space | Less quantitative measure Obscuration by cirrus shields |

Table 2.1 TRMM sensors complementarity (Meneghini and Kozu, 1990)

Many algorithms exist for calculating rainfall from infrared or visible images from geostationary satellites.

The approach in this thesis is the TAMSAT method for rainfall estimation in Africa, which only uses information from the infrared sensor on the METEOSAT satellite.

The reason for this is according to (Grimes, Bonifacio and Loftie, 1998):

• In most of Africa a significant fraction of rain falls at night. The visible sensor has no use during the night.

• Calculations based on a single sensor have the great merit of simplicity, which is important for automatic operational procedures. Marginally better results might be achievable by including visible imagery for daytime storms, but this would be at the expense of a more complicated algorithm, which is more difficult to automate.

• It is difficult to verify small improvements that might be expected from the inclusion of visible images because of the sparseness of rain gauges in Africa.

2.3.3 General approach in rainfall estimation

The approaches discussed here pertain to making quantitative estimates of rainfall by using satellites visible and infrared techniques.

Visible and infrared techniques

There are three dominant approaches: the cloud indexing approach, the thresholding approach, and the life-history approach (Quanwei, 1996).

1. Cloud-indexing methods:

It is time independent, and it identifies different types of rain clouds and estimates the rainfall from the number and the duration of clouds of their area.

The techniques rely on visible and infrared data to characterize a cloud type or temperature, which is then related to rainfall via empirical relationships. Different methods have been used to calibrate the indices to give rainfall estimates.

The Earthsat method, (Moses and Barrett., 1986) is an operational rainfall estimation scheme that has been developed to provide input to crop yield models and commodity forecasting systems. The Earthsat method uses a regression approach to estimate 6-hour precipitation from cloud temperature and empirical information for the major crop-growing regions of the world.

The manual Bristol method uses an empirical relationship between satellite-determined cloud indices, climatic indices dependent on the mean monthly rainfall, and 12-hour rainfall totals. The Bristol method has been further developed into an interactive method known as BIAS (Bristol/NOAA Interactive System) originally for the USDA agRISTARS program (Schultz and Barrett, 1989). BIAS uses the following relationship:

 $R = f (C_t, C_a, C_d, C_c, S_w)$ (2.2)

Where: **R** is the 6-12 or 24-hour rainfall, C_t is a rain cloud type, C_a is the fraction of raincloud-type area and C_d is the duration. The product of C_t , C_a and C_d is the cloud index, which is translated into rainfall estimates through the regression equations. Each pixel is assigned a climate category, C_c , in order to select the proper cloud index/rainfall regression equation to be used in the absence of surface measurements of rainfall. However, if the surface measurements are available, the synoptic weather term, S_w , may be used to provide more accurate results.

2. Thresholding methods:

Consider that all clouds with low upper-surface temperature and clouds often brighter than others are likely to be rain clouds. So, there exist two types of thresholding methods, one is based on cloud top brightness, and the other is based on cloud top temperatures.

The cloud brightness techniques: depend on the assumption that precipitating clouds are often brighter than others, so that automatic brightness thresholding can be used to map rainfall from satellite visible imagery, and that calibration of rainfall amounts can be achieved using rain gauge and/or radar observations.

The cloud temperature technique: is based on temperature thresholding of thermal infrared imagery analyzed by computer to identify potential rain clouds and considers that all clouds with low upper-surface temperatures are likely to be rain clouds.

Examples of this technique include the TAMSAT and the PERMIT methods.

• The TAMSAT approach:

The use of Cold Cloud Duration (CCD) as a surrogate for rainfall has its roots in the work of (Arkin and Meissner, 1987) who showed that rainfall in the tropical could be related to the fractional coverage of cloud with satellite-measured temperature below 235K (-38°C). This work has lead to the development of the GOES precipitation index (GPI) which is widely used for climatological studies of global precipitation.

$GPI = 3f\Delta t$(2.3)

Where: **GPI** is the mean rain rate estimate in an area, **f** is the fraction of the area covered with clouds colder than 235K and Δt is time in hours between successive images.

The **GPI** works well for rainfall over the ocean but generally tends to underestimate rainfall over land. This is unsurprising as no allowance is made for the effect of land surface characteristics such as topography.

The TAMSAT method will be described in more detail in the next chapter since it is applied in this study

• PERMIT:

The PERMIT method (Polar-orbiter Effective Rainfall Monitoring Integrative Technique) uses a TIR threshold for the discrimination of rain cloud areas. The main objective of this discrimination is to identify rainy days, not cold cloud duration. The relation between rainy days and rainfall is therefore not based on regression analysis using meteorological data, but instead on climatological data of mean rain-per-rainy-day (Snijders, 1991).

The relationship used in PERMIT can be expressed as:

$$R = f (C_T, C_d, M_c, S_w)(2.4)$$

Where: **R** is the estimated rainfall for periods of 10 days or longer, C_T is the cloud top temperature, C_d is the number of satellite observed rain cloud days, M_c is an empirical term that describes the combined climate/terrain effect and S_w is a synoptic weight related to surface measurements.

3. Life-history methods

Some life-cycle methods are designed to provide rain estimates from any type of convectional clouds by taking into objective consideration of the growth or dissipation of individual clouds with time. This approach implicitly recognizes that convective clouds exhibit different rainfall intensities during their growth and dissipation cycle.

The *Woodley-Griffith techniques* were developed initially to predict rainfall over south Florida as part of the Florida area cumulus experiment. (Griffith et al., 1978). This method uses an empirically derived relationship between calibrated ground-based radar echoes and geostationary satellite imagery of cloud areas. A time-cycle relationship between the radar echo area and the cloud area is developed for discrete time intervals during the lifetime of the cloud.

$$\mathbf{R}_{\mathbf{v}} = \mathbf{I}\mathbf{A}_{\mathbf{e}} \sum q_i b_i \Delta t \dots (2.5)$$

Where: $\mathbf{R}_{\mathbf{v}}$ is the rain volume in mm, I is the rain rate in m³ km⁻²h⁻¹, $\mathbf{A}_{\mathbf{e}}$ is the inferred radar echo in square kilometers, I is the temperature index, q is the fraction of pixels at each threshold within the cloud, b is a temperature-dependent weighting factor and Δt is the time interval between successive satellite images.

| Model | Analysis Type | Parameters/equation | Characteristics |
|---------------|----------------|------------------------------|--|
| | | • | |
| Earthsat | Cloud indexing | R=[a+b(C*V*0 .6)]M | Empirical. Uses a regression approach to estimate 6h rainfall from cloud temp. and empirical information. |
| BIAS | Cloud indexing | R= f (Ct, Ca, Cd ,Cc, Sw) | Design for unsual events, 12h rainfall total. Uses satellite determined cloud indices dependent on mean monthly rainfall and 12h rainfall totals. (fully interactive) |
| GPI | Cloud indexing | R = f(CT) | Give monthly rainfall estimates for 2.50 squares. It is a global hyd. model.Temperature statistics of cloud top required. |
| NESS | Cloud indexing | R=(K1A1+K2A2+K3A3)/A0 | gives 24h period av. rain across the area |
| PERMIT | Threshhold | R=f(CT,Cd,Mc,Sw) | Estimates rainfall for, >=10days. Based on T thresholding of thermal IR imagery for potential rain cloud. |
| ADMIT/ (FAO) | Threshhold | Rv=f(CB,CT,Cd,Mc,Sw). | An extension of PERMIT .Uses daytime visible and IR images to establish rain/no- rain threshold. |
| TAMSAT Method | Threshhold | R=f(C _T) | IR based cloud-top temperature technique. Uses hourly imagery, to displays regional regressions to translate CCD into rainfall estimates for time frames of 1,5,10 & 30 days |
| CST | Threshold | $R=f(C_T,T_S)$ | Estimates both convective and stratiform rainfall |

Table 2.2 Summary of Several Visible/Infrared Satellite Rainfall monitoring Techniques. (Schultz and Barrett, 1989) as discussed in (Adegu, 1999).

f-function, a, b-rainfall coefficients, R-rainrate, Sw-synoptic weather term

C -local cloud brightness category, Ct-rain cloud type, CT-cloud top temp.

V-vertical motion class, Cd-sat. obs. rain cloud days, M-weighting factor

Ce-climate category, CB -cloud brightness

A0-total area, A1, A2 ... areas covered by the 3 most rain-producing clouds(cumulonimbus, cumulocongestus, nimbostratus), K1,K2 ..- empirical coefficients.

CHAPTER 3

3. APPLICATION OF THE TAMSAT METHOD FOR RAINFALL ESTIMATION.

3.1 General

The TAMSAT rainfall estimation is one of a number of approaches developed from the GPI application in Africa (Milford and Dugdale, 1990). It was devised in response to the needs of some African countries for rapid identification of regions with rainfall deficits and likely shortfall in crop yields. The method uses cloud-top temperature calculated from METEOSAT TIR radiance and utilizes more frequent images (every half an hour), needed to monitor the highly variable rainfall of a region.

The basic assumptions inherent in the TAMSAT rainfall estimation procedure are, (Grimes, Bonifacio and Loftie, 1998):

- 1. Rainfall comes mainly from convective storm clouds.
- 2. These clouds only rain when their tops have reached a certain minimum height (the height threshold).
- 3. The cloud top height can be identified by its temperature on the thermal infrared (TIR) image. This temperature is referred to as threshold temperature T_t.
- 4. At a given location, the quantity of rainfall can be calculated from the length of time the cloud top has been above the height threshold (or colder than the corresponding temperature threshold T_t). This length of time is the *Cold Cloud Duration or CCD*.

A further assumption is that the relationship between *rainfall quantity* and *CCD* is *linear* provided there is adequate averaging of the data either in space or in time. Thus we can write

 $R = a_0 + a_1 \times CCD$for CCD > 0

Where: **R** is rainfall, **CCD** is Cold Cloud Duration, a_0,a_1 are respectively the offset and the slope (or coefficient) of the straight line graph represented by equation 3.1. a_0,a_1 and T_t depend on local climate conditions and hence vary both in space and time.

3.2 Overview of rainfall estimation procedure

The steps involved in the production of the rainfall estimates are as follows: (Grimes, Bonifacio and Loftie, 1998):

- Generation of **CCD** images at a number of temperature thresholds.
- Determination of the optimum threshold T_t for the calibration zone
- Determination of optimum calibration parameters \mathbf{a}_0 and \mathbf{a}_1 for the zone.

- Calculation of rainfall estimates.
- Evaluation (geostatistical approach) of rainfall estimates.

3.2.1 Generation of CCD images

Thermal Infrared Red (TIR) images

TIR images are transmitted by METEOSAT every 30 minutes. It is from these that CCD images are derived. The row data are in the form of radiometer counts, which are related to the radiance of the observed surface by the equation

 $L = \alpha (C - C_0)$(3.2)

Where: L is radiance (Wm⁻²s⁻¹), C is the radiometer count, α and C₀ are calibration coefficients, which depend on the radiometer. C₀ is known as the space count. To allow the calibration drift, the values of α and C₀ are adjusted with a calibration system on the satellite and transmitted with the imagery twice per day (usually 8.a.m and 8.p.m). The radiance can be converted to temperatures by a look-up table or alternatively the following relationship between radiance and temperature T (k) can be applied.

$$L = \exp{A+B/T}$$
.....(3.3)

The value of A and B depend on the radiometer used. Values for Meteosat 2 to 7 are given in table 3.1 below.

Table 3.1 Values of coefficients A and B in the radiance-temperature relationship provided by EUMETSAT.

| Metosat | M2 | M3 | M4 | M5 | M6 | M7-1 | M7-2 |
|---------|----------|----------|----------|----------|----------|----------|----------|
| А | 6.1401 | 6.1694 | 6.7300 | 6.7348 | 6.7615 | 6.9676 | 6.9618 |
| В | -1267.00 | -1262.70 | -1272.20 | -1272.20 | -1267.20 | -1255.61 | -1255.55 |

Radiometer counts C in terms of radiance is obtained by rearranging equation (3.2)

$$C = (C_0 - L/\alpha)$$
.....(3.4)

An equation relating temperature to digital counts or vice versa for any date and Meteosat satellite can be obtained by combining (3.3) and (3.4)

| C = | $C_0 + 1/\alpha (exp(A+B/T)(A+B/T))$ | 3. | . 5) |) |
|-----|--------------------------------------|----|------|---|
|-----|--------------------------------------|----|------|---|

or

 $T = B/(-A+ln[\alpha(C-CO)])$(3.6)

Thus, from a table of **T** and **C**, one can know the **T** corresponding to any count.

Estimation of rainfall using METEOSAT TIR data for the Naivasha catchment (Kenya)

Derivation of CCD (CCU) images

To begin generation of CCD images, a temperature threshold is selected which is converted to a radiometer count via the calibration relationship. After that the procedure is (Grimes, Bonifacio and Loftie, 1998):

The threshold \mathbf{T}_t is applied to each individual TIR image. This means that the pixels within temperature value below a threshold \mathbf{T}_t (assumed 'rainy') is assigned value 1 and those with T above \mathbf{T}_t (assumed 'dry') are assigned 0. This forms a Boolean image (as a secondary image).

The thresholding is repeated for 48 half hourly TIR images to obtain 48 Boolean images. The 48 Boolean images are added up-the result is a daily CCD image. Each pixel value is the number of hours that the pixel was under rain-bearing cloud.

To produce a decadal CCD image, the daily CCU images in slots are totaled over the appropriate number of days and divided by 2 to give the cold cloud duration in hours for that decade.

3.2.2 Determination of optimum threshold Tt for the calibration zone

In order to determine the optimum temperature threshold for the zone, the CCD images at a number of different thresholds are compared with contemporaneous rain gauge data. The optimum threshold is the one, which shows the highest level of agreement with the gauge data as to whether or not rainfall has occurred within pixels containing gauges. This can be done most conveniently using contingency table as shown below

| | CCD = 0 | CCD > 0 |
|-----------|----------|-----------------|
| Gauge = 0 | N_{ll} | N_{12} |
| Gauge > 0 | N_{21} | N ₂₂ |

Where:

• N_{11} is the number of occasions when both gauge records zero rain and CCD is zero.

- N_{12} is the number of occasions when gauge records zero but there is some CCD.
- \bullet $N_{\rm 21}$ is the number of occasions when gauge records some rain but CCD is zero.
- N_{22} is the number of occasions when gauge records and CCD values are non-zero.

 $(N_{\rm 11}~and~N_{\rm 22}\,)~$ represent agreement between the gauge and the satellite while $(N_{\rm 12}~and~N_{\rm 21})$ represent disagreement.

For the optimum temperature threshold, we would like the number of occasions on which the satellite and gauge agree to be much greater than the number of disagreement. Also the number of occasions for which the gauge register rain but there is zero CCD should just be roughly balanced by the number of occasions for which the gauge registers no rain but there is some CCD. Thus the two conditions for the optimum temperature threshold are:

$$N_{11} + N_{22} >> N_{12} + N_{21}$$

 $N_{12} \cong N_{21}$

The most important parameters that should be seen to choose optimum threshold temperature are:

1.Percent correctness \rightarrow P_{C} = $(N_{11}$ + $N_{22})\,/\,($ N_{11} + N_{22} + N_{21} + $N_{12})$ to check the accuracy

2.Bias = $(N_{12} + N_{22}) / (N_{21} + N_{22}) =$ (estimated rainy day/no of rain day), desired value = 1 to check un biasdnes.

3.HIT RATE \rightarrow HR = (N₂₂) / (N₂₂ + N₂₁) = (fraction of observed rainy day that are correctly estimated), desired value = 1

4.FAR (false alarm rate) = $(N_{12}) / (N_{11} + N_{12}) =$ (fraction of observed dry day that estimated as wet), desired value = 0

5.Kuipers skill score \rightarrow KSS = (HR-FAR), desired value = 1

Success \rightarrow corresponds to CCD=0, R=0 or/and CCD>0, R>0 Too cold \rightarrow corresponds to CCD=0, R>0 Too warm \rightarrow corresponds to CCD>0, R=0

For too cold (if CCD = 0, R>0), then some warmer threshold would likely give the correct classification, hence the temperature threshold is too cold for discrimination. The reverse is true for too warm.

In this study CCD30 and CCD40 decadal data are compared, it is shown that CCD 30 is an optimum threshold which shows the highest level of agreement with the gauge data in this region. See appendix C-1

The result of the analysis of the daily CCD30/Rain data pairs for Naivasha based on the above five conditions, including the contingency table are shown below, for decade see appendix C-1

| | | | March | | | | | | | April | | | |
|------|------|------|---------|------|------|------|------|------|------|----------|------|------|----------|
| | | | Ir=0 | Ir=1 | | | | | | Ir=0 | Ir=1 | | |
| | - | Ic=0 | 2551 | 597 | | | | | IC=0 | 1275 | 658 | | |
| R > | 0mm | Ic=1 | 596 | 586 | | | R > | Omm | Ic=1 | 346 | 837 | | |
| h = | 0 | 2 | 4 | 6 | 8 | 10 | h= | 0 | 2 | 4 | 6 | 8 | 10 |
| PC | 0.72 | 0.74 | 0.75 | 0.75 | 0.74 | 0.74 | PC | 0.68 | 0.66 | 0.64 | 0.62 | 0.59 | 0.60 |
| Bias | 1.00 | 0.74 | 0.55 | 0.46 | 0.37 | 0.31 | Bias | 0.79 | 0.61 | 0.49 | 0.40 | 0.32 | 0.27 |
| HR | 0.50 | 0.39 | 0.31 | 0.27 | 0.22 | 0.19 | HR | 0.56 | 0.45 | 0.36 | 0.31 | 0.25 | 0.22 |
| FAR | 0.19 | 0.13 | 0.09 | 0.07 | 0.06 | 0.05 | FAR | 0.21 | 0.14 | 0.11 | 0.09 | 0.06 | 0.05 |
| KSS | 0.31 | 0.26 | 0.22 | 0.20 | 0.16 | 0.14 | KSS | 0.35 | 0.31 | 0.25 | 0.22 | 0.19 | 0.17 |
| | | | | | | | | | | | | | |
| | | | Мау | | | | | | | June | | | |
| | | - | Ir=0 | Ir=1 | | | | | - | Ir=0 | Ir=1 | | |
| | | Ic=0 | 2063 | 1124 | | | | | Ic=0 | 2015 | 846 | | |
| R > | 0mm | Ic=1 | 431 | 753 | | | R > | Omm | Ic=1 | 321 | 466 | | |
| h= | 0 | 2 | 4 | 6 | 8 | 10 | h = | 0 | 2 | 4 | 6 | 8 | 10 |
| PC | 0.64 | 0.64 | 0.63 | 0.62 | 0.60 | 0.60 | PC | 0.68 | 0.68 | 0.68 | 0.67 | 0.65 | 0.65 |
| Bias | 0.63 | 0.44 | 0.32 | 0.24 | 0.17 | 0.13 | Bias | 0.60 | 0.44 | 0.32 | 0.21 | 0.13 | 0.09 |
| HR | 0.40 | 0.30 | 0.23 | 0.18 | 0.14 | 0.10 | HR | 0.36 | 0.28 | 0.21 | 0.14 | 0.09 | 0.06 |
| FAR | 0.17 | 0.10 | 0.06 | 0.05 | 0.03 | 0.02 | FAR | 0.14 | 0.09 | 0.06 | 0.04 | 0.02 | 0.01 |
| KSS | 0.23 | 0.20 | 0.17 | 0.14 | 0.11 | 0.08 | KSS | 0.22 | 0.19 | 0.15 | 0.10 | 0.07 | 0.05 |
| | | | | | | | | | | | | | |
| | | | October | | | | | | | November | | | |
| | | - | Ir=0 | Ir=1 | | | | | - | Ir=0 | Ir=1 | | |
| | | Ic=0 | 1614 | 789 | | | | | Ic=0 | 1458 | 1282 | | |
| R > | 0mm | Ic=1 | 267 | 289 | | | R > | 0mm | Ic=1 | 396 | 794 | | |
| h= | 0 | 2 | 4 | 6 | 8 | 10 | h = | 0 | 2 | 4 | 6 | 8 | 10 |
| PC | 0.64 | 0.65 | 0.65 | 0.64 | 0.64 | 0.64 | PC | 0.57 | 0.55 | 0.53 | 0.52 | 0.49 | 0.50 |
| Bias | 0.52 | 0.28 | 0.14 | 0.07 | 0.04 | 0.02 | Bias | 0.57 | 0.41 | 0.29 | 0.21 | 0.15 | 0.10 |
| HR | 0.27 | 0.15 | 0.08 | 0.05 | 0.03 | 0.01 | HR | 0.38 | 0.28 | 0.20 | 0.15 | 0.11 | 0.08 |
| FAR | 0.14 | 0.07 | 0.03 | 0.01 | 0.01 | 0.00 | FAR | 0.21 | 0.15 | 0.09 | 0.07 | 0.04 | 0.03 |
| KSS | 0.13 | 0.08 | 0.05 | 0.03 | 0.02 | 0.01 | KSS | 0.17 | 0.13 | 0.11 | 0.08 | 0.06 | 0.05 |
| | | | | | | | | | | | | | <u> </u> |

Table 3.2 Determination of CCD30 slot for best estimation of daily rainfall for the Naivasha catchment.

| PC 0.77 0.78 0.77 0.76 0.75 0.75 | | | | | | | |
|---|------|------|------|----------|------|------|------|
| $\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$ | | | | December | | | |
| R > 0mm Ic=1 174 258 h= 0 2 4 6 8 10 PC 0.77 0.78 0.77 0.76 0.75 0.75 | | | | Ir=0 | Ir=1 | | |
| h= 0 2 4 6 8 10 PC 0.77 0.78 0.77 0.76 0.75 0.75 | | | IC=0 | 2752 | 712 | | |
| PC 0.77 0.78 0.77 0.76 0.75 0.75 | R > | 0mm | Ic=1 | 174 | 258 | | |
| | h= | 0 | 2 | 4 | 6 | 8 | 10 |
| Bias 0.45 0.24 0.13 0.08 0.06 0.04 | PC | 0.77 | 0.78 | 0.77 | 0.76 | 0.75 | 0.75 |
| | Bias | 0.45 | 0.24 | 0.13 | 0.08 | 0.06 | 0.04 |
| HR 0.27 0.17 0.10 0.06 0.04 0.02 | HR | 0.27 | 0.17 | 0.10 | 0.06 | 0.04 | 0.02 |
| FAR 0.06 0.02 0.01 0.01 0.00 0.00 | FAR | 0.06 | 0.02 | 0.01 | 0.01 | 0.00 | 0.00 |
| KSS 0.21 0.15 0.09 0.06 0.04 0.02 | KSS | 0.21 | 0.15 | 0.09 | 0.06 | 0.04 | 0.02 |

The above contingency table reveal a problem with the satellite data, for most months the bias is nearly always below 1.0. December is the worst, when bias = 0.45 for rainfall>0, using CCD>0. This means more than half of the rainfall events are not detected by the satellite.

3.2.3 Calibration of parameters

The choice of approach in determining the parameter \mathbf{a}_0 and \mathbf{a}_1 in the equation 3.1 depends to a large extent on the application.

Three approaches described by include: (Grimes et al., 1993) as described in (Adegu, 1999)

(A) Days are classified according to CCD values. Regressing the median gauge in each class against the mid-class CCD carries out the calibration. The choice of the median as the representative rainfall value prevents abnormally large events from having an undue influence on the calibration.

(B) Mean rain gauge values are regressed against mean CCD for the pixels containing rain gauges, with the assumption that the gauge pixels are representative of the rainfall/CCD relationship for the area.

(C) Mean gauge value is regressed against mean CCD for the area, with the assumption that the gauge pixels are representative of the area rainfall.

Since the ultimate goal of this thesis is to estimate rainfall for hydrological purposes, method **B** and **C** are adopted in the analysis.

3.2.4 Evaluation (geostatistical approach) of rainfall estimates.

Interpolation (Kriging)

There is a difficulty in comparing data from gauges with those from satellites in that they provide two different kinds of information. Satellite estimates are essentially average of the area of the satellite pixel, where as gauges provides measurement made at a point (Grimes and Rogerio, 1998).

For meaningful comparison between the two data sets, one must be either derive point value from the satellite pixel or compute pixel areal average from rain gauge data. Here we choose the latter approach; this can be conveniently carried out by using **block kriging** (Journel and Huijbregts, 1978). As discussed in, (Grimes and Rogerio, 1998).

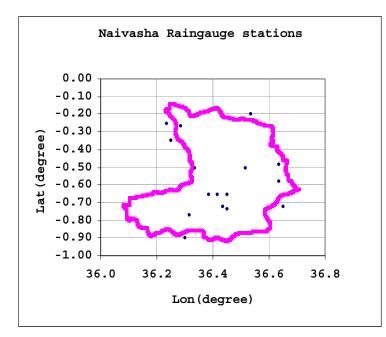
We are interested in the mean rainfall, P_{At} over area A at time t. This can be found by first determining rainfall estimate P_{rt} at any other point at distance r in the area under study from the available rain gauge data. Then, the area rainfall estimate, can be integrated numerically from the equation:

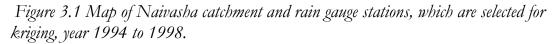
$$\mathbf{p}_{\mathbf{At}} = \mathbf{1}/\mathbf{A} \int_{A} P_{rt} dr \dots (3.7)$$

This quantity \mathbf{p}_{At} obviously unknown, since the rainfall depth is accessible only at finite number (say, n) of scattered point wise observations. It is therefore common practice in hydrology to estimate \mathbf{p}_{At} using linear estimator of the form:

$$\mathbf{p}_{At} = \sum_{j=1}^{n} \lambda_j p(x_j)$$
.....(3.8)

That is as weighted mean of the random variables $P(X_1)$, $P(X_2)$, P(Xn) observed at the rain gauges.





The linear estimates should satisfy two main conditions; these are

• Estimate is Unbiased

$$\sum \lambda_j = 1.....(3.9)$$

• Estimate has minimum error. (Journel and Huijbregts, 1978)

Where μ is a LaGrange multiplier, $\gamma(X_i, X_j)$ is the rainfall variogram function (matrix) among **n** measuring points, and $\gamma(X_i, X_0)$ is variogram values between each measurement point and estimation point. Therefore, if the variogram function is known, two matrices can be built to find the unknown weights and LaGrange multiplier.

Variogram

The variogram $\gamma(X_i, X_j)$ describes the variation of the correlation of rainfall field with distance. It is defined as (Jobard and Desbois, 1992).

$$\gamma(h) = \gamma(X_i - X_j) = 1/2n(h) \sum_{i=1}^{n(h)} \{P[X+h] - P[X]\}^2$$
(3.11)

where **h** is the vector separating X_i and X_j and **n(h)** is the number of gauge pairs with separating vector (h). This is on the assumption of a constant mean and infinite variance (intrinsic hypothesis), the mean and variance of the first order increments are independent of the actual locations and dependent only on the vector difference (h).

Where gauges are sufficiently close that their observed rainfalls are well correlated, $\gamma(\mathbf{h})$ will have a **small** value. Where the gauges are further apart, $\gamma(\mathbf{h})$ is **large**, eventually reaching a limiting value equal to the spatial variance of the rainfall field. The inclusion of $\gamma(\mathbf{h})$ in equation (3.9) and (3.10) means that both the rainfall estimates and their associated errors take account of the distribution of the gauges relative to the spatial structure of the rainfall.(Clark, 1979).

Here in the above equation if we use $P^*(x) = (P_i - P_{mean}) / P$ then the variogram becomes *standardized*.

$$\gamma^*(h) = 1/2n(h) * \sum_{i=1}^{n(h)} [P^*(x) - P^*(x+h)]^2$$
(3.12)

Where:

$$\gamma^*(h) = \gamma(h) / \sigma^2$$
.....(3.13)

Climatological variogram

In application to real-time estimation of areal rainfall, previous studies (Bastin et al.,1984, Label and Bastin, 1985) have lead to the development of "climatological kriging" i.e., kriging with a "climatological Variogram" as the covariance function. As described in, (Lebel et al.,1987)

We have, n points and t time steps, if we look at variogram at t-steps we will have t variograms, but the number of gauge stations (n) is very small. Hence, apart from being laborious, the t-variogram will have poor quality. The idea of climatological variogram is then to obtain a single variogram from all (n*t) points.

The same as the above is applied with a little modification

Where:

 $P^*(x) = P_i - P_{mean} / \sigma P$

Monthly variogram:

For the Naivasha catchment, variograms were determined on the basis of months (grouping wet season months data together), for the period 1994-1998. The variogram function was standardized by spatial mean and variance (σ^2) of each data set. Illustrations of the variograms obtained are shown in Figure 3.2.

<u>Model</u>

The main types of the theoretical variogram models commonly used are.(Delhomme, 1978):

• Exponential model:-

$\gamma(d) = C0 + C1 \{1 - \exp[-(d/a)2]\}$

• Spherical model:-

 $\gamma(d) = C_0 + C_1 [(3/2) (d/a) - (1/2) (d/a)^3]$ for d <a

 $\gamma(d) = C_0 + C_1$ for $d \Rightarrow a$

where $\mathbf{d} =$ denotes the length of the vector \mathbf{d} , \mathbf{C}_0 is the *nugget* effect, $\mathbf{C}_0+\mathbf{C}_1$ is the *sill* and \mathbf{a} is the *range*. The variogram approaches the sill when the distance approaches the range.

Range:

It is the distance at which the model reaches its maximum value or sill. The larger the range, the stronger the spatial correlation. The variance of the estimation error decreases with increase of range.

Sill:

The upper limit of any variogram model which has such a limit. If the variogram goes beyond the sill then it is an indication of a trend.

Nugget:

This is a discontinuity at the origin. It is variance at very low distances. It caused by smallscale variations or by measurement error. With the nugget effect the kriging weights become more similar and the variance of the estimation error increases.

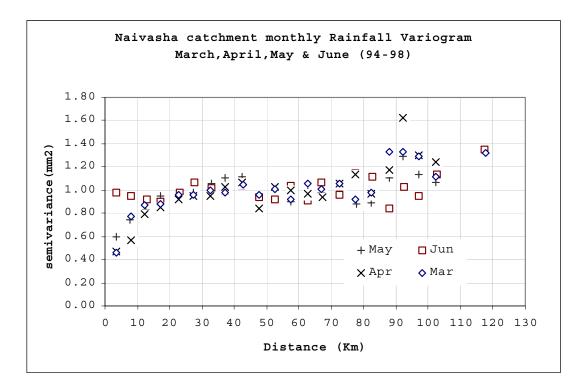
Model fitting

There are two type of model fitting, these are:

1.interactively (Visual) if only for smooth variograms

2.statistical fitting : these are least square and maximum likelihood

Generalized least square fitting method and exponential model is applied here, since most of the time rainfall varies exponentially with space and time. See Fig 3.2 and 3.3



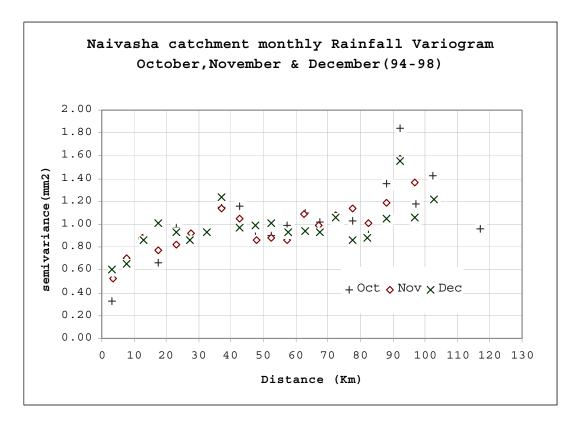
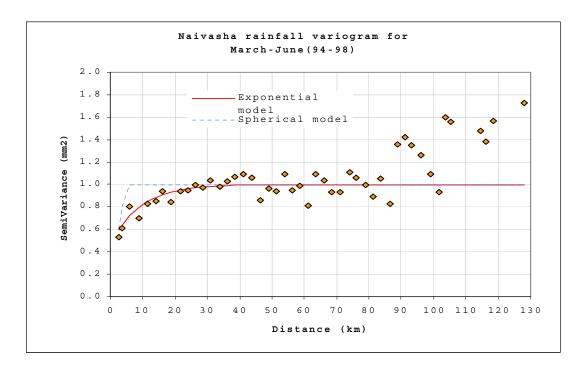


Figure 3.2 Graphical illustration of monthly variograms for rainfall data (1994-1998), with lag spacing of 5 km for the above 30 station. (for daily data) before combining the long and short rainy season months.



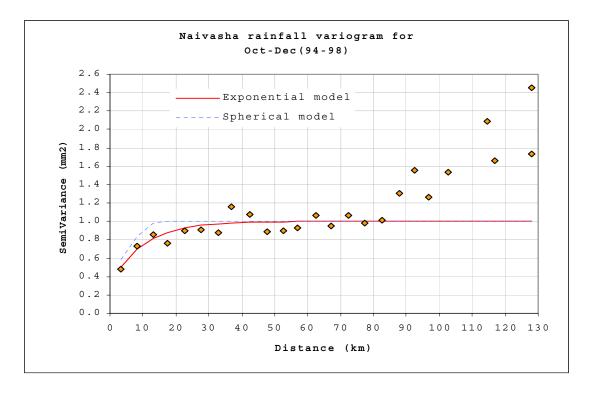


Figure 3.3 Graphical illustration of variograms for March-June and October-November rainfall data (1994-1998), with lag spacing of 2.5Km and 5km respectively for the above 30 stations. (For daily data).

All the variograms for the months are fairly close to each other and consistent between themselves, hence only two variograms one for Oct, Nov and Dec and another for the other months can be used. The only month outside is June because of strange rainfall values and less data points than the other months.

The big advantage in putting several months together is that it is possible to get more data to use a smaller lag, in this case it is very important since the data is so noisy.

After combining the months we use lag spacing 2.5km and 5 km for the derivation of variograms, for the long and short rainy season respectively, because the variograms at this spacing are not too noisy and not too smooth. (See appendix D, for decadal scale)

Table 3.3 Summary result of fitted theoretical variograms to the experimental variograms for the wet season of the year (Naivasha rainfall data 1994-1998).

| | MONTH | Range | Sill | Nugget |
|---------|---------------------|-------|------|--------|
| Daily | MAR to June | 9 | 0.54 | 0.46 |
| | October to December | 10 | 0.68 | 0.32 |
| | MAR to June | 14 | 0.92 | 0.08 |
| Decadal | October to December | 14 | 0.95 | 0.05 |

The range for the Naivasha catchment varies between 9-14km (for both daily and decade scale) this is generally a low value, the sill values γ are always greater than 0.5 for both daily and decadal scale and the nugget effect is high for daily data this is may be an indication that the spatial variability of the rainfall in this region is high, this can be supplemented by the following two graphs.

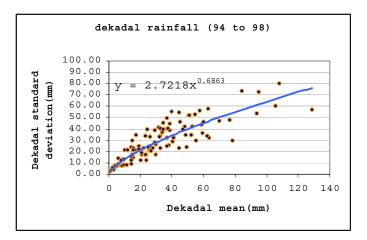


Figure 3.4 Plot of standard deviation against mean rainfall for decadal data (1994 to 1998) for the above 30 station.

Estimation of rainfall using METEOSAT TIR data for the Naivasha catchment (Kenya)

From the plot above, the standard deviation of decadal rainfall for the area is comparable to the decadal mean rainfall, besides the standard deviation increase as the rainfall value increase, which is called **heteroscedasticity** which causes a problem to plot a regression line between rainfall and CCD.

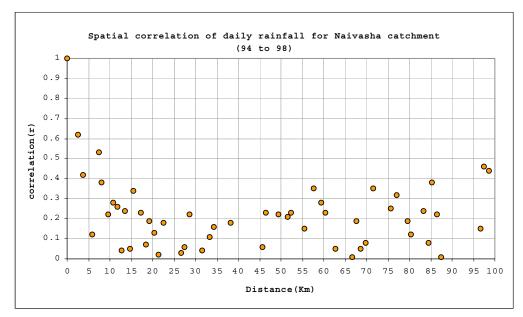


Figure 3.5 Graph, showing the spatial correlation of daily rainfall for the Naivasha catchment using 30 stations for the year 1994 to 1998.

The spatial correlation of the daily rainfall data is less than 50% after 5km.

Remarks: Due to the high nugget effect in almost all the variograms, the high spatial variation of the rainfall and low density of gauge in the region, arithmetic mean and Thiessen polygon can be used to find the area rainfall, see appendix G.

Note: because the variogram shows us the spatial characteristics of the rainfall around the area we use all the 30 stations inside and around the catchment to derive the variogram. But for kriging, we used only 16 stations. 11 stations inside and 5 stations around the catchment. see Fig 3.1.

3.2.5 Calibration for hydrological monitoring

In the hydrological case, the greatest importance is attached to successful estimation of heavy rainfall. Furthermore, for short-medium term flow forecasting daily or decadal data is usually required.(Grimes, Bonifacio and Loftie, 1998):

Preliminary preparation of the CCD images involved the conversion of Meteosat images to Longitude-Latitude projection by the AWK program.

The following scheme was devised to allow decadal or daily estimation on a catchment basis,

• A mask image is created for which each pixel within the catchment is assigned the value 1; each pixel outside the catchment is assigned the value zero. In this study IDRISI, modules INITIAL and POLYRAS were used to create the mask image.

• The decadal (daily) CCD image is multiplied by the mask, and the average value of CCD within the Catchment, \mathbf{D}_{av} calculated. (achieved through Meanpol prog).

• A decadal (daily) average area rainfall value for the catchment \mathbf{R}_{av} is calculated (kriged).

• A linear regression is performed of R_{av} against D_{av} to determine the calibration parameter a_0 and a_1 from the relation,

Once the parameter \mathbf{a}_0 and \mathbf{a}_1 are found, rainfall estimates can be calculated from equation (3.14) for any other period. Because the calibration has been performed on non-zero CCD days only, the relationship only applies to the fraction of the catchment with non-zero cold cloud. Thus, if the average CCD over the area covered by cold cloud (the rainy area) is $\mathbf{D'}_{av}$, the average rainfall over the same area is:

 $R'_{av} = a_0 + a_1 \times D'_{av}$ (3.15)

However for hydrological purposes, (Grimes, Bonifacio and Loftie, 1998): it is convenient to calculate the average rainfall over the whole catchment rather than the average over the rainy area. If the area covered by CCD is \mathbf{f} , then the average rainfall over the whole catchment is,

 $R_{av} = f(R'_{av})$ = f(a₀ + a₁× D'_{av}) = fa₀ + a₁fD'_{av}

But fD'_{av} is the average CCD over the whole catchment (including the zero CCD fraction). Then R_{av} is,

 $R_{av} = fa_0 + a_1 D_{av}$ (3.16)

Where: \mathbf{D}_{av} is the average CCD over the whole catchment. Figure 3.10 illustrates this procedure.

Derivation of the above constants a_0 and a_1 using only area covered by CCD (wet) is preferable, provided that the area is very big in size. In this study, it doesn't matter much which approach is used, since, the Naivasha catchment is very small in size.

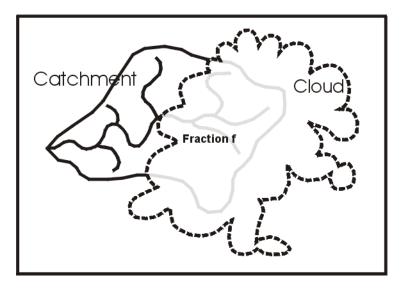


Figure 3.6 Cold Cloud over the catchment. The intersection of the cloud area and the catchment is the fraction \mathbf{f} of the catchment covered by cloud. (Modified from NRI-TAMSAT).

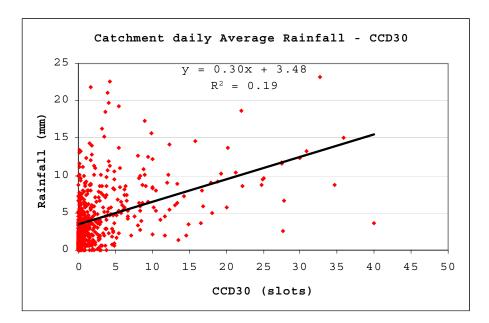
To obtain f (the area cover) the following procedure is followed,

• A mask image of each CCD image (already converted to Longitude/Latitude projection) is created. By the module RECLASS in IDRISI, all pixel values of the CCD image greater than 0 (in this case, 1-48), are assigned the value 1.

• The daily CCD image is then multiplied by the catchment mask image, and the mean value of the resultant image is obtained. This gives the daily mean fraction of catchment covered by cold cloud, **f**. (Executed through "Meanpol program").

The calibration is carried out for the wet season of Naivasha. The results of the calibration procedure for the Naivasha catchment is shown in graphical illustration in figure 3.11 and appendix E.

Note: pixel calibration is also carried out for the decadal data just to have some idea of the distribution of rainfall within the catchment. Averaging the resulting rainfall estimate image with a catchment mask would give us a mean amount over the catchment.See, appendix H for the plot.



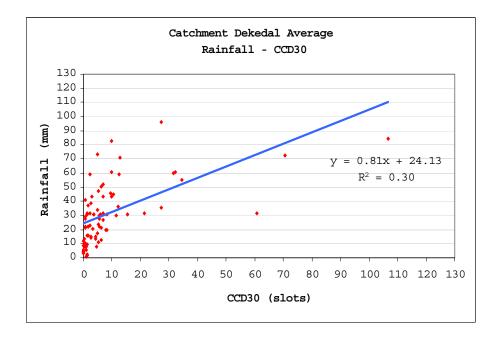


Figure 3.7 Graph showing relation between CCD and rainfall, for daily and decadal rainfall data (1994 to 1998).

CHAPTER 4

4. PRECIPITATION AND CCD CORRELATION ANALYSIS

4.1 Introduction

Besides the sparse distribution of gauges inside the Naivasha catchment, large variation in precipitation over relative short distance contributes to poor correlation.

In the table daily rainfall for a few selected stations are listed.

Table 4. 1 Daily rainfall for a few selected stations, which have large variation as compared to nearby stations.

| Date | Station | Recorded value | Near by stations(5-25km) recorded value |
|----------|---------|----------------|--|
| 07/10/97 | 9036308 | 148.5mm | 0 - 5 mm |
| 21/04/98 | 9036308 | 100.5mm | 0-10mm |
| 15/05/95 | 9036072 | 93.5mm | 0-10mm |
| 12/03/95 | 9036323 | 104.6mm | 0-10mm |

This may show that either the gauge recording may not be very good or that strong convectional rainfall occurs. This causes problem to the calibration (makes it noisy).

As seen in the bias and accuracy presented in chapter three, in this region the cloud produces rain without reaching enough in to the atmosphere to register as "cold" clouds. In such cases rainfall would indeed occur but would not appear in the satellite rainfall estimate image.

All the above problem from CCD image and rainfall data lead us to treat the data in a more detailed statistical approach.

Daily and decadal CCD data for the year 1994 to 1998; the corresponding rainfall data from 30 stations in and around the catchment is also available. Out of 32101 available rainfall data 3647 data are missed, the daily raingauge data is found in the xls file, the decadal data is attached to appendix B.

Using the above data set, it is tried to do the univariate statistics for the raw data. Since the data is not normally distributed. Transformation of the data is executed through Box-Cox transformation.

The regression analysis is applied for the transformed data since in this stage the data already satisfies the regression assumption. It is also shown that there is a significant relation ship between the CCD and rainfall transformed data, then the CCD and kriged rainfall relationship established.

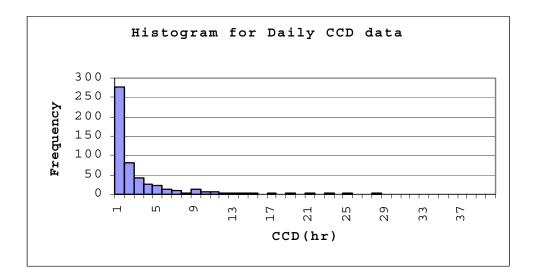
4.2 Univariate statistics on the CCD and rainfall data

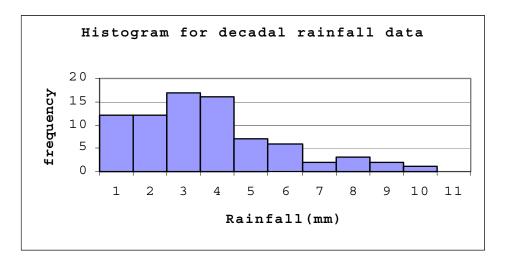
It is generally risky to assume the distribution of the data is normal without actually examining some statistical parameters of the data..

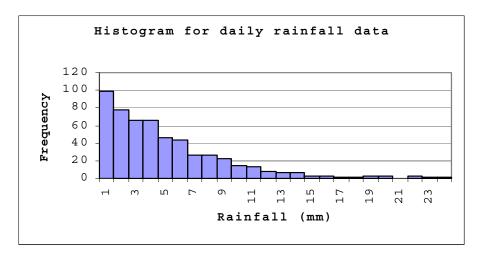
The normal distributions provide good models for some distributions of real data In this study it is tried to judge whether the row data is normally distributed or not, by constructing a histogram for both CCD and rainfall data set. (see Fig 4.1) all the data set are not normally distributed.

Table 4.2 Summary result of some descriptive parameters for the raw CCD and rainfall data.

| | data | Mean | Median | Skewness | standard | deviation | Maximum | Minimu | Kurtosis |
|---------|----------|-------|--------|----------|----------|-----------|---------|--------|----------|
| | type | | | | | | | m | |
| Daily | CCD | 3.16 | 0.91 | 3.29 | | 5.76 | 39.94 | 0.02 | 12.31 |
| Data | rainfall | 4.43 | 3.48 | 1.59 | | 4.01 | 23.16 | 0.00 | 3.24 |
| Decadal | CCD | 9.42 | 4.79 | 3.83 | | 16.56 | 106.60 | 0.09 | 17.45 |
| data | rainfall | 32.27 | 29.68 | 1.57 | | 24.06 | 136.14 | 0.86 | 3.75 |







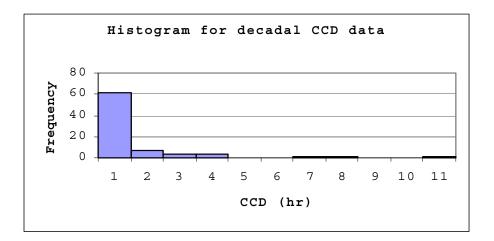


Figure 4.1 Histogram plot which shows that the above data sets are not normally distributed.

4.2.1 Normal Quantile plot

If x is an observation from a distribution that has mean μ and standard deviation $\sigma,$ the standardized value of x is

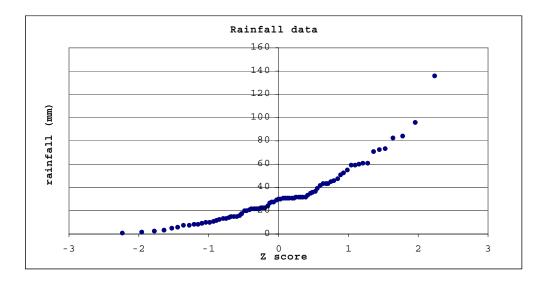
 $Z = (x-\mu)/\sigma$

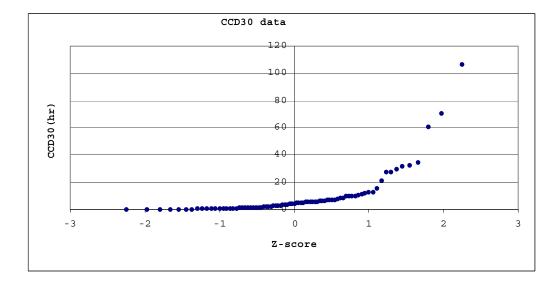
A standardized value is often called a z- score

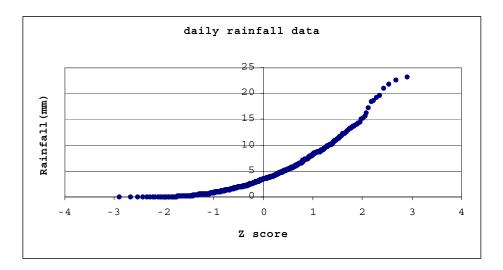
The most useful tool for assessing whether the data is normally distributed or not is the normal quantile plot; it is a plot, which shows the data points x against the corresponding Z score.

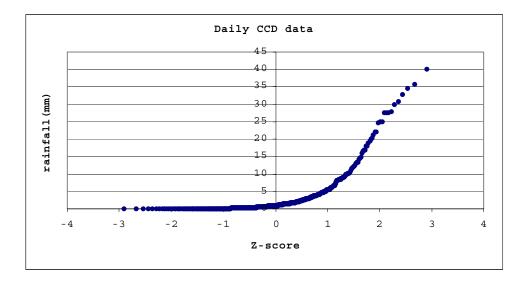
Fig 4.2 shows normal quantile plots for decadal rainfall and CCD data, it is shown that there is a deviation from a straight line which indicates that the data are not normally distributed,

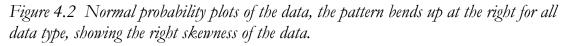
the skewness of the distribution on the above summary table indicate that the distribution is right-skewed. In a right-skewed distribution, the largest observations fall distinctly above a line drown through the main body of points.











The distributions are different from normal distribution and positively skewed. This indicates that the assumption of constant standard deviation, or homogeneity of variances is violated, this can cause regression difficult between the two data set.

4.3 BOX-COX transformations

It is possible to improve the above model by applying transformations of the data.

There are really three situations in which transformation of the data may be appropriate in regression analysis. (Cook and Weisberg, 1982); these are: as discussed in (Clarke, 1994)

1.Where the response variable **Y** comes from a family of distributions known to be nonnormal. A transformation is selected so that the distribution of the transformed responses is sufficiently near to normal to allow us to use standard methods, based on normal theory.

2. Where the expected response $\mathbf{E}(\mathbf{Y})$ is related to the explanatory variables \mathbf{X} by a known non-linear function of the parameters. A transformation is selected to **linearise** this response function;

3. Where neither the distribution of error nor the functional form of the relationship between **E** (**Y**) and **X** is known. This situation is the most difficult to handle since a specific rationale for choosing a transformation is lacking. Generally, we would like a transformation to result in a model with constant error variance, approximately normal errors, and a systematic component **X** $\boldsymbol{\beta}$ which is easily interpreted in hydrological terms.

One method of proceeding in case 3 is to specify a family of transformation **R** (**P**), with parameter **P**. We then use the data to select which transformation **R** (**P**) of the family is most appropriate, in the sense that it yields a model **R**(**P**) = $\mathbf{X}\beta + \boldsymbol{\varepsilon}$ having all the desirable properties. (Clarke, 1994).

One such family of transformation is the **Box-Cox** family; which finds transformation to **maximize correlation** between two variables; it is defined by,

$R_T = (R^P-1)/P$ when P is non zero = logR when P is zero

In this case, **R** is rainfall, which is being transformed; $\mathbf{R}_{\mathbf{T}}$ is the transformed variable. **P** is transformation variable parameter, usually in the range between 2 and -2.

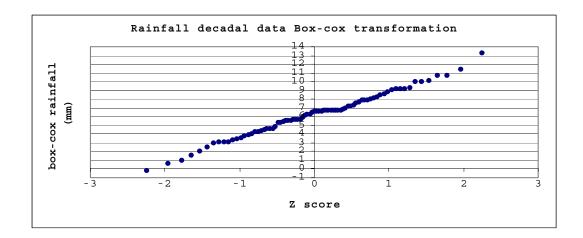
The transformation is carried out by varying \mathbf{p} until the skewness of the transformed data becomes zero.

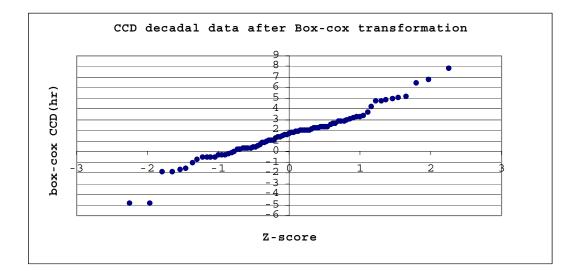
| | P for kriged rainfall | P for CCD |
|--------------|-----------------------|-----------|
| Decadal data | 0.35 | 0.35 |
| Daily data | 0.21 | 0.21 |

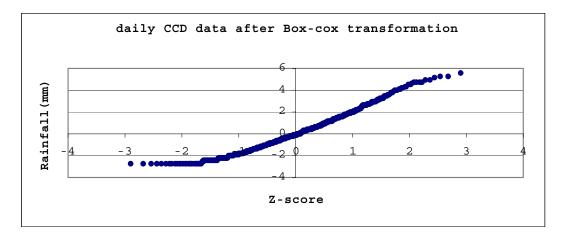
Table 4.3 The assumed values for the transformation variable parameter

The normal quantile plot is constructed between the transformed data and the

Z score including the histogram. The straight pattern for all the data shows that the distribution of the data after transformation is close to normal, the same is true for the histogram, which shows approximately normal distribution for the entire data set.







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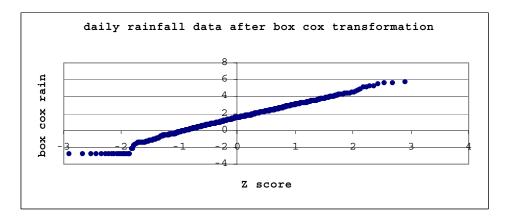
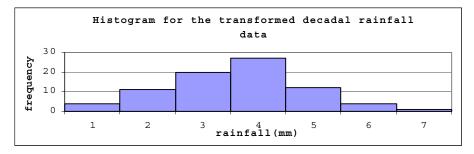
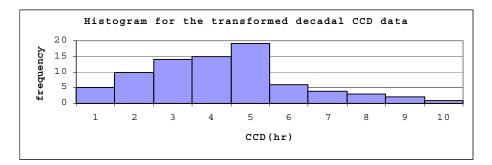
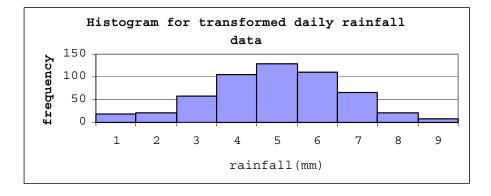


Figure 4.3 Normal probability plots of the rainfall and CCD data. The straight pattern shows that this distribution is close to normal. There are also low outliers in CCD and rainfall data plot.







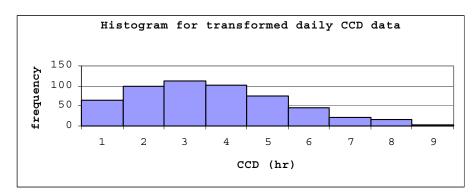
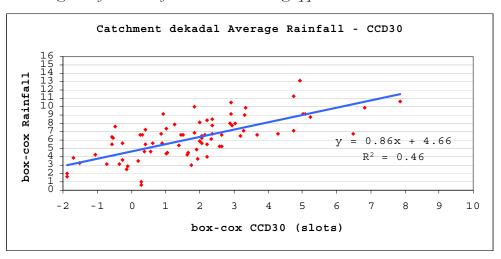


Figure 4.4 Histogram of the transformed data showing approximate normal distribution.



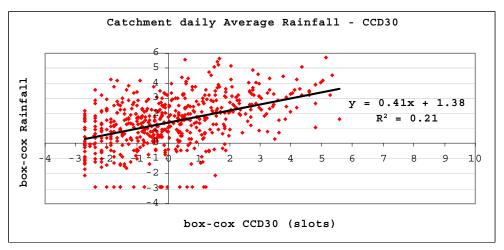


Figure 4.5 Graph showing the relation between CCD and rainfall data after Box-Cox transformation for decadal and daily data.

The plot of the transformed data indicates a better fit than the original data. In addition, the variability of the data across the horizontal range of the plot seems relatively constant, which satisfy the assumption of homogeneous variances.

4.4 Regression analysis and hypothesis testing

Using the Naivasha rainfall data set (30 stations, 1994 to 1998) and the CCD values extracted, regression analysis is applied for both daily and decadal transformed data.

Given **n** observations on the explanatory variable **x** and the response variable **y**,

$$(x_1, y_1)$$
, (x_2, y_2) , (x_n, y_n)

The statistical model for simple linear regression states that the observed response y_i when the explanatory variable takes the value x_i is

 $Y_i = \beta o + \beta_1 x_i + \varepsilon_i \dots 4.1$

Here $\beta_0 + \beta_i \mathbf{x}_i$ is the mean response when $\mathbf{x} = \mathbf{x}_i$. The deviation $\boldsymbol{\varepsilon}_i$ are assumed to be independent and normally distributed with mean 0 and standard deviation $\boldsymbol{\sigma}$.

The parameter of the model are β_0 , $\beta_1 x_i$ and σ . (David and Gorge, 1998).

From the equation for the regression line $\mu_y = \beta_0 + \beta_1 x$, β_0 is the mean response corresponding to x = 0. On the other hand, the test Ho: $\beta_1 = 0$ is useful, when we substitute $\beta_1 = 0$ in the model, the x term drops out and we are left with $\mu_y = \beta_0$, this means that in this model the mean of y does not vary with x.

The hypothesis H_0 : $\beta_1 = 0$ therefore says that there is no straight-line relationship between y and x and that linear regression of y on x is of no value for predicting y.

In this study it is tried to do the above hypothesis using t test statistics using 95% confidence interval.

A confidence interval for the intercept is $b_0 \pm t^* SE_{b_0}$

A confidence interval for slope is equal to $b_1 \pm t^* SE_{b_1}$

In this expression t is the value for the t (n-2) density curve with area of the curve between -t and t, and can estimated as

 SE_{b_1} is the standard error of the slope b_1

 SE_{b_0} is the standard error of the intercept b_0

$$SE_{b_0} = S\sqrt{\frac{1}{n}} + \frac{x^2}{\sum (x_i - x)^2}$$
....4.3

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To test the hypothesis Ho: $\beta_1 = 0$ we compute $t = b_1 / SE_{b_1}$

Where:

S is estimated standard deviation

$$S = \sqrt{\frac{\sum e_i^2}{n-2}} \dots 4.4$$

 e_i = the residuals = $y_i - \hat{y}_i$

x and \hat{y} are the mean of the data

n number of data

The degree of freedom is n-2. Interms of a random variable T having the t (n-2) distribution, the probability value for a test Ho against the two sided alternative is

Ha: $\beta_1 \neq 0$ is 2P (T $\geq |t|$)

The probability-value corresponding to t statistics in table 4.4 shows that there is strong evidence against the null hypothesis for the above transformed daily and decadal plot. So we may conclude that linear regression on CCD measure is useful for predicting rainfall for both daily and decadal data.

Table 4.4 Summary of t statistics for the transformed rainfall and CCD data.

| Decadale Regressi | on Statistics | | | | | |
|-------------------|---------------|----------------|--------|----------|-----------|-----------|
| Multiple R | 0.68 | | | | | |
| R Square | 0.46 | | | | | |
| Adjusted R Square | 0.46 | | | | | |
| Standard Error | 1.86 | | | | | |
| Observations | 79 | | | | | |
| | Coefficients | Standard Error | t Stat | P-value | Lower 95% | Upper 95% |
| βο | 4.66 | 0.28 | 16.59 | 4.E-27 | 4.10 | 5.22 |
| β1 | 0.86 | 0.11 | 8.13 | 5.64E-12 | 0.65 | 1.07 |
| Daily Regression | 1 Statistics | | | | | |
| Multiple R | 0.45 | | | | | |
| R Square | 0.21 | | | | | |
| Adjusted R Square | 0.21 | | | | | |
| Standard Error | 1.48 | | | | | |
| Observations | 540 | | | | | |
| | Coefficients | Standard Error | t Stat | P-value | Lower 95% | Upper 95% |
| βο | 1.38 | 0.06 | 21.61 | 5.13E-75 | 1.26 | 1.51 |
| β1 | 0.41 | 0.03 | 11.84 | 6.44E-29 | 0.34 | 0.48 |

4.5 Estimation of rainfall from CCD

It is clear that the relation between CCD and precipitation is poor for daily data The improvement in correlation coefficient in decadal data is quite notable. On decadal bases the correlation coefficient reaches 0.68. The standard error (the standard deviation of the rainfall about the regression line, and is given by equation 4.4) is 1.86mm on the average for the decade. For daily data the correlation coefficient is 0.45, the standard error is 1.48mm.See table 4.4, for the detail of regression analysis.

Finally the calibration plot is constructed between the rainfall and the CCD data after the rainfall is estimated in terms box-Cox transformed CCD data, See Fig 4.5 for decadal and daily calibration plot.

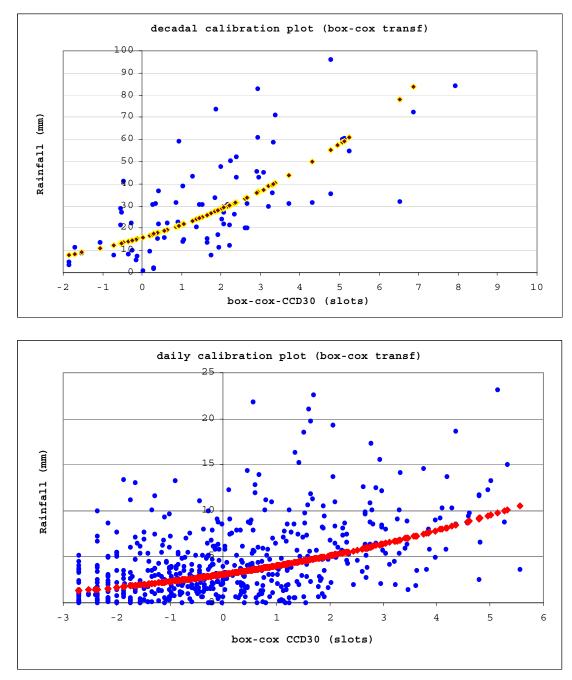


Figure 4.6 Calibration plot, the estimated rainfall is in terms of Box-Cox transformed CCD data.

In Fig4.5 the regression line between the already transformed CCD and rainfall data is presented, so the equation for these graphs have the form:

 \mathbf{R}^* is the transformed rainfall data, which is equal to

 $R^* = (R^{Pr} - 1) / P_r$4.6

R is the rainfall data before transformation (the raw data).

 \mathbf{P}_r is transformation variable parameter, is equals to 0.35 for both daily and decadal rainfall data.

CCD^{*} is the transformed CCD data, which is equals to

CCD is the Cold Cloud duration data before transformation (raw data), and here

 $\boldsymbol{P}_{ccd}~$ is equals to $\boldsymbol{0.21}$ for both daily and decadal CCD data.

Combining equation 4.4 and 4.5

$$(R^{P_{r}} - 1)/P_{r} = a_{o}CCD^{*} + a_{1}$$

The equation of the line for the calibration plot which is presented on Figure 4.4 become

 $R = \{ [a_o CCD^* + a_1] * P_r + 1 \}^{1/P_r} \dots 4.8$

We can further expand the above equation in the form of the following

$$R = [\{ [a_o ((CCD^{P_{ccd}} - 1)/P_{ccd}) + a_1] \} * P_r + 1]^{1/P_r}4.9$$

Assume

$$[a_{o}((CCD^{P_{ccd}}-1)/P_{ccd})+a_{1}] = K$$

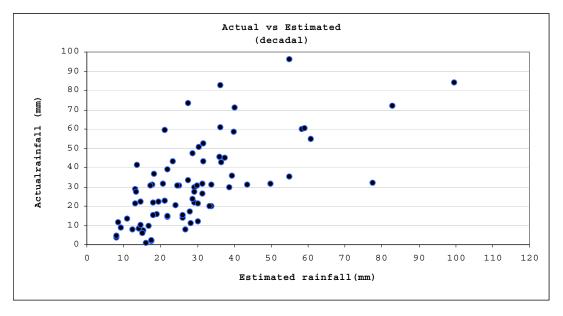
Estimated rainfall become:

$$R = [K* P_r + 1]^{1/P} \dots 4.10$$

So before we estimate the rainfall from CCD, the CCD data has to be transformed, using Box-Cox transformation.

4.6 Deviation assessment

Following the poor correlation between CCD and rainfall some assessment is done just to have an overview of the deviation between actual and estimated rainfall and to discern where the maximum error occurs, see Fig 4.5 and 4.6 and see appendix F for the calculation.



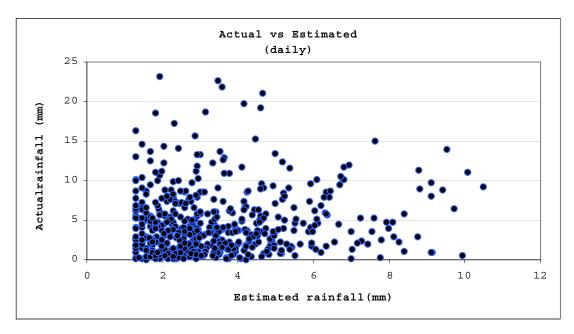
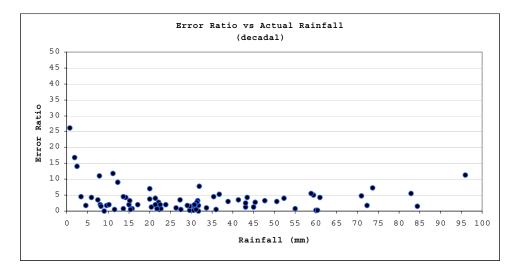


Figure 4.7 Graph showing actual rainfall Vs Estimated rainfall (decadal and daily data, 1994 to 1998).



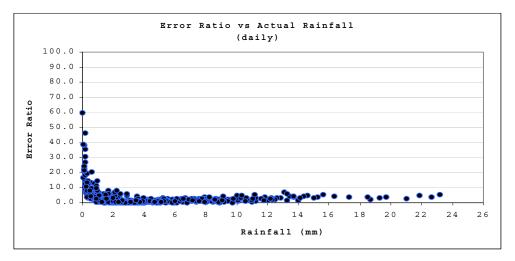


Figure 4.8 Graph showing error ratio (ratio between absolute and actual error) Vs actual rainfall (decadal and daily data, 94 to 98).

Absolute error = ABS (estimated rainfall-actual rainfall).

Actual error = error calculated by kriging.

If we draw a straight line Y = X on the scatter plot of fig 4.5, we find almost equal amount of underestimate and overestimate values showing the estimated rainfall is unbiased.

Actually notable error also occurs for the value between 0 to 1 mm for daily and 0 to 5mm for decadal data, otherwise the estimated value doesn't have notable error as compared to the actual rainfall.

4.7 Discussion of the result

It is shown that the CCD and rainfall data are not normally distributed. To satisfy the assumption of regression model between the two data points, the data were transformed using Box-Cox transformation. Consequently the correlation between rainfall and CCD data remarkably improved, the hypothesis testing also proves that linear regression on CCD measure is useful for predicting rainfall.

The calibration plot is constructed between the actual rainfall and the Box-Cox transformed CCD data and the equation of the line between these two data set is presented in equation 4.8.

As seen on the calibration plot which is presented above, there are data points which are deviated far away from the estimated rainfall line. The reasons for such discrepancies between ground based and estimated rainfall amounts may be manifold: among these, the following are common.

1. Raingauge do not always properly measure the actual rainfall amount reaching the ground. Differences up to 30% have been reported. (Huygen, 1989).

2. Because of the spatial and temporal variability of rainfall in the area, precipitation can not be determined accurately by means of interpolation (kriging). This error is caused by low density and heterogeneous distribution of rainfall stations as well as by inaccuracies in the measurement themselves. See Fig 1.3, 3.4, and 3.5. Moreover it is generally accepted that altitude is the main variable, governing the spatial distribution of rainfall in areas of complex topography. The area that has been selected for this study has a complex topography, but the daily or decadal rainfall data for the Naivasha catchment are not correlated with the altitude values. For this reason orographic effect were not considered in this study. See appendix H for annual rainfall and altitude relation.

3. Satellite TIR images are used to distinguish raining cloud from non- raining cloud on the basis of there observed cloud top temperature. This is because it is assumed that all rain comes from deep convective clouds with cold, high tops. However, even in the tropics there is some variability in the type of clouds, which produce rain. In particular, regions near the coast or in mountainous area (like, Naivasha) may experience rainfall from clouds, which have not formed from vigorous local convection. Consequently they do not reach high enough in to the atmosphere to register as "cold" clouds. In such cases rainfall would indeed occur but would not appear in the satellite rainfall estimate image. (Grimes, Bonifacio and Loftie, 1998). The contingency tables which is presented in chapter 3 reveals the above problem with the satellite data, for most months the bias is nearly always below 1.0. This means most of the time the rainfall events are not detected by the satellite.

The reverse is true for cirrus clouds; such clouds appear as very cold to the satellite and therefore would indicate the presence of rain, although infact the clouds are not enough for rainfall to develop.

4. Lack of a direct physical connection between the observed radiance and the precipitationsized drops falling at the surface (indirect measurement of rain) also contributes to the discrepancies between CCD and rainfall.

CHAPTER 5

5. Runoff response to CCD, rainfall and estimated rainfall events

5.1 Introduction

After rainfall falls on the earth, it evaporates, infiltrates or lies in the depression storage. When these losses become surplus flows, and thresholds are exceeded, runoff is generated over the surface to the nearest stream channel.

With an adjusted and well-measured rating curve (curve between stage and discharge on the same section of the river) the daily gauge reading can be converted directly to runoff volume.

Daily runoff hydrographs including CCD30, kriged rainfall and estimated rainfall are presented in Fig 5.2 and 5.3.

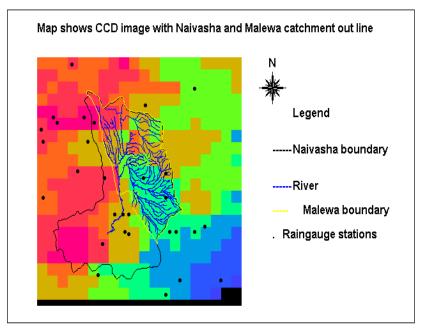


Figure 5.1 CCD image with Naivasha and Malewa catchment outlines including rain gauge stations.

5.2 Hydrology of the catchment

The main river in the Malewa catchment is the Malewa River; it has a number of tributaries, contributing to the discharge at the outlet of the catchment. (Fig 5.1).

The low relative humidity and the average daily temperature 24°C in the area combine to cause an annual potential evapotranspiration of 1500-1900mm/year (Trottman, 1998)

The rainfall pattern in this area is bimodal; the rainy seasons are typically from March to June (long rainy season) and from October to December (short rainy season).

5.3 Data analysis

5.3.1 Qualitative analysis

Due to the lack of discharge data for the period 1994 to mid 1997 for which the TAMSAT have been obtained, the analysis for this period could not be done.

Year 1997 short rainy season (October to December) and 1998 long rainy season (March to June) daily discharge data at the outlet of Malewa catchment and the corresponding CCD, rainfall data and estimated rainfall are used in the analysis of examining the cause and effect relationship between the events and the response. The result for the above two time periods is presented in the form of graphs below (Figs 5.2 and 5.3).

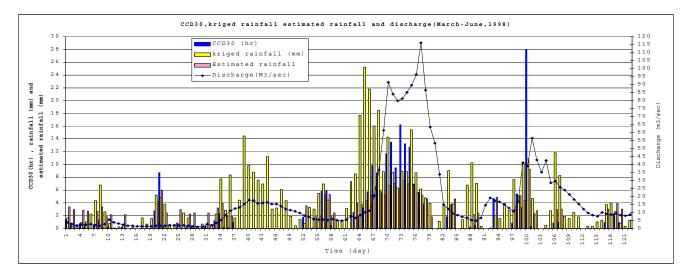


Figure 5.2 Runoff response at the outlet of Malewa for CCD, rainfall and estimated rainfall event (long rainy season 1998).

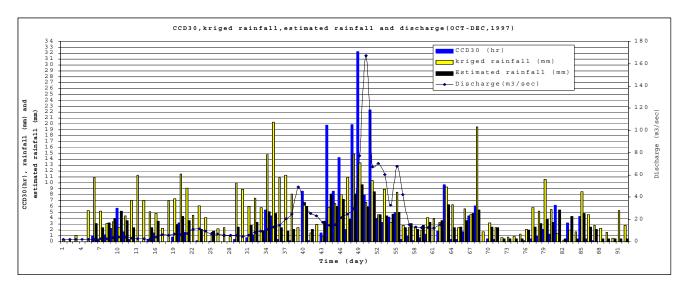


Figure 5.3 Runoff response at the outlet of Malewa for CCD, rainfall and estimated rainfall event (short rainy season 1997).

In fact it is difficult to evaluate the above graphs in this condition because most of the CCD data are missed and invalid, consequently it is difficult to say which event is best fit for the observed response. However, there is a cause and effect relationship between the events and the response even if it is difficult to know the exact lag between the events and the response.

There are also some discrepancies between the events and the response; it is tried to analyze these discrepancies by examining the CCD images on the date when these discrepancies occurred.

5.3.2 CCD image analysis

IMAGES: (refer to Table 5.1 and Figs 5.2, 5.3 and 5.4)

• L3L: it is the date when large CCD and very small response recorded. Large value of CCD are recorded at those pixels which are found at the most remote point of the catchment, so may be it takes time to see the corresponding response at the outlet of the catchment. The same may happened at KAA. (Fig 5.4).

• L68: large CCD small response. Those pixels, which are very near to the catchment, have small value of CCD and we may only see the response of these pixels with small lag time.

• L5C: CCD and large response, here most of the CCD pixels have average values. What this may show us is that possibly CCD has missed the rainfall event at this time, the opposite is happened at the date KBD is called False alarm rate.

Generally looking at the value of CCD on a pixel scale gives us a detailed overview distribution of rainfall within the catchment; the above daily images also indicate the problem of averaging CCD values over the area.

| Image | Julian day | Date |
|-------|---------------|----------|
| KAA | 10 | 10/10/97 |
| KBD | 44 | 13/11/97 |
| KBI | 49 | 18/11/97 |
| L3L | 21 | 21/3/98 |
| L5C | 73 | 12/5/98 |
| L68 | 100 | 8/6/98 |

Table 5.1 Table showing naming convention with the corresponding dates.

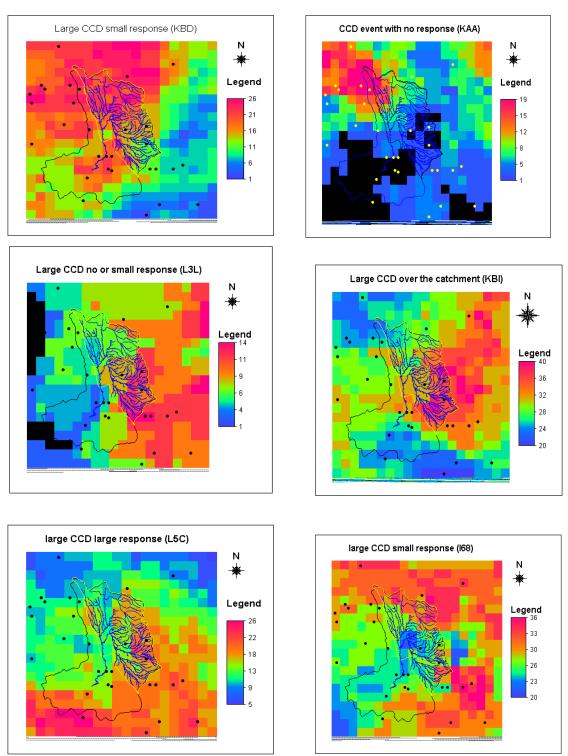


Figure 5.4 Daily CCD images for the date large discrepancies between the event and the response recorded.

5.4 Discussion of the result

In attempting to describe the rainfall event response process, one must keep in mind the possibilities that

• The water identified as the response to a given event may originate on only a portion of the watershed. That portion is called the **contributing area**.

• At least some of the water identified as the response to a given event may be "old water" that entered the watershed in a previous event. (Dingman, 1994).

Depending on the climate and the transmissivity of the aquifer bordering the stream, the lag between rainfall and runoff may extend to periods of days or weeks. (Wilsson, 1990).

Because the Malewa river is perennial it is always fed by base flow, even with a low dry season, and there may be a bank storage which flows into the river even in the absence of rain, that is why we may encounter a base flow throughout the season.

On the other hand there are dates when the CCD is high with very small response, this may be due to the high permeability of the soil in the catchment and high evaporation after rain to evaporate the water which is already available at a shallow depth below the surface.

There are also dates when there is quick responses to the event CCD this is may be due the presence of "old water" that entered in the watershed before this event.

CHAPTER 6

6. CONCLUSION AND RECOMMENDATION

6.1 Conclusions

In the thresholding technique the TAMSAT approach is a simple method to derive CCD within reasonable time scale. Moreover, it is automated and easy for operational application.

A statistical (Kriging) estimation technique for areal estimation is plausible, because this technique provides a mean rainfall over an area and an associated standard deviation. These values allow a better comparison of rainfall and satellite data.

The area of the Naivasha catchment is about 3200km² and the pixel size of the METEOSAT is 25km², only 128 pixels, nearly 11*11 pixel square area which is very small and very difficult to compare cloud and rain using only these pixels.

In the study area there are quite a few huge rainfall amount differences between even fairly nearby gauges. However, the bottom line is that in this region the satellite doesn't have much power to properly discriminate rainfall and in particular it misses a fair number of rainfall events, see the contingency table presented in chapter three, for most months the Bias is nearly always below 1.0. This means more than half of the rainfall events do not detected by the satellite. We would need a warmer threshold of CCD (say -20°C, which isn't available) to catch them.

It was shown that the relation between rain and CCD notably improved for the Box-Cox transformed variables, consequently the calibration plot has been carried out between rainfall and transformed CCD variables, this implies that the relation between rain and CCD is non-linear.

Hence trying to fit a linear relationship between the untransformed variables would be an error in this case.

Due to lack of CCD data for the year 1998 long rainy and 1997 short rainy season, it was difficult to compare the runoff response from CCD estimated rainfall and kriged rainfall events. Hence it is difficult to say the rainfall-runoff relation is improved in the case of CCD estimated rainfall.

The present study has shown that METEOSAT data and the TAMSAT method are valuable supplementary tools in assessing rainfall and runoff characteristics in remote areas where rainfall data are scarce.

6.2 Recommendations

If convective clouds can be identified with TIR data, and if there is a direct connection between the observed radiance and precipitation sized drop, a reasonable estimate (not measured) of rain could be made. So systematic attention should be paid to the refinement of existing technique so that general biases, special local regional factors, etc. may be recognized and accommodated.

A combination of satellite data and rainfall data will still be necessary for a comparison, since the constant a_0 and a_1 depend on season.

It is better to test the method with more data (and a higher number of gauges) in the area to minimize the associated error in the estimation of areal rainfall. Averaging the data in space and time also improves the result; it is shown that the correlation for decadal values is not very much degraded as compared to daily data.

The method of merging rain gauges data and satellite data seems promising if it is applied to areas, which are flat and large in size.

Networks and methods for quality control, notably for point observation from surface station, should be designed to improve the reliability of the point data.

In collaboration with the TAMSAT group and other relevant organizations it is essential to improve the estimate by using the TAMSAT technique to test CCD20 threshold which is not done in this study.

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APPENDICES

APPENDIX A Station names and Locations

| Station name | Staton ID | longitude | Latitude |
|---------------------------------|-----------|-----------|----------|
| NAIVASHA D.O. | 9036002 | 36.43 | -0.72 |
| N. KINANGOP FOREST STATION | 9036025 | 36.63 | -0.58 |
| GILGIL RAILWAY STATION. | 9036034 | 36.33 | -0.50 |
| KIRITA FOREST STATION | 9036061 | 36.63 | -0.98 |
| MWEIGA ESTATE | 9036072 | 36.25 | -0.35 |
| TECHNOLOGY FARM, NAKURU | 9036076 | 36.02 | -0.30 |
| NAIVASHA VET.EXPT. STATION | 9036081 | 36.42 | -0.65 |
| KARAMENO SHOPPING CENTRE N/MORU | 9036085 | 36.77 | -0.13 |
| NAIVASHA MARULA ESTATE | 9036109 | 36.38 | -0.65 |
| ELEMENTAITA, SOYSAMBU ESTATE | 9036147 | 36.20 | -0.47 |
| SUBUKIA PYRETHRUM NURSERY | 9036151 | 36.17 | -0.03 |
| S.KINANGOP NJABINI F.T.C. | 9036152 | 36.65 | -0.72 |
| S. KINANGOP FOREST STATION | 9036164 | 36.68 | -0.72 |
| DUNDORI FOREST STATION | 9036243 | 36.23 | -0.25 |
| MENENGAI FOREST STATION | 9036252 | 36.08 | -0.25 |
| EASTERN RIFT SAWMILL LTD. | 9036257 | 36.70 | -0.92 |
| GATARE FOREST STATION | 9036259 | 36.77 | -0.72 |
| NAKURU METEOROLOGICAL STATION | 9036261 | 36.10 | -0.27 |
| OLARAGWAI FARM NAIVASHA | 9036262 | 36.45 | -0.65 |
| N. KINANGOP MAWINGO SCHEME | 9036264 | 36.52 | -0.50 |
| MUTUBIO GATE (A.N.PARK) | 9036272 | 36.63 | -0.48 |
| NAIVASHA W.D.D. | 9036281 | 36.45 | -0.73 |
| NGETHU WATER SUPPLY | 9036308 | 36.90 | -0.92 |
| KAMIRITHU FANCY FARM | 9036310 | 36.03 | -0.35 |
| CHAMATA GATE | 9036312 | 36.53 | -0.20 |
| CRESCENT ISLAND | 9036322 | 36.32 | -0.77 |
| KIANGANYE FARM ICHICHI | 9036323 | 36.82 | -0.70 |
| TUMAINI N.Y.S. CAMP | 9036336 | 36.28 | -0.27 |
| SURURU FOREST STATION | 9036337 | 36.03 | -0.58 |
| OLKARIA GEOTHERMAL STATION | 9036343 | 36.30 | -0.90 |

1. Available rainfall stations which have daily rainfall data for the year 1994 to1998, the arranged daily data can be found in the xls Caliberation on the daily file.

| Runoff station | Longitude | Latitude |
|----------------|-----------|----------|
| 2GB1 | 36.40 | -0.56 |
| 2GB4 | 36.48 | -0.28 |
| 2GB5 | 36.40 | -0.49 |
| 2GC4 | 36.42 | -0.48 |
| 2GC5 | 36.56 | -0.55 |
| 2GC7 | 36.49 | -0.57 |

2. Available runoff gauging stations in the Malewa catchment. Only 2GB1 has daily data for the year 1997 to 1998.

| March | ID | LON | LAT | нзх | НЗҮ | H3Z | I3X | I3Y | I3Z | J3X | J3Y | J3Z | кзх | КЗХ | K3Z | L3X | L3Y | L3Z |
|-------|---------|-------|-------|------|------|------|-----|------|------|------|------|-----|-----|-----|-----|-----|------|------|
| | 9036002 | 36.43 | -0.72 | 9.9 | 26 | 20.2 | 61 | 6 | 26.8 | 17.2 | 37.3 | 39 | 0 | 0 | 31 | 5.2 | 15 | 11.3 |
| | 9036025 | 36.63 | -0.58 | 12.4 | 7.6 | 65.1 | 101 | 66.9 | 23.5 | 14 | 15.7 | 42 | 0 | 4.2 | 49 | 19 | 24.1 | 8.6 |
| | 9036034 | 36.33 | -0.50 | 8.2 | 14 | 0 | 26 | 5.8 | 11.7 | 9.8 | 3.6 | 47 | 0 | 0 | 5.7 | 22 | 0 | 11.5 |
| | 9036061 | 36.63 | -0.98 | 34.2 | 13.1 | 74.2 | 111 | 7 | 19.5 | 8.5 | 26.2 | 50 | 0 | 0 | 46 | 52 | 25 | 60.6 |
| | 9036072 | 36.25 | -0.35 | 24.1 | 4.7 | 43.2 | 37 | 0 | 50.6 | 31.7 | 17.2 | 79 | 0 | 15 | 38 | 64 | 18.1 | 33.5 |
| | 9036076 | 36.02 | -0.30 | 23.3 | 6.1 | 49.2 | 58 | 5.3 | 29.6 | 0 | 8.8 | 45 | 0 | 0 | 15 | 0 | 2 | 61.3 |
| | 9036081 | 36.42 | -0.65 | 35.9 | 16.7 | 20 | 104 | 5 | 13.2 | 6.3 | 8.2 | 35 | 10 | 0 | 16 | 4.8 | 9.6 | 1 |
| | 9036085 | 36.77 | -0.13 | 8 | 26.7 | 53.1 | 31 | 0 | 20.6 | 13 | 9 | 39 | 5.5 | 0 | 25 | 73 | 14 | 46 |
| | 9036109 | 36.38 | -0.65 | 15.5 | 14.5 | 41.8 | 89 | 0 | 22.1 | 7.4 | 15.3 | 43 | 0.4 | 0 | 8.1 | 31 | 0 | 25 |
| | 9036147 | 36.20 | -0.47 | 0 | 5.6 | 9 | 63 | 13.3 | 10.2 | 15.2 | 0 | 12 | 0 | 0 | 11 | 28 | 0 | 5.2 |
| | 9036151 | 36.17 | -0.03 | 5.5 | 4.2 | 13.8 | 73 | 19 | 0 | 2.5 | 6.3 | 48 | 0 | 0 | 0 | 11 | 0 | 0 |
| | 9036152 | 36.65 | -0.72 | 69.7 | 27.2 | 76.7 | 120 | 28.7 | 19.1 | 9.6 | 13.5 | 108 | 0 | 0 | 74 | 16 | 33 | 18.6 |
| | 9036164 | 36.68 | -0.72 | -99 | -99 | -99 | -99 | -99 | -99 | 6.1 | 13 | 50 | 0 | 0 | 167 | 1 | 108 | 22 |
| | 9036243 | 36.23 | -0.25 | -99 | -99 | -99 | 45 | 26.7 | 10.3 | 4 | 18.8 | 47 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 9036252 | 36.08 | -0.25 | 17.5 | 10.1 | 53.7 | 68 | 16 | 21.6 | 4 | 10 | 54 | 0 | 0 | 26 | 50 | 0 | 8.5 |
| | 9036257 | 36.70 | -0.92 | 11.1 | 5.9 | 75.6 | 91 | 26.7 | 17.1 | 9.3 | 19.5 | 86 | 0 | 0 | 89 | 0 | 7 | 19 |
| | 9036259 | 36.77 | -0.72 | 19.6 | 28.7 | 87.8 | 126 | 1.5 | 50 | 29 | 36.7 | 86 | 0 | 0 | 127 | 55 | 11.3 | 137 |
| | 9036261 | 36.10 | -0.27 | 22.9 | 9.3 | 41.7 | 64 | 14.5 | 24.5 | 5.9 | 10.3 | 54 | 0 | 0 | 22 | 36 | 0.8 | 15.5 |
| | 9036262 | | -0.65 | | 8.1 | 13.1 | 56 | 1.4 | 12.1 | 3.5 | 10.2 | 28 | 0 | 0 | 15 | 18 | 4.3 | 6.2 |
| | 9036264 | 36.52 | -0.50 | 23.1 | 12.2 | 22.4 | 55 | 5.3 | 10.8 | 5 | 11 | 25 | 0 | 0 | 23 | 13 | 1.5 | 0.3 |
| | 9036272 | 36.63 | -0.48 | 24.7 | 14.8 | 75.5 | 74 | 3 | 91 | 0.8 | 27.4 | 144 | 0 | 9 | 92 | 28 | 19 | 55 |
| | 9036281 | | -0.73 | 0 | | 1.9 | 70 | 8.3 | 32.5 | | 34.6 | 40 | 0 | 0 | 51 | 13 | 13.6 | |
| | 9036308 | 36.90 | -0.92 | 3.5 | 5.2 | 47.8 | 93 | 2.6 | 20.2 | 7 | 42.3 | 106 | 0 | 0 | 25 | 96 | 51.6 | 96.2 |
| | 9036310 | | -0.35 | 6 | | 61.9 | | 16.9 | | 11.8 | 9.5 | 68 | 0 | 0 | 7.5 | 34 | 0 | 10.2 |
| | 9036312 | | -0.20 | 0 | 19.6 | 11.3 | 0 | 0 | 20.1 | 9 | 1.0 | 24 | 2 | 3 | - | 13 | 6.2 | 12.6 |
| | 9036322 | | -0.77 | | 7.7 | 17.4 | 65 | 0 | 24.6 | | 37.1 | 23 | 2.5 | 0 | 47 | 3.6 | 14.7 | 7.7 |
| | 9036323 | | -0.70 | 6.5 | | 52.9 | 0 | 114 | | 18.2 | | 67 | 0 | 0 | 88 | 77 | 3.5 | - |
| | 9036336 | | -0.27 | 5 | | 25.4 | -99 | -99 | -99 | | 31.4 | 103 | 0 | 0 | | 41 | 1 | 4.5 |
| | 9036337 | 36.03 | -0.58 | 0 | 33 | 53 | 35 | 16 | 19.5 | 32.9 | - | 55 | 0 | 0 | 18 | 33 | 9 | 9 |
| | 9036343 | 36.49 | -0.52 | 16.9 | 9 | 57.2 | 71 | 24.2 | 11.1 | 0.9 | 35.2 | 52 | 2.2 | 0 | 13 | 29 | 0 | 28.9 |

APPENDIX B Arranged decadal rainfall data

| Annil | TD | LON | τλπ | H4X | 11432 | H4Z | TAV | TAV | T 4 17 | J4X | TAV | T477 | VAV | TZ A XZ | 1247 | TAV | L4Y | L4Z |
|-------|--|---|---|--|--|---|---|--|--|---|---|--|---|---|--|--|--|---|
| April | 9036002 | 36.43 | LAT -0.72 | | H4Y 12.3 | н42 76.6 | I4X 7.7 | I4Y 32.5 | I4Z | - | J4Y 12 | J4Z 0 | K4X 78 | K4Y 13 | K4Z 60 | L4X 22 | 141 36.6 | 15.8 |
| | 9036002 | | -0.58 | 34.7 42.3 | | 126 | 15 | | 67.2 | 44.2 | 12 | 6.8 | 121 | 45 | 105 | 162 | 47.8 | 15.6 |
| | 9036025 | 36.63 | -0.50 | 28.8 | 31.8 6.5 | 89.1 | 21 | 0 6.8 | 38.3 46.9 | 44.2 | 6.9 | 0.0 | 44 | 45 27 | 63 | 37 | 34.2 | 29.9 |
| | 9036061 | 36.63 | -0.98 | 42.7 | 108 | 155 | 99 | | 79.6 | 73.8 | 28 | 13 | 108 | 105 | 178 | 119 | 74.7 | 104 |
| | 9036072 | 36.25 | -0.35 | | 21.8 | 111 | 15 | 7.5 | 53.4 | 6.7 | 4.7 | 21 | 46 | 31 | 95 | 44 | 42.3 | 43.6 |
| | 9036072 | 36.02 | -0.30 | 20.4 | 18.7 | 70.6 | 17 | 3.5 | 37.6 | | | 10 | 6.4 | 11 | 21 | 29 | 78 | 44.8 |
| | 9036081 | 36.42 | -0.65 | 9 | 26.4 | 130 | 26 | 8.6 | 3.7 | 21.2 | 3.6 | 14 | 68 | 44 | 95 | 25 | 17.9 | 4.7 |
| | 9036085 | 36.77 | -0.13 | _ | 34.6 | 63.7 | 20 | 3 | 28 | 41 | 0.5 | 0 | 99 | 14 | 61 | 39 | 33.9 | -1.7 |
| | 9036109 | 36.38 | -0.65 | 26.9 | 33 | 87.7 | 8.4 | 8.8 | 55.9 | 9 | 2.4 | 0 | 70 | 38 | 94 | 48 | 46.5 | 57.4 |
| | 9036147 | 36.20 | -0.47 | 7.2 | 2.8 | 81.9 | 10 | 6.4 | 54.9 | 12 | 3.1 | 3.2 | 53 | 37 | 75 | 31 | 27.9 | 63.3 |
| | 9036151 | 36.17 | -0.03 | 0 | 35.2 | 181 | 12 | 0.1 | 152.9 | -99 | -99 | -99 | 201 | 10 | 160 | 30 | 4.5 | 2 |
| | 9036152 | | | 77.3 | 48.3 | 121 | 24 | 21 | 11.5 | | | 8.7 | 179 | 83 | 186 | 110 | 60.3 | 28.8 |
| | 9036164 | 36.68 | -0.72 | -99 | -99 | -99 | 18 | 26.4 | 38.8 | -99 | -99 | -99 | 149 | 82 | 176 | 163 | 84 | 31.3 |
| | 9036243 | 36.23 | -0.25 | 0 | 9 | 91.5 | 30 | 20.2 | 102.4 | 9.6 | 0 | 0 | 85 | 40 | 187 | 0 | 0 | 28.7 |
| | 9036252 | 36.08 | -0.25 | 3.9 | 18.5 | 90.2 | 20 | 8.5 | 82.4 | 15.2 | 12.8 | 28 | 80 | 64 | 80 | 23 | 48.6 | 43.5 |
| | 9036257 | 36.70 | -0.92 | 82 | 39.2 | 83.4 | 7.3 | 16.7 | 84.6 | 33.2 | 8.5 | 1.2 | 168 | 51 | 90 | 10 | 9 | 10 |
| | 9036259 | 36.77 | -0.72 | 112 | 126 | 322 | 162 | 52.9 | 127.8 | 210 | 37.1 | 55 | 213 | 161 | 305 | 179 | 165 | 97.4 |
| | 9036261 | 36.10 | -0.27 | 13.2 | 12.1 | 89.7 | 16 | 9.5 | 45.6 | 14.7 | 25.3 | 6 | 85 | 56 | 66 | 18 | 52.8 | 19.7 |
| | 9036262 | 36.45 | -0.65 | 18 | 12.5 | 106 | 12 | 2 | 31.6 | 14.9 | 0 | 6 | 62 | 64 | 41 | 31 | 43.5 | 3 |
| | 9036264 | 36.52 | -0.50 | 50.9 | 25.9 | 143 | 58 | 0 | 37.7 | 7.5 | 0 | 23 | 99 | 29 | 74 | 38 | 78.3 | 53 |
| | 9036272 | 36.63 | -0.48 | 51.5 | 34.2 | 93.6 | 54 | 18.9 | 84.1 | 67.5 | 7.7 | 9.5 | 172 | 42 | 99 | 158 | 60 | 47 |
| | 9036281 | 36.45 | -0.73 | 21.1 | 17.8 | 47.9 | 2.4 | 36.8 | 52.3 | 50.1 | 7.1 | 0 | 103 | 14 | 61 | 35 | 24.3 | 20.8 |
| | 9036308 | 36.90 | -0.92 | 104 | 161 | 181 | 110 | 38.9 | 35.8 | 86.7 | 112 | 15 | 180 | 189 | 200 | 150 | 134 | 177 |
| | 9036310 | 36.03 | -0.35 | 9.9 | 9.5 | 90.1 | 17 | 3 | 25.7 | 16.8 | 16.7 | 6.3 | 80 | 33 | 110 | 38 | 50.8 | 39.8 |
| | 9036312 | 36.53 | -0.20 | 10.3 | 8.1 | 103 | 11 | 12.9 | 38 | 3.8 | 5 | 10 | 25 | 94 | 263 | 43 | 29.7 | 4.7 |
| | 9036322 | 36.32 | -0.77 | 17.8 | 22.6 | 46.3 | 1.5 | 22.8 | 40.4 | 36.8 | 12.7 | 0 | 72 | 15 | 62 | 28 | 12.2 | 19.1 |
| | 9036323 | 36.82 | -0.70 | 111 | 134 | 253 | 96 | | 202 | 172 | 28.9 | 39 | 143 | 153 | 358 | 157 | 179 | 97.5 |
| | 9036336 | 36.28 | -0.27 | 2.4 | 19.5 | 102 | -99 | -99 | -99 | | 8.4 | 33 | 29 | 31 | 128 | 36 | 49.1 | 114 |
| | 9036337 | 36.03 | -0.58 | 25 | 38 | 77.5 | 37 | 7 | 119.5 | | 9.5 | 0 | 101 | 24 | 63 | 51 | 45.5 | 28.5 |
| | 9036343 | 36.49 | -0.52 | -99 | -99 | -99 | 68 | 9.3 | 70.1 | 28.6 | 1.7 | 0 | 115 | 27 | 55 | 13 | 75.9 | 0 |
| 36 | TD | 1 011 | | ** ** | ** ** | ** * * | T F W | | | | | | | | | T E 17 | | |
| May | ID | LON | LAT | H5X | H5Y | H5Z | 15X | 15Y | I5Z | J5X | J5Y | J5Z | ĸ5x | К5Ү | K5Z | | L5Y | L5Z |
| May | 9036002 | 36.43 | -0.72 | 13.9 | 8.2 | 37.9 | 52 | 15Y 21.8 | 152 6.3 | J5X 5.1 | J5Y 16.8 | J5Z 18 | K5X 5.3 | K5Y 35 | K5Z | 44 | 8.3 | 41.9 |
| Мау | 9036002 9036025 | 36.43 36.63 | -0.72 -0.58 | 13.9 40.2 | 8.2 17.7 | 37.9 138 | 52 81 | I5Y 21.8 19.2 | 152 6.3 10 | J5X 5.1 20.5 | J5Y 16.8 26.8 | J5Z 18 13 | K5X 5.3 28 | K5Y 35 1.6 | K5Z 0 | 44 138 | 8.3 63.3 | 41.9 77.2 |
| Мау | 9036002 9036025 9036034 | 36.43 36.63 36.33 | -0.72 -0.58 -0.50 | 13.9 40.2 22.5 | 8.2 17.7 18.2 | 37.9 138 25.3 | 52 81 13 | 15Y 21.8 19.2 14.9 | 15Z 6.3 10 0 | J5X 5.1 20.5 14.1 | J5Y 16.8 26.8 30.7 | J5Z 18 13 5.3 | K5X 5.3 28 23 | K5Y 35 1.6 0 | K5Z 0 0 3.8 | 44 138 169 | 8.3 63.3 148 | 41.9 77.2 45 |
| Мау | 9036002 9036025 9036034 9036061 | 36.43 36.63 36.33 36.63 | -0.72 -0.58 | 13.9 40.2 22.5 145 | 8.2 17.7 18.2 88 | 37.9 138 | 52 81 | 15Y 21.8 19.2 14.9 63.1 | 152 6.3 10 0 39.8 | J5X 5.1 20.5 14.1 25.9 | J5Y 16.8 26.8 30.7 50.7 | J5Z 18 13 5.3 77 | K5X 5.3 28 23 43 | K5Y 35 1.6 0 70 | K5Z 0 | 44 138 169 146 | 8.3 63.3 148 60.8 | 41.9 77.2 45 57.4 |
| May | 9036002 9036025 9036034 9036061 9036072 | 36.43 36.63 36.33 36.63 36.25 | -0.72 -0.58 -0.50 -0.98 -0.35 | 13.9 40.2 22.5 145 65.8 | 8.2 17.7 18.2 88 93.5 | 37.9 138 25.3 69.8 0 | 52 81 13 63 40 | 15 Y 21.8 19.2 14.9 63.1 116 | 152 6.3 10 0 39.8 17.7 | J5X 5.1 20.5 14.1 25.9 9.6 | J5Y 16.8 26.8 30.7 50.7 78.2 | J5Z 18 13 5.3 77 21 | K5X 5.3 28 23 43 61 | K5Y 35 1.6 0 70 25 | K5Z 0 3.8 2 25 | 44 138 169 146 174 | 8.3 63.3 148 60.8 49.3 | 41.9 77.2 45 57.4 19.1 |
| May | 9036002 9036025 9036034 9036061 | 36.43 36.63 36.33 36.63 | -0.72 -0.58 -0.50 -0.98 | 13.9 40.2 22.5 145 | 8.2 17.7 18.2 88 | 37.9 138 25.3 69.8 | 52 81 13 63 | 15Y 21.8 19.2 14.9 63.1 | 152 6.3 10 0 39.8 | J5X 5.1 20.5 14.1 25.9 9.6 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 | J5Z 18 13 5.3 77 | K5X 5.3 28 23 43 | K5Y 35 1.6 0 70 | K5Z 0 3.8 2 | 44 138 169 146 | 8.3 63.3 148 60.8 | 41.9 77.2 45 57.4 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 | 36.43 36.63 36.33 36.63 36.25 36.02 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 | 13.9 40.2 22.5 145 65.8 -99 | 8.2 17.7 18.2 88 93.5 -99 | 37.9 138 25.3 69.8 0 -99 | 52 81 13 63 40 21 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 | 152 6.3 10 0 39.8 17.7 26.5 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 | J5Z 18 13 5.3 77 21 39 | K5X 5.3 28 23 43 61 13 | K5Y 35 1.6 0 70 25 8.3 | K5Z 0 3.8 2 25 19 | 44 138 169 146 174 115 | 8.3 63.3 148 60.8 49.3 86.8 | 41.9 77.2 45 57.4 19.1 5.8 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 | 13.9 40.2 22.5 145 65.8 -99 47 | 8.2 17.7 18.2 88 93.5 -99 4.6 | 37.9 138 25.3 69.8 0 -99 18.8 | 52 81 13 63 40 21 21 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 | 152 6.3 10 0 39.8 17.7 26.5 23.6 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 | J5Z 18 13 5.3 77 21 39 5.9 | K5X 5.3 28 23 43 61 13 9.9 | K5Y 35 1.6 0 70 25 8.3 6.5 | K5Z 0 3.8 25 19 0 | 44 138 169 146 174 115 61 | 8.3 63.3 148 60.8 49.3 86.8 41.6 | 41.9 77.2 45 57.4 19.1 5.8 44.1 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 | 13.9 40.2 22.5 145 65.8 -99 47 8.4 -99 | 8.2 17.7 18.2 88 93.5 -99 4.6 1.6 -99 | 37.9 138 25.3 69.8 0 -99 18.8 0.3 | 52 81 13 63 40 21 21 30 35 | 15 Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 | 152 6.3 10 0 39.8 17.7 26.5 23.6 2 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 0 3.9 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 | J5Z 18 13 5.3 77 21 39 5.9 5.9 | K5X 5.3 28 23 43 61 13 9.9 35 | K5Y 35 1.6 0 70 25 8.3 6.5 31 | K5Z 0 3.8 2 25 19 0 0 | 44 138 169 146 174 115 61 109 | 8.3 63.3 148 60.8 49.3 86.8 41.6 36 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 | 13.9 40.2 22.5 145 65.8 -99 47 8.4 -99 51.5 | 8.2 17.7 18.2 88 93.5 -99 4.6 1.6 -99 0 | 37.9 138 25.3 69.8 0 -99 18.8 0.3 -99 41.5 | 52 81 13 63 40 21 21 30 35 5 | 15 Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 | 152 6.3 10 39.8 17.7 26.5 23.6 23.4 20.5 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 0 3.9 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 | J5Z 18 13 5.3 77 21 39 5.9 5.9 5.9 6.6 | K5X 5.3 28 23 43 61 13 9.9 35 7.8 | K5Y 35 1.6 0 70 25 8.3 6.5 31 0 | K5Z 0 3.8 2 25 19 0 0 0 | 44 138 169 146 174 115 61 109 64 88 | 8.3 63.3 148 60.8 49.3 86.8 41.6 63 17.3 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 | 36.43 36.63 36.33 36.25 36.02 36.42 36.77 36.38 36.20 36.17 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 | 13.9 40.2 22.5 145 65.8 -99 47 8.4 -99 51.5 47.9 | 8.2 17.7 18.2 88 93.5 -99 4.6 1.6 -99 0 85.5 | 37.9 138 25.3 69.8 0 -99 18.8 0.3 -99 41.5 | 52 81 13 63 40 21 21 30 35 5 91 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 | 152 6.3 10 39.8 17.7 26.5 23.6 2 32.4 20.5 18.3 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 0 3.9 8.5 13.9 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 | J5Z 18 13 5.3 77 21 39 5.9 5.9 5.6 6.6 12 | K5X 5.3 28 23 43 61 13 9.9 35 7.8 17 | K5Y 35 1.6 0 70 25 8.3 6.5 31 0 11 | K5 Z 0 3.8 2 25 19 0 0 0 0 0 | 44 138 169 146 174 115 61 109 64 88 104 | 8.3 63.3 148 60.8 49.3 86.8 41.6 36 63 17.3 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 | 13.9 40.2 22.5 145 65.8 -99 47 8.4 -99 51.5 47.9 69 | 8.2 17.7 18.2 88 93.5 -99 4.6 1.6 -99 0 85.5 64.3 | 37.9 138 25.3 69.8 0 -99 18.8 0.3 -99 41.5 22.4 | 52 81 13 63 40 21 21 30 35 5 91 91 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 | 152 6.3 10 39.8 17.7 26.5 23.6 23.4 20.5 18.3 33.4 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 0 3.9 8.5 13.9 27.5 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 | J5Z 18 13 5.3 77 21 39 5.9 5.9 5.6 6.6 12 63 39 | K5X 5.3 28 23 43 61 13 9.9 35 7.8 17 24 | K5Y 35 1.6 0 25 8.3 6.5 31 0 11 4.1 19 | K5 Z 0 3.8 2 25 19 0 0 0 0 0 | 44 138 169 146 174 115 61 109 64 88 104 173 | 8.3 63.3 148 60.8 49.3 86.8 41.6 63 17.3 41.5 58.1 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 | 13.9 40.2 22.5 145 65.8 -99 47 8.4 -99 51.5 47.9 69 -99 43.8 | 8.2 17.7 18.2 88 93.5 -99 4.6 1.6 -99 0 85.5 64.3 -99 68.8 | 37.9 138 25.3 69.8 0 -99 18.8 0.3 -99 41.5 22.4 72.5 -99 24.1 | 52 81 13 63 40 21 21 30 35 5 91 91 149 26 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 27 147 25.5 | 152 6.3 10 39.8 17.7 26.5 23.6 2 32.4 20.5 18.3 33.4 48.2 62 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 0 3.9 8.5 13.9 27.5 -99 31.7 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 65.5 -99 63.5 | J5Z 18 13 5.3 77 21 39 5.9 5 6.6 12 63 39 -99 60 | K5X 5.3 28 23 43 61 13 9.9 35 7.8 17 24 56 -99 38 | K5Y 35 1.6 0 25 8.3 6.5 31 0 11 4.1 19 -99 0 | K5 Z 0 3.8 2 25 19 0 0 0 0 4.5 | 44 138 169 146 174 115 61 109 64 88 104 173 165 | 8.3 63.3 148 60.8 49.3 86.8 41.6 63 17.3 41.5 58.1 28 40.6 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 34.3 41.7 38.8 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036085 9036109 9036147 9036151 9036152 9036164 9036243 9036252 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 | 13.9 40.2 22.5 145 65.8 -99 47 8.4 -99 51.5 47.9 69 -99 43.8 39.2 | 8.2 17.7 18.2 88 93.5 -99 4.6 1.6 -99 0 85.5 64.3 -99 68.8 0.5 | 37.9 138 25.3 69.8 0 -99 18.8 0.3 -99 41.5 22.4 72.5 -99 24.1 44.1 | 52 81 13 63 40 21 21 30 35 5 91 91 149 26 24 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 27 147 25.5 67.7 | 152 6.3 10 39.8 17.7 26.5 23.6 23.4 20.5 18.3 33.4 48.2 62 49.4 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 0 3.9 8.5 13.9 27.5 -99 31.7 1.5 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 65.5 -99 63.5 24.3 | J5Z 18 13 5.3 77 21 39 5.9 5.9 6.6 12 63 39 -99 60 45 | K5x 5.3 28 23 43 61 13 9.9 355 7.8 17 24 56 -99 38 23 | K5Y 35 1.6 0 70 25 8.3 6.5 31 0 11 4.1 19 -999 0 16 | K52 0 3.8 2 25 19 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 44 138 169 146 174 115 61 109 64 88 104 173 165 183 88 | 8.3 63.3 148 60.8 49.3 86.8 41.6 63 17.3 41.5 58.1 28 40.6 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 34.3 41.7 38.8 |
| May | 9036002 9036025 9036034 9036072 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 9036252 9036257 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.25 -0.92 | 13.9 40.2 22.5 145 65.8 -99 47 8.4 -99 51.5 47.9 69 -99 43.8 39.2 44.8 | 8.2 17.7 18.2 88 93.5 -99 4.6 1.6 -99 0 85.5 64.3 -99 68.8 0.5 64 | 37.9 138 25.3 69.8 0 -99 18.8 0.3 -99 41.5 22.4 72.5 -99 24.1 44.1 21.5 | 52 81 13 63 40 21 21 30 35 5 91 91 149 26 24 58 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 27 147 25.5 67.7 49.6 | I5Z 6.3 0 39.8 17.7 26.5 23.6 22.4 20.5 18.3 33.4 48.2 62 49.4 47.8 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 0 3.9 8.5 13.9 27.5 -99 31.7 1.5 -99 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 65.5 -99 63.5 24.3 -99 | J5Z 18 13 5.3 777 211 39 5.9 5.9 6.6 12 63 39 -99 60 45 -99 | K5X 5.3 28 23 43 61 13 9.9 355 7.8 17 24 56 -99 38 23 37 | K5Y 35 1.6 0 70 25 8.3 6.5 31 0 11 4.1 19 -999 0 16 16 | K5Z 0 3.8 2 25 19 0 16 0 | 44 138 169 146 174 115 61 109 64 88 104 173 165 183 88 88 80 | 8.3 63.3 148 60.8 49.3 86.8 41.6 63 17.3 41.5 58.1 28 40.6 87.5 26 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 34.3 41.7 38.8 0 8 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 9036252 9036257 9036259 | 36.43 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.92 -0.72 | 13.9 40.2 22.5 145 65.8 -99 47 8.4 -99 51.5 47.9 69 -99 43.8 39.2 44.8 201 | 8.2 17.7 18.2 88 93.5 -99 4.6 1.6 -99 0 85.5 64.3 -99 68.8 0.5 64 208 | 37.9 138 25.3 69.8 0 -99 18.8 0.3 -99 41.5 22.4 72.5 -99 24.1 44.1 21.5 59.3 | 52 81 13 63 40 21 21 30 35 5 91 91 149 26 24 58 206 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 27 147 25.5 67.7 49.6 115 | I5Z 6.3 10 0 39.8 17.7 26.5 23.6 22.4 20.5 18.3 33.4 48.2 62 49.4 89.7 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 0 3.9 8.5 13.9 27.5 -99 31.7 1.5 -99 77.2 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 65.5 -99 63.5 24.3 -99 183 | J5Z 18 13 5.3 777 211 39 5.9 5.9 6.6 12 63 39 -99 60 45 -99 91 | K5X 5.3 28 23 43 61 13 9.9 35 7.8 17 24 56 -99 38 23 37 218 | K5Y 35 1.6 0 70 25 8.3 6.5 31 0 11 4.1 19 -99 0 16 92 | K5Z 0 3.8 2 19 0 3.5 | 44 138 169 146 174 115 61 109 64 88 104 173 165 183 88 88 80 253 | 8.3 63.3 148 60.8 49.3 86.8 41.6 63 17.3 41.5 58.1 28 40.6 87.5 26 58.8 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 34.3 41.7 38.8 0 0 8 8 113 |
| May | 9036002 9036025 9036034 9036072 9036076 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 9036252 9036257 9036259 9036261 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.92 -0.72 -0.72 | 13.9 40.2 22.5 145 65.8 -99 47 8.4 -99 51.5 47.9 69 -99 43.8 39.2 44.8 201 50.7 | 8.2 17.7 18.2 88 93.5 -99 4.6 1.6 -99 0 85.5 64.3 -99 68.8 0.5 64.3 -99 68.8 0.5 64 | 37.9 138 25.3 69.8 0 -99 18.8 0.3 -99 41.5 22.4 72.5 -99 24.1 44.1 21.5 59.3 45.4 | 52 81 13 63 40 21 21 30 35 5 91 91 149 26 24 58 206 9.9 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 27 147 25.5 67.7 49.6 115 27.2 | 152 6.3 10 0 39.8 17.7 26.5 23.6 23.4 20.5 18.3 33.4 48.2 62 49.4 47.8 89.7 50.3 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 0 3.9 8.5 13.9 27.5 -999 31.7 1.5 -999 77.2 6.1 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 65.5 -99 63.5 24.3 -99 183 23.3 | J5Z 18 13 5.3 777 21 39 5.9 5.9 6.6 12 63 39 -99 60 45 -99 91 52 | K5X 5.3 28 23 43 61 13 9.9 35 7.8 17 24 56 -99 38 23 377 218 28 | K5Y 35 1.6 0 70 8.3 6.5 31 0 11 4.1 19 -999 0 16 92 12 | K5Z 0 3.8 2 19 0 3.5 1.5 | 444 1388 1699 1466 1744 1155 61 1099 64 109 64 1733 1655 1833 888 880 2533 91 | 8.3 63.3 148 60.8 49.3 86.8 41.6 63 17.3 41.5 58.1 28 40.6 87.5 28 40.6 87.5 28 84.6 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 34.3 41.7 38.8 0 8 113 11.9 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 9036252 9036257 9036259 9036261 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.45 | -0.72 -0.58 -0.50 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.92 -0.72 -0.72 -0.5 | 13.9 40.2 22.5 145 65.8 -99 47 8.4 -99 51.5 47.9 69 -99 43.8 39.2 44.8 201 50.7 25.8 | 8.2 17.7 18.2 88 93.5 -99 4.6 1.6 -99 0 85.5 64.3 -99 68.8 0.5 64.3 -99 68.8 0.5 64.3 -99 5.9 | $\begin{array}{c} 37.9\\ 138\\ 25.3\\ 69.8\\ 0\\ -99\\ 18.8\\ 0.3\\ -99\\ 41.5\\ 22.4\\ 72.5\\ -99\\ 24.1\\ 44.1\\ 21.5\\ 59.3\\ 45.4\\ 20.7 \end{array}$ | 52 81 13 40 21 30 35 5 91 149 26 24 58 206 9.9 32 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 27 147 25.5 67.7 49.6 115 27.2 20.8 | I5Z 6.3 10 0 39.8 17.7 26.5 23.6 22.4 20.5 18.3 33.4 48.2 62 49.4 89.7 50.3 6.4 | J5x 5.1 20.5 14.1 25.9 9.6 12.3 0.7 0 3.9 8.5 13.9 27.5 -999 31.7 1.5 -999 77.2 6.1 8.3 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 65.5 -99 63.5 24.3 -99 183 23.3 45.4 | J5Z 18 13 5.3 77 21 39 5.9 5.9 6.6 12 63 39 -99 60 45 -99 91 52 17 | K5X 5.3 28 23 43 61 13 9.9 35 7.8 17 24 56 -99 38 23 377 218 28 30 | K5Y 35 1.6 0 70 25 8.3 6.5 31 0 11 4.1 19 -99 0 16 92 12 10 | K5Z 0 3.8 2 19 0 16 0 35 15 0 | 444 1388 1699 1466 1744 1155 61 1099 64 888 808 104 1733 1655 1833 888 800 2533 911 63 | 8.3 63.3 148 60.8 49.3 86.8 41.6 36 63 17.3 41.5 58.1 28 40.6 87.5 28 87.5 28 84.6 52.4 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 34.3 41.7 38.8 0 8 113 11.9 65.7 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036243 9036252 9036257 9036259 9036261 9036264 | 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.77 36.10 36.45 36.52 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.92 -0.72 -0.72 -0.55 | $\begin{array}{c} 13.9\\ 40.2\\ 22.5\\ 145\\ 65.8\\ -99\\ 47\\ 8.4\\ -99\\ 51.5\\ 47.9\\ 69\\ -99\\ 43.8\\ 39.2\\ 44.8\\ 201\\ 50.7\\ 25.8\\ 94.5 \end{array}$ | 8.2 17.7 18.2 88 93.5 -99 4.6 1.6 -99 0 85.5 64.3 -99 68.8 0.5 64.3 -99 68.8 0.5 64.2 208 4.7 5.9 12.6 | 37.9 138 25.3 69.8 0 -99 18.8 0.3 -99 41.5 22.4 72.5 -99 24.1 44.1 21.5 59.3 45.4 20.7 35.8 | 52 81 13 63 40 21 30 35 5 91 91 149 26 24 58 206 9.9 32 37 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 27 147 25.5 67.7 49.6 115 27.2 20.8 32.3 | I5Z 6.3 10 0 39.8 17.7 26.5 23.6 22.4 20.5 18.3 33.4 48.2 62 49.4 89.7 50.3 6.4 24 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 3.9 8.5 13.9 27.5 -999 31.7 1.5 -999 77.2 6.1 8.3 35.1 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 65.5 -99 63.5 24.3 -99 183 23.3 45.4 71.2 | J5Z 18 13 5.3 77 21 39 5.9 5.9 5.9 6.6 12 63 39 -99 60 45 -99 91 52 17 7.3 | K5X 5.3 28 23 43 61 13 9.9 35 7.8 17 24 56 -99 38 23 377 218 28 30 32 | K5Y 35 1.6 0 70 25 8.3 6.5 31 0 11 4.1 19 -99 0 16 92 12 10 0 | K5Z 0 3.8 2 19 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 16 0 35 15 0 10 | 444 1388 1699 1466 1744 1155 611 1099 644 1733 1655 1833 888 800 2533 911 633 117 | 8.3 63.3 148 60.8 49.3 86.8 41.6 36 63 17.3 41.5 58.1 28 40.6 87.5 26 58.8 84.6 52.4 80.4 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 34.3 41.7 38.8 0 8 113 11.9 65.7 62.2 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036252 9036257 9036259 9036261 9036264 9036272 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.45 36.52 36.63 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.92 -0.72 -0.72 -0.50 -0.50 -0.48 | $\begin{array}{c} 13.9\\ 40.2\\ 22.5\\ 145\\ 65.8\\ -99\\ 47\\ 8.4\\ -99\\ 51.5\\ 47.9\\ 69\\ -99\\ 43.8\\ 39.2\\ 44.8\\ 201\\ 50.7\\ 25.8\\ 94.5\\ 65.8 \end{array}$ | 8.2 17.7 18.2 88 93.5 -99 4.6 1.6 -99 0 85.5 64.3 -99 68.8 0.5 64.4 208 4.7 5.9 12.6 38.6 | $\begin{array}{c} 37.9\\ 138\\ 25.3\\ 69.8\\ 0\\ -99\\ 18.8\\ 0.3\\ -99\\ 41.5\\ 22.4\\ 72.5\\ -99\\ 24.1\\ 44.1\\ 21.5\\ 59.3\\ 45.4\\ 20.7\\ 35.8\\ 51.4 \end{array}$ | 52 81 13 40 21 21 30 35 5 91 149 26 24 58 206 9.9 32 37 96 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 27 147 25.5 67.7 49.6 115 27.2 20.8 32.3 49.7 | I5Z 6.3 10 0 39.8 17.7 26.5 23.6 22.32.4 20.5 18.3 33.4 48.2 62 49.4 750.3 6.4 24 14 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 3.9 8.5 13.9 27.5 -999 31.7 1.5 -999 77.2 6.1 8.3 35.1 -999 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 65.5 -99 63.5 24.3 -99 183 23.3 45.4 71.2 -99 | J5Z 18 13 5.3 77 21 39 5.9 5.9 5.9 6.6 12 63 39 -99 60 45 -99 91 52 17 7.3 -99 | K5X 5.3 28 23 43 61 39.9 35 7.8 17 24 56 -99 38 23 377 218 300 32 19 | K5Y 35 1.6 0 70 25 8.3 6.5 31 0 11 4.1 19 -99 0 16 92 12 10 0 19 | K5Z 0 3.8 2 19 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 16 0 35 15 0 10 5 | 444 1388 1699 1466 1744 1155 611 1099 644 1733 1655 1833 888 800 2533 911 633 1177 228 | 8.3 63.3 148 60.8 49.3 86.8 41.6 36 63 17.3 41.5 58.1 28 40.6 87.5 28 87.5 28 84.6 58.8 84.6 52.4 80.4 81 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 34.3 41.7 38.8 0 8 113 11.9 65.7 62.2 50 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036252 9036257 9036259 9036261 9036262 9036264 9036272 9036281 | 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.77 36.10 36.45 36.52 36.63 36.45 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.92 -0.72 -0.72 -0.50 -0.50 -0.48 -0.73 | $\begin{array}{c} 13.9\\ 40.2\\ 22.5\\ 145\\ 65.8\\ -99\\ 47\\ 8.4\\ -99\\ 51.5\\ 47.9\\ 69\\ -99\\ 43.8\\ 39.2\\ 44.8\\ 201\\ 50.7\\ 25.8\\ 94.5\\ 65.8\\ 10.1 \end{array}$ | $\begin{array}{c} 8.2\\ 17.7\\ 18.2\\ 88\\ 93.5\\ -99\\ 4.6\\ 1.6\\ -99\\ 0\\ 85.5\\ 64.3\\ -99\\ 68.8\\ 0.5\\ 64.3\\ -99\\ 68.8\\ 0.5\\ 64.3\\ -99\\ 12.6\\ 38.6\\ 9.7\\ \end{array}$ | $\begin{array}{c} 37.9\\ 138\\ 25.3\\ 69.8\\ 0\\ -99\\ 18.8\\ 0.3\\ -99\\ 41.5\\ 22.4\\ 72.5\\ -99\\ 24.1\\ 44.1\\ 21.5\\ 59.3\\ 45.4\\ 20.7\\ 35.8\\ 51.4\\ 50.6 \end{array}$ | 52 81 13 63 40 21 30 35 5 91 149 26 24 58 206 9.9 32 37 96 63 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 27 147 25.5 67.7 49.6 115 27.2 20.8 32.3 49.7 27.9 | 152 6.3 10 0 39.8 17.7 26.5 23.6 23.6 23.4 20.5 18.3 33.4 48.2 62 49.4 47.8 89.7 50.3 6.4 24 14 5.7 | J5x 5.1 20.5 14.1 25.9 9.6 12.3 0.7 3.9 8.5 13.9 27.5 -999 31.7 1.5 -999 77.2 6.1 8.3 35.1 -999 0 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 65.5 -99 63.5 24.3 -99 183 23.3 45.4 71.2 -99 15 | J5Z 18 13 5.3 77 21 39 5.9 5.9 5.9 6.6 12 6.3 39 -99 60 45 -99 91 52 17 7.3 -99 922 | K5X 5.3 28 23 43 61 13 9.9 35 7.8 17 24 56 -99 38 237 218 300 32 19 38 | K5Y 35 1.6 0 25 8.3 6.5 31 0 11 4.1 19 -99 0 16 92 12 10 19 4.9 | K5Z 0 3.8 2 19 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 16 0 3.5 15 0 10 5 0 | 444 1388 1699 1466 1744 1155 61 1099 644 109 644 1733 1655 1833 888 800 2533 91 633 117 2288 556 | 8.3 63.3 148 60.8 49.3 86.8 41.6 36 63 17.3 41.5 58.1 28 40.6 87.5 26 58.8 84.6 52.4 80.4 80.4 81 11.3 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 34.3 41.7 38.8 0 8 113 11.9 65.7 62.2 50 39.3 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036187 9036147 9036151 9036152 9036164 9036252 9036257 9036257 9036261 9036262 9036264 9036272 9036281 9036308 | 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.77 36.10 36.45 36.52 36.63 36.45 36.90 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.92 -0.72 -0.65 -0.50 -0.50 -0.48 -0.73 -0.92 | $\begin{array}{c} 13.9\\ 40.2\\ 22.5\\ 145\\ 65.8\\ -99\\ 47\\ 8.4\\ -99\\ 51.5\\ 47.9\\ 69\\ -99\\ 43.8\\ 39.2\\ 44.8\\ 201\\ 50.7\\ 25.8\\ 94.5\\ 65.8\\ 10.1\\ 55.7\\ \end{array}$ | $\begin{array}{c} 8.2\\ 17.7\\ 18.2\\ 88\\ 93.5\\ -99\\ 4.6\\ 1.6\\ -99\\ 0\\ 85.5\\ 64.3\\ -99\\ 68.8\\ 0.5\\ 64.3\\ -99\\ 68.8\\ 0.5\\ 64.3\\ -99\\ 12.6\\ 38.6\\ 9.7\\ 56.6\end{array}$ | $\begin{array}{c} 37.9\\ 138\\ 25.3\\ 69.8\\ 0\\ -99\\ 18.8\\ 0.3\\ -99\\ 41.5\\ 22.4\\ 72.5\\ -99\\ 24.1\\ 44.1\\ 21.5\\ 59.3\\ 45.4\\ 20.7\\ 35.8\\ 51.4\\ 50.6\\ 21.3\\ \end{array}$ | 52 81 13 40 21 21 30 35 5 91 149 26 24 24 58 206 9.9 32 37 96 63 64 | 15Y 21.8 19.2 14.9 63.1 29.6 7.7 20 5.4 18.2 18.4 27 147 25.5 67.7 49.6 115 27.2 20.8 32.3 49.7 27.9 90.3 | I5Z 6.3 10 0 39.8 17.7 26.5 23.6 22.32.4 20.5 18.3 33.4 48.2 62 49.4 750.3 6.4 24 14 5.7 28.5 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 3.9 8.5 13.9 27.5 -999 31.7 1.5 -999 31.7 1.5 -999 77.2 6.1 8.3 35.1 -999 0 59.8 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 65.5 -99 63.5 24.3 -99 183 23.3 45.4 71.2 -99 15 64.5 | J5Z 18 13 5.3 77 21 39 5.9 5.9 5.9 6.6 12 63 39 -99 60 45 -99 91 52 17 7.3 -99 22 68 | K5X 5.3 28 23 43 61 13 9.9 35 7.8 17 24 56 -99 38 237 218 300 32 19 38 67 | K5Y 35 1.6 0 25 8.3 6.5 31 0 11 4.1 19 -999 0 16 92 12 10 19 19 19 19 192 | K5Z 0 0 3.8 2 19 0 0 0 0 0 0 0 0 0 0 0 0 0 16 0 3.5 15 0 10 5 0 17 | 444 1388 1699 1466 1744 1155 61 1099 644 1039 165 1833 1655 1833 888 800 2533 91 633 117 2288 566 173 | 8.3 63.3 148 60.8 49.3 86.8 41.6 36 63 17.3 41.5 58.1 28 40.6 87.5 26 58.8 84.6 52.4 80.4 80.4 81 11.3 151 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 34.3 41.7 38.8 0 8 113 11.9 65.7 62.2 50 39.3 204 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036185 9036147 9036151 9036152 9036164 9036252 9036257 9036257 9036261 9036262 9036264 9036272 9036281 9036308 9036310 | 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.77 36.10 36.45 36.52 36.63 36.45 36.90 36.03 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.92 -0.72 -0.50 -0.50 -0.48 -0.73 -0.92 -0.73 -0.59 | $\begin{array}{c} 13.9\\ 40.2\\ 22.5\\ 145\\ 65.8\\ -99\\ 47\\ 8.4\\ -99\\ 51.5\\ 47.9\\ 69\\ -99\\ 43.8\\ 39.2\\ 44.8\\ 201\\ 50.7\\ 25.8\\ 94.5\\ 65.8\\ 10.1\\ 55.7\\ 12\end{array}$ | $\begin{array}{c} 8.2\\ 17.7\\ 18.2\\ 88\\ 93.5\\ -99\\ 4.6\\ 1.6\\ -99\\ 0\\ 85.5\\ 64.3\\ -99\\ 68.8\\ 0.5\\ 64.3\\ -99\\ 68.8\\ 0.5\\ 64.3\\ -99\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 56.6\\ 27.5\\ \end{array}$ | $\begin{array}{c} 37.9\\ 138\\ 25.3\\ 69.8\\ 0\\ -99\\ 18.8\\ 0.3\\ -99\\ 41.5\\ 22.4\\ 72.5\\ -99\\ 24.1\\ 44.1\\ 21.5\\ 59.3\\ 45.4\\ 20.7\\ 35.8\\ 51.4\\ 50.6\\ 21.3\\ 40\\ \end{array}$ | 52 81 13 40 21 21 30 35 5 91 149 26 24 24 58 206 9.9 32 37 96 63 64 9.8 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 27 147 25.5 67.7 49.6 115 27.2 20.8 32.3 49.7 27.9 90.3 16 | I5Z 6.3 10 0 39.8 17.7 26.5 23.6 23.4 20.5 18.3 33.4 48.2 62 49.4 47.8 89.7 50.3 6.4 24 14 5.7 28.5 46 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 0 3.9 8.5 13.9 27.5 -99 31.7 1.5 -99 77.2 6.1 8.3 35.1 -99 0 59.8 17.5 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 65.5 -99 63.5 24.3 -99 183 23.3 45.4 71.2 -99 15 64.5 28.4 | J5Z 18 13 5.3 77 21 39 5.9 5.9 5.9 6.6 12 63 39 -99 60 45 -99 91 52 17 7.3 -99 22 68 29 | K5X 5.3 28 23 43 61 35 7.8 7.8 64 9.9 355 7.8 224 56 -999 38 237 218 300 322 19 38 67 20 | K5Y 35 1.6 0 25 8.3 6.5 31 0 11 4.1 19 -99 0 16 92 12 10 19 192 26 | K5Z 0 3.8 25 19 0 0 0 0 0 0 0 0 0 0 0 0 0 0 16 0 35 15 0 10 5 0 177 12 | 444 1388 1699 1466 1744 1155 61 1099 644 1039 165 1833 1655 1833 888 800 2533 91 633 117 2288 566 173 74 | 8.3 63.3 148 60.8 49.3 86.8 41.6 36 63 17.3 41.5 58.1 28 40.6 87.5 26 58.8 84.6 52.4 80.4 80.4 81 11.3 151 87 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 34.3 41.7 38.8 0 8 113 11.9 65.7 62.2 50 39.3 204 6.2 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036081 9036189 9036147 9036151 9036152 9036164 9036252 9036257 9036257 9036261 9036262 9036264 9036272 9036281 9036308 9036310 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.77 36.10 36.45 36.52 36.63 36.45 36.90 36.03 36.53 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.92 -0.72 -0.27 -0.65 -0.50 -0.48 -0.50 -0.48 -0.73 -0.92 -0.35 -0.20 | $\begin{array}{c} 13.9\\ 40.2\\ 22.5\\ 145\\ 65.8\\ -99\\ 47\\ 8.4\\ -99\\ 51.5\\ 47.9\\ 69\\ -99\\ 43.8\\ 39.2\\ 44.8\\ 201\\ 50.7\\ 25.8\\ 94.5\\ 65.8\\ 10.1\\ 55.7\\ 12\\ 25.9\end{array}$ | $\begin{array}{c} 8.2\\ 17.7\\ 18.2\\ 88\\ 93.5\\ -99\\ 4.6\\ 1.6\\ -99\\ 0\\ 85.5\\ 64.3\\ -99\\ 68.8\\ 0.5\\ 64.3\\ -99\\ 68.8\\ 0.5\\ 64.3\\ -99\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 56.6\\ 27.5\\ 57.6\end{array}$ | $\begin{array}{c} 37.9\\ 138\\ 25.3\\ 69.8\\ 0\\ -99\\ 18.8\\ 0.3\\ -99\\ 41.5\\ 22.4\\ 72.5\\ -99\\ 24.1\\ 44.1\\ 21.5\\ 59.3\\ 45.4\\ 20.7\\ 35.8\\ 51.4\\ 50.6\\ 21.3\\ 40\\ 32.6\\ \end{array}$ | 52 81 13 40 21 21 30 35 5 91 149 26 24 24 58 206 9.9 32 37 96 63 64 9.8 40 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 27 147 25.5 67.7 49.6 115 27.2 20.8 32.3 49.7 27.9 90.3 16 40 | I5Z 6.3 10 39.8 17.7 26.5 23.6 22.3 32.4 20.5 18.3 33.4 48.2 62 49.4 750.3 6.4 24 14 5.7 28.5 46 10.5 | J5x 5.1 20.5 14.1 25.9 9.6 12.3 0.7 3.9 8.5 13.9 27.5 -999 31.7 1.5 -999 77.2 6.1 8.3 35.1 -999 0 59.8 17.5 2.5 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 65.5 -99 63.5 24.3 -99 183 23.3 45.4 71.2 -99 15 64.5 28.4 72 | J5Z 18 13 5.3 77 21 39 5.9 5.9 5.9 6.6 12 6.3 39 -99 60 45 -99 91 52 17 7.3 -99 22 68 29 11 | K5X 5.3 28 23 43 61 13 9.9 35 7.8 17 24 56 -99 38 237 218 300 32 19 38 67 20 71 | K5Y 35 1.6 0 25 8.3 6.5 31 0 11 4.1 19 -999 0 16 92 10 19 192 26 17 | K5Z 0 3.8 25 19 0 0 0 0 0 0 0 0 0 0 0 0 16 0 35 15 0 10 5 0 177 12 12 | 444 1388 1699 1466 1744 1155 61 1099 644 1733 1655 1833 1655 1833 888 800 2533 911 633 1177 2288 566 1733 744 169 | 8.3 63.3 148 60.8 49.3 86.8 41.6 36 63 17.3 41.5 58.1 28 40.6 87.5 26 58.8 84.6 52.4 80.4 80.4 81 11.3 151 87 87 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 34.3 41.7 38.8 0 8 113 11.9 65.7 62.2 50 39.3 204 6.2 7.5 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036081 9036189 9036147 9036151 9036152 9036164 9036252 9036257 9036257 9036261 9036262 9036264 9036272 9036281 9036308 9036310 9036312 | 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.20 36.77 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.45 36.52 36.63 36.45 36.53 36.32 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.92 -0.72 -0.27 -0.65 -0.50 -0.48 -0.50 -0.48 -0.73 -0.92 -0.35 -0.20 -0.77 | $\begin{array}{c} 13.9\\ 40.2\\ 22.5\\ 145\\ 65.8\\ -99\\ 47\\ 8.4\\ -99\\ 51.5\\ 47.9\\ 69\\ -99\\ 43.8\\ 39.2\\ 44.8\\ 201\\ 50.7\\ 25.8\\ 94.5\\ 65.8\\ 10.1\\ 55.7\\ 12\\ 25.9\\ 6.6\end{array}$ | $\begin{array}{c} 8.2\\ 17.7\\ 18.2\\ 88\\ 93.5\\ -99\\ 4.6\\ 1.6\\ -99\\ 0\\ 85.5\\ 64.3\\ -99\\ 68.8\\ 0.5\\ 64.3\\ -99\\ 68.8\\ 0.5\\ 64.3\\ -99\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.6\\ 12.6$ | $\begin{array}{c} 37.9\\ 138\\ 25.3\\ 69.8\\ 0\\ -99\\ 18.8\\ 0.3\\ -99\\ 41.5\\ 22.4\\ 72.5\\ -99\\ 24.1\\ 44.1\\ 21.5\\ 59.3\\ 45.4\\ 20.7\\ 35.8\\ 51.4\\ 50.6\\ 21.3\\ 40\\ 32.6\\ 29.7\\ \end{array}$ | 52 81 13 40 21 30 35 5 91 149 26 24 24 58 206 9.9 32 37 96 63 64 9.8 40 49 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 27 147 25.5 67.7 49.6 115 27.2 20.8 32.3 49.7 27.9 90.3 16 40 13.8 | I5Z 6.3 10 0 39.8 17.7 26.5 23.6 24 20.5 18.3 33.4 48.2 62 49.4 750.3 6.4 24 14 5.7 28.5 46 10.5 2.3 | J5x 5.1 20.5 14.1 25.9 9.6 12.3 0.7 3.9 8.5 13.9 27.5 -999 31.7 1.5 -999 31.7 1.5 -999 77.2 6.1 8.3 35.1 -999 0 59.8 17.5 2.5 8.4 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 65.5 -99 63.5 24.3 -99 183 23.3 45.4 71.2 -99 15 64.5 28.4 72 7.6 | J5Z 18 13 5.3 77 21 39 5.9 5.9 5.9 6.6 12 6.3 39 -99 60 45 -99 91 52 17 7.3 -99 22 68 29 11 46 | K5X 5.3 28 23 43 61 13 9.9 35 7.8 17 24 56 -99 38 237 218 300 32 19 38 67 20 71 26 | K5Y 35 1.6 0 25 8.3 6.5 31 0 111 19 -99 0 16 16 92 12 10 19 192 192 26 17 12 | K5Z 0 0 3.8 2 19 0 0 0 0 0 0 0 0 0 0 0 0 0 16 0 3.5 15 0 10 5 0 177 12 12 0 | 444 138 169 1466 1744 1155 61 109 644 888 1044 1733 1655 1833 888 800 2533 91 633 1177 2288 566 1733 744 169 884 | 8.3 63.3 148 60.8 49.3 86.8 41.6 36 63 17.3 41.5 58.1 28 40.6 87.5 26 58.8 84.6 52.4 80.4 80.4 81 11.3 151 87 87 13.3 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 34.3 41.7 38.8 0 8 8 113 11.9 65.7 62.2 50 39.3 204 6.2 7.5 61.6 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036081 9036187 9036151 9036152 9036164 9036243 9036252 9036257 9036261 9036262 9036264 9036272 9036281 9036308 9036310 9036312 9036323 | 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.45 36.52 36.63 36.45 36.52 36.63 36.53 36.32 36.32 36.32 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.92 -0.72 -0.25 -0.92 -0.72 -0.65 -0.48 -0.50 -0.48 -0.73 -0.50 -0.48 -0.73 -0.20 -0.77 -0.20 -0.77 -0.20 -0.77 -0.20 -0.77 -0.20 -0.77 -0.20 | $\begin{array}{c} 13.9\\ 40.2\\ 22.5\\ 145\\ 65.8\\ -99\\ 47\\ 8.4\\ -99\\ 51.5\\ 47.9\\ 69\\ -99\\ 43.8\\ 39.2\\ 44.8\\ 201\\ 50.7\\ 25.8\\ 94.5\\ 65.8\\ 10.1\\ 55.7\\ 12\\ 25.9\\ 6.6\\ 212 \end{array}$ | $\begin{array}{c} 8.2\\ 17.7\\ 18.2\\ 88\\ 93.5\\ -99\\ 4.6\\ 1.6\\ -99\\ 0\\ 85.5\\ 64.3\\ -99\\ 68.8\\ 0.5\\ 64.3\\ -99\\ 68.8\\ 0.5\\ 64.3\\ -99\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 38.6\\ 9.7\\ 5.9\\ 12.6\\ 12.6\\ 12.0\\ 12.6\\ 12.0\\ 12.6\\ 12.0$ | $\begin{array}{c} 37.9\\ 138\\ 25.3\\ 69.8\\ 0\\ -99\\ 18.8\\ 0.3\\ -99\\ 41.5\\ 22.4\\ 72.5\\ -99\\ 24.1\\ 44.1\\ 21.5\\ 59.3\\ 45.4\\ 20.7\\ 35.8\\ 51.4\\ 50.6\\ 21.3\\ 40\\ 32.6\\ 29.7\\ 67.1\\ \end{array}$ | 52 81 13 40 21 30 35 5 91 91 149 26 24 24 58 206 9.9 32 37 96 63 64 9.8 40 49 219 | 15 Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 27 147 25.5 67.7 49.6 115 27.2 20.8 32.3 49.7 27.9 90.3 16 40 13.8 184 | I5Z 6.3 10 0 39.8 17.7 26.5 23.6 24 20.5 18.3 33.4 48.2 62 49.4 750.3 6.4 24 14 5.7 28.5 46 10.5 2.3 72.6 | J5x 5.1 20.5 14.1 25.9 9.6 12.3 0.7 3.9 8.5 13.9 27.5 -999 31.7 1.5 -999 31.7 1.5 -999 77.2 6.1 8.3 35.1 -999 0 59.8 17.5 2.5 8.4 101 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 65.5 -99 63.5 24.3 -99 183 23.3 45.4 71.2 -99 183 23.3 45.4 71.2 -99 15 64.5 28.4 72 7.6 81.6 | J5Z 18 13 5.3 77 21 39 5.9 5.9 5.9 6.6 12 6.3 39 -99 60 45 -99 91 52 17 7.3 -99 22 68 29 11 46 73 | K5x 5.3 28 23 43 61 13 9.9 35 7.8 17 24 56 -99 38 237 218 300 32 19 38 67 20 71 26 50 | K5Y 35 1.6 0 25 8.3 6.5 31 0 11 4.1 19 -999 0 16 92 10 0 19 49 192 266 177 12 777 | K5Z 0 0 3.8 2 19 0 0 0 0 0 0 0 0 0 0 0 16 0 35 0 15 0 10 5 0 177 12 12 0 14 | 444 1388 1699 1466 174 1155 61 109 64 888 800 4 173 1655 1833 888 800 2533 2533 911 633 1177 2288 566 1733 744 1699 844 2000 | 8.3 63.3 148 60.8 49.3 86.8 41.6 36 63 17.3 41.5 58.1 28 40.6 87.5 26 58.8 84.6 52.4 80.4 80.4 81 11.3 151 87 87 13.3 111 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 34.3 41.7 38.8 0 8 113 11.9 65.7 62.2 50 39.3 204 6.2 7.5 61.6 67.5 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036081 9036187 9036151 9036152 9036164 9036243 9036252 9036257 9036257 9036261 9036262 9036264 9036272 9036281 9036308 9036310 9036322 9036323 9036336 | 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.20 36.77 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.45 36.52 36.63 36.45 36.52 36.63 36.53 36.32 36.32 36.32 36.32 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.25 -0.92 -0.72 -0.27 -0.65 -0.50 -0.48 -0.73 -0.50 -0.35 -0.20 -0.77 -0.27 -0.27 | $\begin{array}{c} 13.9\\ 40.2\\ 22.5\\ 145\\ 65.8\\ -99\\ 47\\ 8.4\\ -99\\ 51.5\\ 47.9\\ 69\\ -99\\ 43.8\\ 39.2\\ 44.8\\ 201\\ 50.7\\ 25.8\\ 94.5\\ 65.8\\ 10.1\\ 55.7\\ 12\\ 25.9\\ 6.6\\ 212\\ 51.5\\ \end{array}$ | 8.2 17.7 18.2 88 93.5 -99 4.6 1.6 -99 0 85.5 64.3 -99 68.8 0.5 64.3 -99 68.8 0.5 64 208 4.7 5.9 12.6 38.6 9.7 56.6 27.5 57.6 9.1 209 49.3 | 37.9 138 25.3 69.8 0 -99 18.8 0.3 -99 41.5 22.4 72.5 -99 24.1 44.1 21.5 59.3 45.4 20.7 35.8 51.4 50.6 21.3 40 32.6 29.7 67.1 7.8 | 52 81 13 63 40 21 21 30 35 5 91 91 149 26 24 58 206 9.9 32 37 96 63 64 9.8 40 49 9.8 40 9.9 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 27 147 25.5 67.7 49.6 115 27.2 20.8 32.3 49.7 27.9 90.3 16 40 13.8 184 -99 | 152 6.3 10 0 39.8 17.7 26.5 23.6 2 32.4 20.5 18.3 33.4 48.2 62 49.4 47.8 89.7 50.3 6.4 24 14 5.7 28.5 46 10.5 2.3 72.6 -99 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 0 3.9 8.5 13.9 27.5 -99 31.7 1.5 -99 77.2 6.1 8.3 35.1 -99 0 59.8 17.5 2.5 8.4 101 -99 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 65.5 -99 63.5 24.3 -99 183 23.3 45.4 71.2 -99 183 23.3 45.4 71.2 -99 15 64.5 28.4 72 72 64.5 28.4 72 72 64.5 | J5Z 18 13 5.3 77 21 39 5.9 5.9 5.9 6.6 12 6.3 39 -99 60 45 -99 91 52 17 7.3 -99 22 68 29 11 46 73 -99 | K5X 5.3 28 23 43 61 13 9.9 35 7.8 17 24 56 -99 38 23 37 218 30 32 19 38 67 20 71 26 50 57 | K5Y 35 1.6 0 25 8.3 6.5 31 0 111 19 -99 0 16 92 12 10 19 -99 0 16 16 92 12 10 199 192 26 17 12 777 34 | K5Z 0 0 3.8 2 19 0 0 0 0 0 0 0 0 0 0 0 16 0 35 0 15 0 10 5 0 177 12 12 0 14 1.1 | 444 138 169 1466 174 115 61 109 64 88 88 104 173 165 183 88 80 253 88 80 253 91 63 1177 228 56 63 1177 228 84 200 215 | 8.3 63.3 148 60.8 49.3 86.8 41.6 36 63 17.3 41.5 58.1 28 40.6 87.5 26 58.8 84.6 52.4 80.4 80.4 81 11.3 151 87 87 13.3 111 54.2 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 34.3 41.7 38.8 0 8 113 11.9 65.7 62.2 50 39.3 204 6.2 7.5 61.6 67.5 12.6 |
| May | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036081 9036187 9036151 9036152 9036164 9036243 9036252 9036257 9036261 9036262 9036264 9036272 9036281 9036308 9036310 9036312 9036323 | 36.43 36.63 36.63 36.63 36.62 36.42 36.77 36.38 36.20 36.42 36.77 36.38 36.20 36.17 36.65 36.63 36.70 36.70 36.77 36.10 36.77 36.10 36.77 36.10 36.77 36.10 36.77 36.10 36.72 36.52 36.63 36.45 36.90 36.32 36.32 36.32 36.28 36.03 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.25 -0.92 -0.72 -0.27 -0.65 -0.50 -0.48 -0.73 -0.50 -0.35 -0.20 -0.77 -0.27 -0.27 | 13.9 40.2 22.5 145 65.8 -99 47 8.4 -99 51.5 47.9 69 -99 43.8 39.2 44.8 201 50.7 25.8 94.5 65.8 10.1 55.7 12 25.9 6.6 212 51.5 40 | 8.2 17.7 18.2 88 93.5 -99 4.6 1.6 -99 0 85.5 64.3 -99 68.8 0.5 64.3 -99 68.8 0.5 64 208 4.7 5.9 12.6 38.6 9.7 56.6 27.5 57.6 9.1 209 49.3 0 | $\begin{array}{c} 37.9\\ 138\\ 25.3\\ 69.8\\ 0\\ -99\\ 18.8\\ 0.3\\ -99\\ 41.5\\ 22.4\\ 72.5\\ -99\\ 24.1\\ 44.1\\ 21.5\\ 59.3\\ 45.4\\ 20.7\\ 35.8\\ 51.4\\ 50.6\\ 21.3\\ 40\\ 32.6\\ 29.7\\ 67.1\\ \end{array}$ | 52 81 13 63 40 21 21 30 35 5 91 91 149 26 24 58 206 9.9 32 37 96 63 64 9.8 40 49 9.8 40 49 53 5 | 15Y 21.8 19.2 14.9 63.1 116 29.6 7.7 20 5.4 18.2 18.4 27 147 25.5 67.7 49.6 115 27.2 20.8 32.3 49.7 27.9 90.3 16 40 13.8 184 -99 225 | I5Z 6.3 10 0 39.8 17.7 26.5 23.6 2 32.4 20.5 18.3 33.4 48.2 62 49.4 47.8 89.7 50.3 6.4 24 14 5.7 28.5 46 10.5 2.3 72.6 -99 5 | J5X 5.1 20.5 14.1 25.9 9.6 12.3 0.7 0 3.9 8.5 13.9 27.5 -99 31.7 1.5 -99 77.2 6.1 8.3 35.1 -99 0 59.8 17.5 2.5 8.4 101 -99 34.7 | J5Y 16.8 26.8 30.7 50.7 78.2 20.1 49.1 37.5 32.6 38.2 79.2 65.5 -99 63.5 24.3 -99 183 23.3 45.4 71.2 -99 183 23.3 45.4 71.2 -99 15 64.5 28.4 72 72 64.5 28.4 72 72 64.5 | J5Z 18 13 5.3 77 21 39 5.9 5 6.6 12 63 39 -99 60 45 -99 91 52 17 7.3 -99 222 68 29 11 46 73 -99 10 | K5x 5.3 28 23 43 61 13 9.9 35 7.8 17 24 56 -99 38 237 218 300 32 19 38 67 20 71 26 50 | K5Y 35 1.6 0 25 8.3 6.5 31 0 111 19 -99 0 16 92 12 10 19 92 12 10 19 192 26 17 34 2 | K5Z 0 3.8 2 25 19 0 0 0 0 0 0 0 0 0 0 0 0 16 0 35 15 0 10 5 0 177 12 12 0 14 1.1 13 | 444 138 169 146 174 115 61 109 64 88 80 173 165 183 88 80 253 88 80 253 91 63 1177 228 56 63 1177 228 84 200 215 564 | 8.3 63.3 148 60.8 49.3 86.8 41.6 36 63 17.3 41.5 58.1 28 40.6 87.5 26 58.8 84.6 52.4 80.4 81 11.3 151 87 87 13.3 111 54.2 21 | 41.9 77.2 45 57.4 19.1 5.8 44.1 29 71.5 66 47.8 34.3 41.7 38.8 0 8 113 11.9 65.7 62.2 50 39.3 204 6.2 7.5 61.6 67.5 12.6 |

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| June | ID | LON | LAT | нбх | нбү | H6Z | I6X | I6Y | I6Z | J6X | J6Y | J6Z | K6X | K6Y | K6Z | L6X | L6Y | L6Z |
|------|--|--|--|--|--|---|---|---|---|---|---|--|---|--|--|---|---|---|
| | 9036002 | 36.43 | -0.72 | 6.4 | 30.8 | | 1.5 | | | 36.5 | | 1.9 | 0 | 72 | 13 | 45 | 40.5 | 0 |
| | 9036025 | 36.63 | -0.58 | 19.8 | 66.6 | 20.8 | 19 | 44.2 | 76.5 | 95.4 | 24.4 | 18 | -99 | -99 | -99 | 129 | 5 | 40.6 |
| | 9036034 | 36.33 | -0.50 | 19.4 | 52.2 | 8.3 | 6.6 | 28.4 | 28.6 | 51.1 | 16.5 | 1.4 | 6 | 15 | 17 | 50 | 46.4 | 0 |
| | 9036061 | 36.63 | -0.98 | 31.2 | 6.2 | 28.8 | -99 | -99 | -99 | 40.5 | 55.1 | 5 | 6.5 | 11 | 4 | 50 | 4.5 | 0 |
| | 9036072 | 36.25 | -0.35 | 4.5 | 18.8 | 17.5 | -99 | -99 | -99 | 48.8 | 42.2 | 0 | 5.6 | 23 | 5.6 | 36 | 0 | 2.9 |
| | 9036076 | 36.02 | -0.30 | 26.2 | 50.7 | 39 | -99 | -99 | -99 | 40 | 44.6 | 3.5 | 11 | 8.1 | 9 | 118 | 17.7 | 40.1 |
| | 9036081 | 36.42 | -0.65 | 9 | 31.8 | | -99 | -99 | -99 | 96.5 | | 0 | 0 | 0.7 | 19 | 33 | 9.1 | 5.4 |
| | 9036085 | 36.77 | -0.13 | 4 | 42.2 | | 0 | 5.4 | 4.5 | | 24.7 | 0 | 0 | 11 | 14 | 11 | 0 | 5 |
| | 9036109 | 36.38 | -0.65 | | 43.8 | 12.3 | | 46.5 | 34.2 | | | 12 | 0 | 1.5 | 31 | 29 | 5.5 | 15 |
| | 9036147 | 36.20 | -0.47 | 44.2 | 54.6 | 22.9 | 11 | | 78.7 | 136 | | 6.5 | 7.3 | 15 | 7.6 | 23 | 7.3 | 26.1 |
| | 9036151 | 36.17 | -0.03 | 49 | 69.5 | 49.9 | 2 | | 64.4 | 139 | 143 | 6.5 | 23 | 25 | 87 | 62 | 12.4 | 63.5 |
| | 9036152 9036164 | 36.65 | -0.72 | 79 -99 | 59.8 -99 | 31.7 -99 | 7.8 -99 | 61 -99 | 22.2 -99 | -99 81.5 | -99 30 | -99 5.1 | 0 -99 | 45 -99 | 14 -99 | 7 104 | 13.2 | 0 |
| | 9036243 | 36.23 | -0.25 | 10.6 | 57.8 | 24.3 | -99 | -99 | -99 | | 30.2 | 0 | 26 | 59 | 14 | 65 | 73.9 | |
| | 9036252 | 36.08 | | 77.2 | 28.9 | 44.9 | | 30.8 | 79.2 | | 12.2 | 16 | 11 | 26 | 23 | 22 | 37.7 | 6 |
| | 9036252 | 36.70 | | 0.2 | 1.6 | | 2.5 | | 20.5 | -99 | -99 | -99 | -99 | -99 | -99 | -99 | -99 | -99 |
| | 9036259 | 36.77 | -0.72 | 23.2 | 34.8 | 51.7 | | 33.5 | 34.6 | -99 | -99 | -99 | 56 | 82 | 60 | 141 | 17.5 | 13 |
| | 9036261 | 36.10 | -0.27 | 49.5 | 32.3 | 35.8 | 13 | | 35.8 | 15.8 | 0 | 0 | 11 | 31 | 30 | 40 | 39.9 | 27.8 |
| | 9036262 | 36.45 | -0.65 | 13.1 | 26.2 | 31.7 | 6.3 | 61.8 | 9.8 | 37.1 | 61.5 | 6.8 | 0 | 47 | 9.4 | 60 | 7.7 | 12.9 |
| | 9036264 | 36.52 | -0.50 | 43.8 | 84.1 | 46.5 | 22 | 2 | 45.6 | 65.2 | 105 | 0 | 14 | 57 | 29 | 64 | 82.2 | 2.1 |
| | 9036272 | 36.63 | -0.48 | 28.1 | 96.8 | 11.8 | 44 | 56.4 | 53.5 | 154 | 73.5 | 30 | 7 | 47 | 31 | 60 | 27 | 4 |
| | 9036281 | 36.45 | -0.73 | 2.5 | 30 | 25.3 | 2 | 16.1 | 18.6 | 35.8 | 49.7 | 1 | 1.1 | 49 | 16 | 39 | 31.9 | 0 |
| | 9036308 | 36.90 | -0.92 | 5.8 | 4.7 | 9 | 13 | 11 | 9.7 | 0 | 0 | 0 | -99 | -99 | -99 | 210 | 11.5 | 1.7 |
| | 9036310 | 36.03 | -0.35 | 26.9 | 18.5 | 14.7 | 26 | 35 | 86.9 | 80.7 | 17 | 11 | 25 | 34 | 24 | 50 | 24.9 | 10 |
| | 9036312 | 36.53 | -0.20 | 34 | 73.2 | 15.9 | | 20.5 | 34.8 | - | 16.1 | 0 | 28 | 39 | 24 | 24 | 19 | 16.8 |
| | 9036322 | 36.32 | -0.77 | | 49.6 | 26.3 | | 14.7 | | 30.3 | | 2.5 | 0 | 3.6 | 12 | 35 | 26.9 | 0 |
| | 9036323 | 36.82 | -0.70 | 10.9 | 45.7 | 30.5 | | 15.4 | 34.3 | | 48.3 | 21 | 31 | 50 | 36 | 117 | 4.1 | 17.5 |
| | 9036336 | 36.28 | -0.27 | 64.4 | 48 | 7.9 | -99 | -99 | -99 | 211 | 15 | 0 | 0 | 70 | 32 | 69 | 85.6 | 84 |
| | 9036337 9036343 | 36.03 | -0.58 | 14 29 | 26.5 21.9 | 12.5 | 30 | 40.5 | 46.5 | 111 | 53 | 2.5 | 9.5 | 32 | 31 26 | -99 33 | -99 3.7 | -99 0 |
| | 9030343 | | | | | | | | | | | | | | | | | |
| Oct | ID | | | | | | | | | | | - | - | | | | | LAZ |
| Oct | ID 9036002 | LON 36.43 | LAT -0.72 | HAX 16.2 | HAY 26.9 | HAZ 52.7 | -99 | | -99 | JAX | 12.3 JAY 22.3 | JAZ 53 | - | | | | LAY 29.8 | LAZ 29.1 |
| Oct | | LON | LAT | HAX | HAY | HAZ | IAX | IAY | IAZ -99 | JAX | JAY 22.3 | JAZ | KAX | KAY | KAZ | LAX | LAY | |
| Oct | 9036002 | LON 36.43 | LAT -0.72 -0.58 | HAX 16.2 | HAY 26.9 | HAZ 52.7 | IAX -99 | IAY -99 | IAZ -99 -99 | JAX 1 | JAY 22.3 45.1 | JAZ | KAX 32 | KAY 54 | KAZ 25 | LAX | LAY 29.8 | 29.1 |
| Oct | 9036002 9036025 | LON 36.43 36.63 | LAT -0.72 -0.58 | HAX 16.2 3.2 | HAY 26.9 55.6 | HAZ 52.7 66.4 | IAX -99 -99 | IAY -99 -99 | IAZ -99 -99 | JAX 1 12.8 | JAY 22.3 45.1 | JAZ 53 30 | KAX 32 28 | KAY 54 87 | KAZ 25 55 | LAX 0 22 | LAY 29.8 15.3 | 29.1 36 |
| Oct | 9036002 9036025 9036034 | LON 36.43 36.63 36.33 | LAT -0.72 -0.58 -0.50 | HAX 16.2 3.2 0 | HAY 26.9 55.6 13.2 | HAZ 52.7 66.4 32.8 | IAX -99 -99 -99 | IAY -99 -99 -99 | IAZ -99 -99 -99 | JAX 1 12.8 12.3 0 | JAY 22.3 45.1 11.7 | JAZ 53 30 4.7 | KAX 32 28 13 | KAY 54 87 18 | KAZ 25 55 27 | LAX 0 22 5.1 | LAY 29.8 15.3 20.7 | 29.1 36 18.4 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 | LON 36.43 36.63 36.33 36.63 | LAT -0.72 -0.58 -0.50 -0.98 | HAX 16.2 3.2 0 9.5 0 0 | HAY 26.9 55.6 13.2 126 38.6 21.4 | HAZ 52.7 66.4 32.8 142 | IAX -99 -99 -99 -99 -99 -99 | IAY -99 -99 -99 -99 -99 -99 | IAZ -99 -99 -99 -99 -99 -99 -99 | JAX 1 12.8 12.3 0 | JAY 22.3 45.1 11.7 0 45.9 | JAZ 53 30 4.7 8.6 11 23 | KAX 32 28 13 64 63 -99 | KAY 54 87 18 89 133 -99 | KAZ 25 55 27 142 93 -99 | LAX 0 22 5.1 0 | LAY 29.8 15.3 20.7 0 3.4 22.4 | 29.1 36 18.4 0 8.9 2.8 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 | LON 36.43 36.63 36.33 36.63 36.25 36.02 36.42 | LAT -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 | HAX 16.2 3.2 0 9.5 0 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 | IAX -99 -99 -99 -99 -99 -99 -99 -99 | IAY - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | IAZ -99 -99 -99 -99 -99 -99 -99 -99 | JAX 12.8 12.3 0 4.5 25.9 0 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 | JAZ 53 30 4.7 8.6 11 23 33 | KAX 32 28 13 64 63 -99 37 | KAY 54 87 18 89 133 -99 47 | KAZ 25 55 27 142 93 -99 16 | LAX 0 22 5.1 0 14 58 0 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 | 29.1 36 18.4 0 8.9 2.8 10.5 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 | LON 36.43 36.63 36.63 36.25 36.02 36.42 36.77 | LAT -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 | HAX 16.2 3.2 0 9.5 0 0 6.8 0 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | JAX 12.8 12.3 0 4.5 25.9 0 8 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 | JAZ 53 30 4.7 8.6 11 23 33 1.5 | KAX 32 28 13 64 63 -99 37 16 | KAY 54 87 18 89 133 -99 47 61 | KAZ 25 55 27 142 93 -99 16 12 | LAX 0 22 5.1 0 14 58 0 47 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 | LON 36.43 36.63 36.63 36.63 36.25 36.02 36.42 36.77 36.38 | LAT -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 | HAX 16.2 3.2 0 9.5 0 0 6.8 0 0 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 1 12.8 12.3 0 4.5 25.9 0 8 29.1 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 0 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 | KAX 32 28 13 64 63 -99 37 16 38 | KAY 54 87 18 89 133 -99 47 61 46 | KAZ 25 55 27 142 93 -99 16 12 21 | LAX 0 22 5.1 0 14 58 0 47 -99 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 | LON 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.42 36.77 36.38 36.20 | LAT -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 | HAX 16.2 3.2 0 9.5 0 0 6.8 0 0 0 0 0 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 1 12.8 12.3 0 4.5 25.9 0 8 29.1 11.9 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 0 10.2 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 14 | KAX 32 28 13 64 63 -99 37 16 38 4.6 | KAY 54 87 18 89 133 -99 47 61 46 41 | KAZ 25 55 27 142 93 -99 16 12 21 7.7 | LAX 0 22 5.1 0 14 58 0 47 -99 4.8 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 | LON 36.43 36.63 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 | LAT -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 | HAX 16.2 3.2 0 9.5 0 0 6.8 0 0 0 3.7 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 1 12.8 12.3 0 4.5 25.9 0 8 29.1 11.9 0 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 0 10.2 33.5 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 14 29 | KAX 32 28 13 64 63 -99 37 16 38 4.6 25 | KAY 54 87 18 89 133 -99 47 61 46 41 69 | <pre>KAZ 25 55 27 142 93 -99 16 12 21 7.7 47</pre> | LAX 0 22 5.1 0 14 58 0 47 -99 4.8 -99 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 | LON 36.43 36.63 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 | LAT -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 | HAX 16.2 3.2 0 9.5 0 0 6.8 0 0 0 0 3.7 15.8 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 12.8 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 0 10.2 33.5 15.3 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 14 29 0 | KAX 32 28 13 64 63 -99 37 16 38 4.6 25 53 | KAY 54 87 18 89 133 -99 47 61 46 41 69 124 | KAZ 25 55 27 142 93 -99 16 12 21 7.7 47 68 | LAX 0 22 5.1 0 14 58 0 47 -99 4.8 -99 -99 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 -99 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 | LON 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.65 | LAT -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 | HAX 16.2 3.2 0 9.5 0 0 6.8 0 0 0 0 3.7 15.8 -99 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 -99 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 -99 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 12.8 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 0 11.9 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 0 10.2 33.5 15.3 0 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 1.4 29 0 14 29 0 38 | KAX 32 28 13 64 63 -99 37 16 38 4.6 25 53 -99 | KAY 54 87 18 89 133 -99 47 61 46 41 69 124 -99 | KAZ 25 55 27 142 93 -99 16 12 21 7.7 47 68 -99 | LAX 0 22 5.1 0 14 58 0 47 -99 4.8 -99 -99 37 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 12.8 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 -99 0 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 | LON 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.65 36.68 36.23 | LAT -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 | HAX 16.2 3.2 0 9.5 0 0 6.8 0 0 0 0 3.7 15.8 -99 0 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 -99 17.1 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 -99 22.4 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 12.8 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 0 13 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 8 0 10.2 33.5 15.3 0 8.7 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 1.4 29 0 14 29 0 38 30 | KAX 32 28 13 64 63 -99 37 16 38 4.6 25 53 -99 68 | KAY 54 87 18 89 133 -99 47 61 46 41 69 124 -99 84 | KAZ 25 55 27 142 93 -99 16 12 21 7.7 47 68 -99 121 | LAX 0 22 5.1 0 14 58 0 47 -99 4.8 -99 -99 37 69 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 -99 12.8 47.8 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 -99 0 61 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036085 9036109 9036147 9036151 9036152 9036164 9036243 9036252 | LON 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.65 36.68 36.23 36.08 | LAT -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.25 | HAX 16.2 3.2 0 9.5 0 0 6.8 0 0 0 0 3.7 15.8 -99 0 3.5 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 -99 17.1 31 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 -99 22.4 23 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 12.8 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 0 13 13 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 0 10.2 33.5 15.3 0 8.7 11.8 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 1.4 29 0 14 29 0 38 30 9.7 | KAX 32 28 13 64 63 -999 377 166 255 53 -999 68 0 | KAY 54 87 18 89 133 -99 47 61 46 41 69 124 -99 | KAZ 25 55 27 142 93 -99 16 12 21 7.7 47 68 -99 121 87 | LAX 0 22 5.1 0 14 58 0 47 -99 4.8 -99 -99 37 69 -99 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 12.8 47.8 -99 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 -99 0 61 -99 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 | LON 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.65 36.68 36.23 36.08 36.70 | LAT -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.25 -0.92 | HAX 16.2 3.2 0 9.5 0 0 6.8 0 0 0 0 3.7 15.8 -99 0 3.5 -99 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 -99 17.1 31 -99 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 -99 22.4 23 -99 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 12.8 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 0 4 0 13 -99 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 8 0 10.2 33.5 15.3 0 8.7 11.8 -99 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 1.4 29 0 14 29 0 38 30 9.7 -99 | KAX 32 28 13 64 63 -999 377 166 255 53 -999 68 0 0 | KAY 54 87 18 93 133 -99 47 61 46 41 69 124 -99 84 54 47 | KAZ 25 55 27 142 93 -99 16 12 21 7.7 47 68 -99 121 87 | LAX 0 22 5.1 0 14 58 0 47 -99 4.8 -99 -99 37 69 -99 -99 -99 -99 -99 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 12.8 47.8 -99 -99 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 -99 0 61 -99 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 9036252 9036257 | LON 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.68 36.70 36.77 | LAT -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.92 -0.72 | HAX 16.2 3.2 0 9.5 0 0 6.8 0 0 6.8 0 0 3.7 15.8 -99 0 3.5 -99 8.9 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 -99 17.1 31 -99 142 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 -99 22.4 23 -99 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 12.8 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 0 13 13 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 0 10.2 33.5 15.3 0 8.7 11.8 -99 57.6 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 1.4 29 0 14 29 0 38 30 9.7 -99 | KAX 32 28 13 64 63 -999 377 166 255 53 -999 68 0 0 | KAY 54 87 18 93 133 -99 47 61 46 41 69 124 -99 84 54 47 | KAZ 25 55 27 142 93 -99 16 21 7.7 68 -99 121 87 40 170 | LAX 0 22 5.1 0 14 58 0 4.8 -99 4.8 -99 37 69 -99 37 69 -99 -99 7.5 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 12.8 47.8 -99 -99 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 -99 0 61 -99 -99 -99 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 9036252 9036257 9036259 | LON 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.68 36.23 36.77 36.68 36.77 36.68 | LAT -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.25 -0.92 -0.72 -0.72 | HAX 16.2 3.2 0 9.5 0 6.8 0 0 6.8 0 0 6.8 0 0 3.7 15.8 -99 0 3.5 -99 8.9 8.9 8.9 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 -99 17.1 31 -99 142 17 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 -99 22.4 23 -99 198 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 12.8 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 0 13 -99 11.3 10.6 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 0 10.2 33.5 15.3 0 8.7 11.8 -99 57.6 36.1 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 1.4 29 0 14 29 0 38 30 9.7 -99 48 17 | KAX 32 28 13 64 63 -99 37 16 38 4.6 53 -99 68 0 86 | KAY 54 54 87 18 99 133 -99 47 61 46 41 69 124 -99 84 54 47 297 | KAZ 25 55 27 142 93 -99 16 121 7.7 68 -99 121 87 40 170 123 | LAX 0 22 5.1 0 14 58 0 4.8 -99 4.8 -99 37 69 -99 37 69 -99 -99 7.5 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 12.8 47.8 -99 9-99 12.2 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 21 -99 0 61 -99 -99 3.9 3.5 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 9036252 9036257 9036259 9036261 | LON 36.43 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.88 36.23 36.70 36.77 36.68 | LAT -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.25 -0.92 -0.72 -0.72 | HAX 16.2 3.2 0 9.5 0 6.8 0 0 6.8 0 0 6.8 0 0 3.7 15.8 -99 0 3.5 -99 8.9 8.9 6.2 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 -99 17.1 31 -99 142 17 28.4 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 -99 22.4 23 -99 198 17.6 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 12.8 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 0 13 -99 11.3 10.6 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 0 10.2 33.5 15.3 0 8.7 11.8 -99 57.6 36.1 0.6 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 1.4 29 0 14 29 0 38 30 9.7 -99 48 17 | KAX 32 28 13 64 63 -99 37 16 25 53 -99 68 0 86 18 | KAY 54 54 87 18 99 133 -99 47 61 46 41 69 124 -99 84 54 47 297 38 | KAZ 25 55 27 142 93 -99 16 121 7.7 68 -99 121 87 40 170 123 | LAX 0 22 5.1 4 4 -99 4.8 -99 4.8 -99 377 69 -99 -99 7.5 9.6 0 0 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 12.8 47.8 -99 91.2 34.3 18.5 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 21 -99 0 61 -99 3.9 3.5 6.5 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 9036252 9036257 9036259 9036261 | LON 36.43 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.88 36.23 36.70 36.77 36.68 | LAT -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.25 -0.27 -0.50 | HAX 16.2 3.2 0 9.5 0 6.8 0 0 6.8 0 0 6.8 0 0 3.7 15.8 -99 0 3.5 -99 8.9 8.9 6.2 5 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 -99 17.1 31 -99 142 177 28.4 15.7 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 -99 22.4 23 -99 198 17.6 46.8 37.4 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 12.3 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 0 13 -99 11.3 10.6 10 28.5 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 0 10.2 33.5 15.3 0 8.7 11.8 -99 57.6 36.1 0.6 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 14 29 0 14 29 0 38 30 9.7 -99 48 17 6.6 | KAX 32 28 13 64 63 -99 37 16 38 4.6 25 53 -999 68 0 86 18 31 | KAY 54 54 87 18 99 133 -99 47 61 46 41 69 124 -99 84 54 47 297 38 46 | KAZ 25 55 27 142 93 -99 16 121 7.7 68 -99 121 87 40 170 123 5.8 15 | LAX 0 22 5.1 1 4 5 4 7 99 4.8 -99 4.8 -99 37 69 -99 37 69 -99 7.5 9.6 0 0 0 0 0 0 0 0 0 0 0 0 0 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 12.8 47.8 -99 91.2 34.3 18.5 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 21 -99 0 61 -99 3.9 3.5 6.5 22 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036185 9036147 9036152 9036164 9036243 9036252 9036257 9036251 9036261 9036264 | LON 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.08 36.70 36.77 36.08 36.23 36.08 36.23 36.08 36.52 36.65 36.52 36.52 36.63 | LAT -0.72 -0.58 -0.50 -0.98 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.25 -0.92 -0.72 -0.50 -0.50 -0.50 -0.50 -0.48 | HAX 16.2 3.2 0 9.5 0 6.8 0 0 6.8 0 0 0 3.7 15.8 -99 0 3.5 -99 8.9 8.9 8.9 6.2 5 32.4 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 -99 17.1 31 -99 142 177 28.4 15.7 48.9 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 -99 22.4 23 -99 198 17.6 46.8 37.4 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 12.3 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 0 13 -99 11.3 10.6 10 28.5 19 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 0 10.2 33.5 15.3 0 8.7 11.8 -99 57.6 36.1 0.6 59.6 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 14 29 0 14 29 0 38 30 9.7 -99 48 17 6.6 59 21 | KAX 32 28 13 64 63 -999 377 166 25 53 -999 68 0 86 18 31 12 | KAY 54 57 18 99 133 -99 47 61 46 41 69 124 -99 84 54 47 38 46 45 | KAZ 25 55 27 142 93 -99 16 221 7.77 477 68 -99 121 877 40 170 123 5.8 15 138 | LAX 0 22 5.1 4 4 -99 4.8 -99 4.8 -99 377 69 -99 7.5 9.6 0 5.9 64 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 12.8 47.8 -99 91.2 34.3 18.5 12.6 41 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 21 -99 0 61 -99 3.9 3.5 6.5 22 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036081 9036185 9036147 9036151 9036152 9036164 9036252 9036257 9036251 9036261 9036264 9036272 | LON 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.08 36.70 36.77 36.65 36.63 36.73 36.63 36.45 | LAT -0.72 -0.58 -0.50 -0.98 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.25 -0.92 -0.72 -0.50 -0.50 -0.50 -0.50 -0.48 -0.73 | HAX 16.2 3.2 0 9.5 0 0 6.8 0 0 6.8 0 0 3.7 15.8 -99 0 3.5 -99 8.9 8.9 8.9 6.2 5 32.4 13.2 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 -99 17.1 31 -99 142 177 28.4 15.7 48.9 34.6 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 -99 22.4 23 -99 198 17.6 46.8 37.4 62.9 24.4 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 12.3 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 0 13 -99 11.3 10.6 10 28.5 19 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 0 10.2 33.5 15.3 0 8.7 11.8 -99 57.6 36.1 0.6 59.6 73 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 14 29 0 14 29 0 38 30 9.7 -99 48 17 6.6 59 21 53 | KAX 32 28 13 64 63 -999 377 166 25 53 -999 68 0 0 866 18 31 12 64 31 | KAY 54 57 18 99 133 -99 47 61 46 41 69 124 -99 84 54 47 297 38 46 45 117 | KAZ 25 55 27 142 93 -99 16 221 7.77 477 68 -99 121 877 40 170 123 5.8 15 138 | LAX 0 22 5.1 4 4 -99 4.8 -99 4.8 -99 377 69 -99 7.5 9.6 0 5.9 64 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 12.8 47.8 -99 91.2 34.3 18.5 12.6 41 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 21 -99 0 61 -99 3.9 3.5 6.5 22 55 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036081 9036185 9036147 9036151 9036152 9036164 9036252 9036257 9036251 9036261 9036262 9036264 9036272 9036281 | LON 36.43 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.70 36.77 36.10 36.77 36.10 36.72 36.63 36.45 36.52 36.63 36.45 36.90 | LAT -0.72 -0.58 -0.50 -0.98 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.92 -0.72 -0.50 -0.50 -0.48 -0.50 -0.48 -0.73 -0.92 | HAX 16.2 3.2 0 9.5 0 6.8 0 0 6.8 0 0 0 3.7 15.8 -99 0 3.5 -99 8.9 8.9 6.2 5 32.4 13.2 0 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 -99 17.1 31 -99 142 177 28.4 15.7 48.9 34.6 135 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 -99 22.4 23 -99 198 17.6 46.8 37.4 62.9 24.4 74.8 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 12.3 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 0 13 -99 11.3 10.6 10 28.5 19 1.8 0 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 0 10.2 33.5 15.3 0 8.7 11.8 -99 57.6 36.1 0.6 59.6 73 16 0 0 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 14 29 0 14 29 0 38 30 9.7 -99 48 17 6.6 59 21 53 | KAX 32 28 13 64 63 -999 377 166 38 4.6 25 53 -999 68 0 0 866 18 31 12 64 31 237 | KAY 54 57 18 99 133 -99 47 61 46 41 69 124 -99 84 54 47 297 38 46 45 117 48 | KAZ 25 55 27 142 93 -99 16 221 7.77 477 68 -999 121 877 400 1700 123 5.8 15 138 6.4 | LAX 0 22 5.1 14 58 0 4.8 -99 4.8 -99 37 69 -99 7.5 9.6 0 5.9 64 4.4 37 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 12.8 47.8 -99 91.2 34.3 18.5 12.6 41 43 0 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 21 -99 0 61 -99 3.9 3.5 6.5 22 55 18.4 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036252 9036257 9036257 9036261 9036262 9036264 9036272 9036281 9036308 | LON 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.77 36.10 36.72 36.62 36.52 36.52 36.52 36.52 36.63 36.45 36.90 36.03 | LAT -0.72 -0.58 -0.50 -0.98 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.25 -0.92 -0.72 -0.50 -0.50 -0.50 -0.48 -0.73 -0.92 -0.73 -0.92 -0.35 | HAX 16.2 3.2 0 9.5 0 0 6.8 0 0 6.8 0 0 0 3.7 15.8 -99 0 3.5 -99 8.9 8.9 8.9 6.2 5 32.4 13.2 0 0 0 0 0 0 0 0 0 0 0 0 0 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 -99 17.1 31 -99 142 177 28.4 15.7 48.9 34.6 135 22.7 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 -99 22.4 23 -99 198 17.6 46.8 37.4 62.9 24.4 74.8 2.1 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 12.3 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 0 13 -99 11.3 10.6 10 28.5 19 1.8 0 5 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 0 10.2 33.5 15.3 0 8.7 11.8 -99 57.6 36.1 0.6 59.6 73 16 0 0 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 14 29 0 14 29 0 388 30 9.7 -99 48 17 6.6 59 21 53 0 | KAX 32 28 13 64 63 -999 377 166 38 4.6 25 53 -999 68 0 0 866 18 31 12 64 31 237 | KAY 54 87 18 99 47 61 46 41 69 124 -99 84 54 47 38 46 45 117 48 104 | KAZ 25 55 27 142 93 -99 16 221 7.7 47 68 -99 121 87 40 170 123 5.8 15 138 6.4 115 58 | LAX 0 22 5.1 14 58 0 4.8 -99 4.8 -99 37 69 -99 7.5 9.6 0 5.9 64 4.4 37 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 12.8 47.8 -99 91.2 34.3 18.5 12.6 41 43 0 36.7 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 21 -99 0 61 -99 3.9 3.5 6.5 222 55 18.4 0 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036187 9036151 9036152 9036164 9036243 9036252 9036257 9036261 9036262 9036264 9036272 9036281 9036308 9036310 9036312 | LON 36.43 36.63 36.63 36.25 36.02 36.42 36.42 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.68 36.77 36.68 36.23 36.08 36.70 36.77 36.10 36.77 36.10 36.77 36.38 36.23 36.32 36.32 | LAT - 0.72 - 0.58 - 0.50 - 0.98 - 0.35 - 0.30 - 0.65 - 0.13 - 0.65 - 0.47 - 0.03 - 0.72 - 0.72 - 0.25 - 0.25 - 0.27 - 0.25 - 0.27 - 0.65 - 0.50 - 0.48 - 0.73 - 0.92 - 0.50 - 0.35 - 0.20 - 0.27 - 0.25 - 0.27 - | HAX 16.2 3.2 0 9.5 0 0 6.8 0 0 0 0 3.7 15.8 -99 0 3.5 -99 8.9 8.9 6.2 5 32.4 13.2 0 0 18.2 21.1 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 -99 17.1 31 -99 142 177 28.4 15.7 48.9 34.6 135 22.7 16 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 -99 22.4 23 -99 198 17.6 46.8 37.4 62.9 24.4 74.8 2.1 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 1 12.8 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 0 13 -99 11.3 10.6 10 28.5 19 1.8 0 5 3.5 15.8 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 7 33.5 15.3 0 8.7 11.8 -99 57.6 36.1 0.6 59.6 73 16 0 6 2 2 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 14 29 0 14 29 0 38 30 9.7 -99 48 17 6.6 59 21 53 0 0 0 24 29 | KAX 32 28 13 64 63 -999 37 166 38 4.6 25 53 -999 68 0 0 866 18 311 122 64 31 237 9.2 100 24 | KAY 54 57 18 -99 47 61 46 41 69 124 -99 84 54 47 38 46 417 38 46 45 117 48 104 32 48 26 | KAZ 25 55 27 142 93 -99 16 21 7.7 47 68 -99 121 87 40 123 5.8 15 138 6.4 115 58 30 23 | LAX 0 22 5.1 4 -99 4.8 -99 4.8 -99 37 69 -99 7.5 9.6 0 5.9 64 4.4 37 16 30 8.4 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 12.8 47.8 47.8 -99 91.2 34.3 18.5 12.6 41 43 0 36.7 61.6 45.7 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 21 -99 0 61 -99 3.9 3.5 6.5 22 55 18.4 0 0 15.2 19.8 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036072 9036081 9036085 9036187 9036151 9036152 9036147 9036152 9036252 9036257 9036257 9036261 9036262 9036264 9036272 9036281 9036308 9036310 9036312 9036323 | LON 36.43 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.77 36.65 36.63 36.23 36.68 36.70 36.70 36.70 36.65 36.68 36.70 36.70 36.65 36.68 36.70 36.52 36.63 36.52 36.63 36.52 36.63 36.53 36.53 36.32 36.32 36.32 | LAT -0.72 -0.58 -0.50 -0.98 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.92 -0.72 -0.25 -0.92 -0.50 -0.50 -0.48 -0.50 -0.48 -0.50 -0.48 -0.73 -0.50 -0.48 -0.73 -0.50 -0.48 -0.73 -0.50 -0.48 -0.73 -0.50 -0.48 -0.77 -0.50 -0.50 -0.50 -0.50 -0.50 -0.72 -0.50 -0.72 -0.50 -0.50 -0.72 -0.50 -0.72 -0.72 -0.50 -0.72 -0.72 -0.50 -0.72 -0.25 -0.92 -0.50 -0.50 -0.72 -0.50 -0.50 -0.72 -0.50 -0.50 -0.72 -0.50 -0.72 -0.50 -0.50 -0.72 -0.50 -0.50 -0.50 -0.50 -0.50 -0.50 -0.72 -0.50 -0.5 | HAX 16.2 3.2 0 9.5 0 0 6.8 0 0 6.8 0 0 3.7 15.8 -99 0 3.5 -99 8.9 8.9 6.2 5 32.4 13.2 0 13.2 5 32.4 13.2 0 13.2 5 13.2 13. | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 -99 17.1 31 -99 142 177 28.4 15.7 48.9 34.6 135 22.7 16 21.8 112 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 -99 22.4 23 -99 198 17.6 46.8 37.4 62.9 24.4 74.8 2.1 30 19.7 221 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 1 12.8 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 13 -99 11.3 10.6 10 28.5 19 1.8 0 5 3.5 15.8 7.5 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 0 10.2 33.5 15.3 0 8.7 11.8 -99 57.6 36.1 0.6 59.6 73 16 0 0 6 2 2 2 2 2 2 2 2 2 2 2 2 2 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 14 29 0 14 29 0 14 29 0 388 30 9.7 -99 48 17 6.6 59 21 53 0 0 0 21 | KAX 32 28 13 64 63 -999 377 166 38 4.6 25 53 -999 68 0 0 886 112 64 31 237 9.2 10 | KAY 54 87 18 -99 47 61 46 41 69 124 -99 84 54 47 38 46 45 117 48 104 32 48 | KAZ 25 55 27 142 93 -99 16 21 7.7 47 68 -99 121 87 40 123 5.8 15 138 6.4 115 58 30 23 145 | LAX 0 22 5.1 4 -99 4.8 -99 4.8 -99 -99 7.5 9.6 0 5.9 64 4.4 37 16 30 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 12.8 47.8 47.8 -99 91.2 34.3 18.5 12.6 41 43 0 36.7 61.6 45.7 | 29.1 36 18.4 0 8.9 2.8 10.5 -99 21 -99 21 -99 0 61 -99 3.9 3.5 6.5 222 55 18.4 0 0 15.2 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036072 9036081 9036085 9036187 9036151 9036152 9036147 9036152 9036147 9036252 9036257 9036257 9036259 9036261 9036262 9036264 9036272 9036281 9036308 9036310 9036322 9036323 9036336 | LON 36.43 36.63 36.63 36.25 36.02 36.42 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.68 36.77 36.68 36.23 36.08 36.70 36.77 36.10 36.77 36.10 36.77 36.38 36.23 36.32 36.32 36.32 36.32 36.32 36.32 36.32 36.32 | LAT - 0. 72 - 0. 58 - 0. 50 - 0. 98 - 0. 35 - 0. 30 - 0. 65 - 0. 13 - 0. 65 - 0. 47 - 0. 03 - 0. 72 - 0. 72 - 0. 25 - 0. 25 - 0. 27 - 0. 27 - 0. 65 - 0. 50 - 0. 48 - 0. 73 - 0. 92 - 0. 73 - 0. 20 - 0. 77 - 0. 35 - 0. 20 - 0. 77 - 0. 20 - 0. 77 - 0. 20 - 0. 20 - 0. 77 - 0. 20 - 0. 20 - 0. 20 - 0. 20 - 0. 27 - 0. 20 - 0. 20 | HAX 16.2 3.2 0 9.5 0 0 6.8 0 0 0 0 3.7 15.8 -99 0 3.5 -99 8.9 8.9 6.2 5 32.4 13.2 0 0 18.2 21.1 7.8 -99 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 -99 17.1 31 -99 142 177 28.4 15.7 48.9 34.6 135 22.7 16 21.8 112 -99 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 -99 22.4 23 -99 198 17.6 46.8 37.4 62.9 24.4 74.8 2.1 30 19.7 221 -99 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 12.3 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 0 13 -99 11.3 10.6 10 28.5 19 1.8 0 5 3.5 15.8 7.5 15.2 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 7 33.5 15.3 0 8.7 11.8 -99 57.6 36.1 0.6 59.6 57.6 36.1 0.6 59.6 59.6 59.6 59.6 59.6 59.6 59.6 59 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 14 29 0 14 29 0 38 30 9.7 -99 48 17 6.6 59 21 53 0 0 22 4 8 21 53 0 0 0 24 29 21 53 | KAX 32 28 13 64 63 -999 377 166 38 4.6 25 53 -999 68 0 0 866 18 31 12 64 31 237 9.2 10 24 72 36 | KAY 54 87 18 -99 47 61 46 41 69 124 -99 84 54 47 297 38 46 45 117 48 104 32 48 26 183 44 | KAZ 25 55 27 142 93 -99 16 21 7.7 47 68 -99 121 87 40 170 123 5.8 15 138 6.4 115 58 30 23 145 124 | LAX 0 22 5.1 14 58 0 4.8 -99 4.8 -99 7.5 9.6 0 5.9 69 -99 7.5 9.6 0 5.9 64 4.4 37 16 30 8.4 -99 33 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 12.8 47.8 47.8 47.8 47.8 47.8 12.6 41 43 0 36.7 61.6 45.7 -99 54.9 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 -99 0 61 -99 3.9 3.5 6.5 222 55 18.4 0 0 15.2 19.8 -99 60 |
| Oct | 9036002 9036025 9036034 9036061 9036072 9036072 9036081 9036085 9036187 9036151 9036152 9036147 9036152 9036252 9036257 9036257 9036261 9036262 9036264 9036272 9036281 9036308 9036310 9036312 9036323 | LON 36.43 36.63 36.63 36.25 36.02 36.42 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.68 36.77 36.68 36.23 36.08 36.70 36.77 36.10 36.77 36.10 36.77 36.38 36.23 36.32 36.45 36.52 36.63 36.52 36.52 36.63 36.52 37.552 36.52 37.552 37.552 37.552 37.552 37.552 37.552 37.5 | LAT -0.72 -0.58 -0.50 -0.98 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.92 -0.72 -0.25 -0.92 -0.50 -0.50 -0.48 -0.50 -0.48 -0.50 -0.48 -0.73 -0.50 -0.48 -0.73 -0.50 -0.48 -0.73 -0.50 -0.48 -0.73 -0.50 -0.48 -0.77 -0.50 -0.50 -0.50 -0.50 -0.50 -0.72 -0.50 -0.72 -0.50 -0.50 -0.72 -0.50 -0.72 -0.72 -0.50 -0.72 -0.72 -0.50 -0.72 -0.25 -0.92 -0.50 -0.50 -0.72 -0.50 -0.50 -0.72 -0.50 -0.50 -0.72 -0.50 -0.72 -0.50 -0.50 -0.72 -0.50 -0.50 -0.50 -0.50 -0.50 -0.50 -0.72 -0.50 -0.5 | HAX 16.2 3.2 0 9.5 0 0 6.8 0 0 0 0 3.7 15.8 -99 0 3.5 -99 8.9 8.9 6.2 5 32.4 13.2 0 0 18.2 21.1 7.8 -99 -99 -99 | HAY 26.9 55.6 13.2 126 38.6 21.4 22.8 14.7 25.5 23.2 8.5 14.9 -99 17.1 31 -99 142 177 28.4 15.7 48.9 34.6 135 22.7 16 21.8 112 -99 -99 -99 -99 -99 | HAZ 52.7 66.4 32.8 142 61.1 23.8 44 34.5 23.2 10.3 0 40 -99 22.4 23 -99 198 17.6 46.8 37.4 62.9 24.4 74.8 2.1 30 19.7 221 -99 | IAX -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAY -99 -99 -99 -99 -99 -99 -99 -99 -99 -9 | IAZ - 99 - 99 - 99 - 99 - 99 - 99 - 99 - 9 | JAX 1 12.8 12.3 0 4.5 25.9 0 8 29.1 11.9 0 4 13 -99 11.3 10.6 10 28.5 19 1.8 0 5 3.5 15.8 7.5 15.2 7 | JAY 22.3 45.1 11.7 0 45.9 16.6 0 8 7 33.5 15.3 0 8.7 11.8 -99 57.6 36.1 0.6 59.6 57.6 36.1 0.6 59.6 59.6 59.6 59.6 59.6 59.6 59.6 59 | JAZ 53 30 4.7 8.6 11 23 33 1.5 0 14 29 0 14 29 0 38 30 9.7 -99 48 17 6.6 59 21 53 0 0 0 22 4 29 21 53 0 0 0 22 1.5 5 32 1.5 | KAX 32 28 13 64 63 -999 377 166 386 25 53 -999 68 0 0 886 112 64 311 122 64 311 2377 9.2 100 24 72 36 299 | KAY 54 87 18 -99 47 61 46 41 69 124 -99 84 54 47 297 38 466 411 69 124 -99 84 54 477 38 466 45 117 48 104 32 48 26 183 | KAZ 25 55 27 142 93 -99 16 12 21 7.7 47 68 -99 121 87 40 170 123 5.8 138 6.4 115 58 30 23 145 124 17 | LAX 0 22 5.1 14 58 0 4.8 -99 4.8 -99 7.5 9.6 0 5.9 69 -99 7.5 9.6 0 5.9 64 4.4 37 16 30 8.4 -99 33 49 | LAY 29.8 15.3 20.7 0 3.4 22.4 5.9 6.5 -99 43.6 -99 43.6 -99 12.8 47.8 -99 91.2 34.3 18.5 12.6 41 43 0 36.7 61.6 45.7 -99 54.9 17.5 | 29.1 36 18.4 0 8.9 2.8 10.5 15.5 -99 21 -99 -99 0 61 -99 3.9 3.5 6.5 222 55 18.4 0 0 15.2 19.8 -99 60 40 |

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| Nov | ID | LON | LAT | HBX | HBY | HBZ | IBX | IBY | IBZ | JBX | JBY | JBZ | квх | KBY | KBZ | LBX | LBY | LBZ |
|----------|--|--|---|---|--|---|--|---|--|---|---|---|--|---|---|--|---|---|
| | 9036002 | 36.43 | -0.72 | 38.9 | 0 | 0 | 1.9 | 43.3 | 7.5 | 28.3 | 3.5 | 27 | 67 | 52 | 37 | 15 | 6.1 | 2 |
| | 9036025 | 36.63 | -0.58 | 111 | 42 | 63.3 | 30 | 78.1 | 14.6 | 29.1 | 18.6 | 48 | 78 | 98 | 16 | 15 | 23.2 | 31.4 |
| | 9036034 | 36.33 | -0.50 | 23.7 | 71.7 | 13 | 0 | 27.4 | 11.2 | 19.3 | 5.9 | 68 | 49 | 81 | 55 | 30 | 17.9 | 0 |
| | 9036061 | 36.63 | -0.98 | 161 | 144 | 30.1 | 66 | 64.2 | 12 | -99 | -99 | -99 | 198 | 84 | 40 | 37 | 21.5 | 14.5 |
| | 9036072 | 36.25 | -0.35 | 70.5 | 34 | 27 | 23 | 29.9 | 6.8 | 9.5 | 75.9 | 32 | 130 | 52 | 24 | 51 | 18.8 | 5.7 |
| | 9036076 | 36.02 | -0.30 | 34.9 | 48.3 | 30.8 | -99 | -99 | -99 | 32.7 | 27 | 27 | -99 | -99 | -99 | 36 | 15.7 | 4.7 |
| | 9036081 | 36.42 | -0.65 | 60.2 | 70 | 42 | 4.2 | 27.4 | 1.1 | 6.9 | 5.4 | 31 | 60 | 54 | 36 | 10 | 17.4 | 10.8 |
| | 9036085 | 36.77 | -0.13 | 83 | 88.5 | 21.5 | 9 | 35 | 36.1 | 31.5 | 20.5 | 43 | 65 | 77 | 58 | 31 | 17.8 | 4 |
| | 9036109 | 36.38 | -0.65 | 41.7 | 54.7 | 12.3 | 6.1 | 38.5 | 18.9 | 9.6 | 0 | 68 | 74 | 68 | 48 | -99 | -99 | -99 |
| | 9036147 | 36.20 | -0.47 | 30.6 | 45.9 | 0 | 0 | 39.6 | 7.9 | 10.4 | 6.1 | 58 | 85 | 63 | 28 | 6.8 | 8 | 0 |
| | 9036151 | 36.17 | -0.03 | 115 | 46.4 | 28.7 | 92 | 22.9 | 3.7 | 3 | 9.5 | 32 | 30 | 101 | 50 | 9 | 25.5 | 0 |
| | 9036152 | 36.65 | -0.72 | 92.3 | 102 | 35.3 | 28 | 39.4 | 3.2 | 34 | 12.5 | 46 | 117 | 122 | 56 | -99 | -99 | -99 |
| | 9036164 | 36.68 | -0.72 | 125 | 111 | 23.4 | -99 | -99 | -99 | 59.1 | 33.5 | 129 | -99 | -99 | -99 | 53 | 36.9 | 51.8 |
| | 9036243 | 36.23 | -0.25 | 109 | 53.4 | 71.9 | 143 | 81.5 | 10.5 | 12.1 | 7.1 | 73 | 58 | 131 | 62 | 56 | 27 | 31.9 |
| | 9036252 | 36.08 | -0.25 | 58.9 | 21.5 | 39 | 26 | 35.2 | 10 | 12.8 | 2.5 | 81 | 120 | 68 | 61 | -99 | -99 | -99 |
| | 9036257 | 36.70 | -0.92 | -99 | -99 | -99 | 18 | 24.3 | 0 | -99 | -99 | -99 | -99 | -99 | -99 | -99 | -99 | -99 |
| | 9036259 | 36.77 | -0.72 | 272 | 178 | 76 | 86 | 108 | 39.5 | 96 | 104 | 144 | 306 | 160 | 96 | 163 | 93.6 | 61 |
| | 9036261 | 36.10 | -0.27 | 43 | 27.6 | 22.9 | 29 | 34.8 | 15.2 | 15.7 | 7.1 | 73 | 77 | 80 | 65 | 58 | 11.8 | 12.4 |
| | 9036262 | 36.45 | -0.65 | 52.4 | 62.8 | 34.7 | 1.8 | 17.8 | 7 | 16 | 0 | 42 | 44 | 92 | 52 | 13 | 22 | 14.2 |
| | 9036264 | 36.52 | -0.50 | 57.9 | 51.3 | 68.2 | 46 | 62.1 | 14.9 | 28.8 | 4.5 | 55 | 60 | 90 | 28 | 22 | 36.8 | 13.6 |
| | 9036272 | 36.63 | -0.48 | -99 | -99 | -99 | 63 | 93.4 | 18.6 | 29.5 | 14 | 88 | 194 | 99 | 63 | 34 | 62.5 | 44 |
| | 9036281 | 36.45 | -0.73 | 91.9 | 82.2 | 31.2 | 6.2 | 17 | 5 | 46.4 | 4.3 | 40 | 75 | 44 | 63 | -99 | -99 | -99 |
| | 9036308 | 36.90 | -0.92 | 194 | 151 | 68.2 | 47 | 184 | 129.5 | 77.1 | 94.8 | 128 | 269 | 95 | 120 | -99 | -99 | -99 |
| | 9036310 | 36.03 | -0.35 | 33.5 | 58 | 18.8 | 33 | 12 | 20.5 | 26 | 10.5 | 67 | 59 | 82 | 28 | 58 | 29.2 | 6.5 |
| | 9036312 | 36.53 | -0.20 | 85 | 55.5 | 62.5 | 55 | 59 | 11.3 | 25.5 | 5.3 | 26 | 110 | 69 | 58 | 18 | 38.5 | 12.5 |
| | 9036322 | 36.32 | -0.77 | 78.7 | 59.5 | 56.4 | 2.3 | 19.6 | 3.5 | 25.5 | 0 | 20 | 58 | 29 | 44 | 25 | 15.5 | 0 |
| | 9036323 | 36.82 | -0.70 | 326 | 191 | 164 | 140 | 140 | 150.6 | 57.7 | 81.6 | 106 | 247 | 129 | 46 | -99 | -99 | -99 |
| | 9036336 | 36.28 | -0.27 | -99 | -99 | -99 | 85 | 119 | 22.5 | 20 | 0 | 8.1 | 66 | 65 | 39 | 63 | 48.8 | 25.5 |
| | 9036337 | 36.03 | -0.58 | -99 | -99 | -99 | 27 | 25 | 14.1 | 7.3 | 8.3 | 75 | 84 | 108 | 106 | 15 | 1.5 | 3 |
| | 9036343 | 36.49 | -0.52 | 40 | 87.8 | 29.6 | 9.2 | 66.6 | 18 | 15.3 | 5.8 | 34 | 67 | 60 | 29 | -99 | -99 | -99 |
| D | | | | | | | | | | | | | | | | | | |
| Dec | ID | LON | LAT | HCX | HCY | HCZ | ICX | ICY | ICZ | JCX | JCY | JCZ | KCX | KCY | KCZ | LCX | LCY | LCZ |
| Dec | ID 9036002 | LON 36.43 | LAT -0.72 | HCX 16.3 | HCY 2.1 | HCZ 0 | ICX -99 | ICY -99 | ICZ -99 | JCX 3.4 | ЈСХ 0 | JCZ 3.3 | KCX 49 | ксч 15 | KCZ 34 | 12 | LCY 1 | LCZ 0 |
| Dec | | | -0.72 | | | - | | | | | | | | | | | | |
| Dec | 9036002 | 36.43 | -0.72 | 16.3 | 2.1 | 0 | -99 -99 | -99 | -99 | 3.4 | 0 | 3.3 | 49 | 15 | 34 | 12 | 1 | 0 |
| Dec | 9036002 9036025 | 36.43 36.63 | -0.72 -0.58 | 16.3 25.7 | 2.1 3.6 | 0 | -99 -99 6.5 | -99 -99 | -99 -99 | 3.4 | 0 7.4 | 3.3 | 49 46 | 15 42 | 34 29 | 12 1.8 | 1 0 | 0 15.3 |
| Dec | 9036002 9036025 9036034 | 36.43 36.63 36.33 | -0.72 -0.58 -0.50 | 16.3 25.7 0 | 2.1 3.6 0 | 0 0 2.4 | -99 -99 6.5 | -99 -99 36.4 49.9 | -99 -99 19.2 | 3.4 2 0 | 0 7.4 7.2 | 3.3 3 0 | 49 46 51 | 15 42 8.4 | 34 29 16 | 12 1.8 15 | 1 0 4.1 | 0 15.3 0 |
| Dec | 9036002 9036025 9036034 9036061 | 36.43 36.63 36.33 36.63 | -0.72 -0.58 -0.50 -0.98 | 16.3 25.7 0 18.3 | 2.1 3.6 0 6 | 0 0 2.4 10 | -99 -99 6.5 13 | -99 -99 36.4 49.9 | -99 -99 19.2 4 | 3.4 2 0 | 0 7.4 7.2 0 | 3.3 3 0 3 | 49 46 51 83 | 15 42 8.4 104 | 34 29 16 53 | 12 1.8 15 27 | 1 0 4.1 0 | 0 15.3 0 0 |
| Dec | 9036002 9036025 9036034 9036061 9036072 | 36.43 36.63 36.33 36.63 36.25 | -0.72 -0.58 -0.50 -0.98 -0.35 | 16.3 25.7 0 18.3 102 | 2.1 3.6 0 6 3.3 | 0 0 2.4 10 9.9 | -99 -99 6.5 13 16 | -99 -99 36.4 49.9 52.6 | -99 -99 19.2 4 6.2 | 3.4 2 0 94.4 7.4 | 0 7.4 7.2 0 31.6 | 3.3 3 0 3 68 | 49 46 51 83 83 | 15 42 8.4 104 28 | 34 29 16 53 59 | 12 1.8 15 27 4.6 | 1 0 4.1 0 8.9 | 0 15.3 0 0 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 | 36.43 36.63 36.33 36.63 36.25 36.02 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 | 16.3 25.7 0 18.3 102 10.3 | 2.1 3.6 0 6 3.3 0 | 0 0 2.4 10 9.9 0 | -99 -99 6.5 13 16 -99 | -99 -99 36.4 49.9 52.6 -99 3.1 | -99 -99 19.2 4 6.2 -99 | 3.4 2 0 94.4 7.4 | 0 7.4 7.2 0 31.6 2.4 | 3.3 3 0 3 68 1.1 | 49 46 51 83 83 -99 | 15 42 8.4 104 28 -99 | 34 29 16 53 59 -99 | 12 1.8 15 27 4.6 1.6 | 1 0 4.1 0 8.9 2.5 | 0 15.3 0 0 0 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 | 16.3 25.7 0 18.3 102 10.3 12.2 | 2.1 3.6 0 6 3.3 0 1.4 | 0 0 2.4 10 9.9 0 3.4 | -99 -99 6.5 13 16 -99 29 6.5 | -99 -99 36.4 49.9 52.6 -99 3.1 | -99 -99 19.2 4 6.2 -99 0 | 3.4 2 0 94.4 7.4 0 | 0 7.4 7.2 0 31.6 2.4 10.8 | 3.3 3 0 3 68 1.1 3.2 | 49 46 51 83 -99 33 | 15 42 8.4 104 28 -99 13 | 34 29 16 53 59 -99 51 | 12 1.8 15 27 4.6 1.6 17 | 1 0 4.1 0 8.9 2.5 5 | 0 15.3 0 0 0 0 0 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 | 16.3 25.7 0 18.3 102 10.3 12.2 30.2 | 2.1 3.6 0 6 3.3 0 1.4 0.5 | 0 0 2.4 10 9.9 0 3.4 0.7 | -99 -99 6.5 13 16 -99 29 6.5 7.2 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 | -99 -99 19.2 4 6.2 -99 0 5 | 3.4 2 0 94.4 7.4 0 24 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 | 3.3 3 0 3 68 1.1 3.2 13 | 49 46 51 83 83 -99 33 32 | 15 42 8.4 104 28 -99 13 0 | 34 29 16 53 59 -99 51 44 | 12 1.8 15 27 4.6 1.6 17 0 | 1 0 4.1 0 8.9 2.5 5 0 | 0 15.3 0 0 0 0 0 0 0 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 | -0.72 -0.58 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 | 16.3 25.7 0 18.3 102 10.3 12.2 30.2 -99 | 2.1 3.6 0 6 3.3 0 1.4 0.5 -99 0 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 10.8 41.6 | -99 -99 19.2 4 6.2 -99 0 5 | 3.4 2 0 94.4 7.4 7.4 0 24 -99 9.7 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 | 3.3 3 0 3 68 1.1 3.2 13 -99 0 | 49 46 51 83 83 -99 33 32 72 | 15 42 8.4 104 28 -99 13 0 16 6.1 | 34 29 16 53 59 -99 51 44 42 | 12 1.8 15 27 4.6 1.6 1.6 17 0 -99 | 1 0 4.1 0 8.9 2.5 5 5 0 -99 4.6 | 0 15.3 0 0 0 0 0 0 0 -99 0 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 | 36.43 36.63 36.33 36.25 36.02 36.42 36.77 36.38 36.20 36.17 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 | 16.3 25.7 0 18.3 102 10.3 12.2 30.2 -99 42.6 7 | 2.1 3.6 0 6 3.3 0 1.4 0.5 -99 0 0 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 10.8 41.6 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 | 3.4 2 0 94.4 7.4 0 24 -99 9.7 5.5 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 | 3.3 3 0 3 68 1.1 3.2 13 -99 0 | 49 46 51 83 83 -99 33 32 72 27 | 15 42 8.4 104 28 -99 13 0 16 6.1 | 34 29 16 53 59 -99 51 44 42 36 | 12 1.8 15 27 4.6 1.6 1.6 17 0 -99 3.6 | 1 0 4.1 0 8.9 2.5 5 5 0 -99 4.6 | 0 15.3 0 0 0 0 0 0 0 -99 0 0 0 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 | 16.3 25.7 0 18.3 102 10.3 12.2 30.2 -99 42.6 7 8.2 | 2.1 3.6 0 6 3.3 0 1.4 0.5 -99 0 0 3.5 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 10.8 41.6 22 32.2 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 | 3.4 2 0 94.4 7.4 0 24 -99 9.7 5.5 34 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 | 3.3 3 0 3 68 1.1 3.2 13 -99 0 0 36 | 49 46 51 83 -99 33 32 72 72 27 19 61 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 | 34 29 16 53 59 -99 51 44 42 36 0 43 | 12 1.8 15 27 4.6 1.6 1.6 1.7 0 -99 3.6 0 2.1 | 1 0 4.1 0 8.9 2.5 5 0 -99 4.6 0 0.4 | 0 15.3 0 0 0 0 -99 0 0 10.7 |
| Dec | 9036002 9036025 9036034 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 | 16.3 25.7 0 18.3 102 10.3 12.2 30.2 -99 42.6 7 8.2 -99 | 2.1 3.6 6 3.3 0 1.4 0.5 -99 0 0 3.5 -99 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 6.7 11 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 10.8 41.6 22 32.2 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 | 3.4 2 0 94.4 7.4 0 24 -99 9.7 5.5 34 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 25 40.9 | 3.3 0 3 68 1.1 3.2 13 -99 0 0 36 0 0 | 49 46 51 83 -99 33 32 72 27 27 19 61 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 111 | 34 29 16 53 59 -99 51 44 42 36 0 43 -99 | 12 1.8 15 27 4.6 1.6 1.6 1.7 0 -99 3.6 0 2.1 | 1 0 4.1 0 8.9 2.5 5 5 0 -99 4.6 0 0.4 | 0 15.3 0 0 0 0 -99 0 0 10.7 3.2 |
| Dec | 9036002 9036025 9036034 9036072 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 | 16.3 25.7 0 18.3 102 10.3 12.2 30.2 -99 42.6 7 8.2 -99 | 2.1 3.6 0 6 3.3 0 1.4 0.5 -99 0 0 3.5 -99 0 0 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 0 0 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 6.7 11 52 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 10.8 41.6 22 32.2 40 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 0 | 3.4 2 0 94.4 7.4 -99 9.7 5.5 34 7.7 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 25 40.9 0 | 3.3 0 3 68 1.1 3.2 13 -99 0 0 36 0 11 | 49 46 51 83 83 -99 33 32 72 27 27 19 61 -99 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 111 -99 | 34 29 16 53 59 -99 51 44 42 36 0 43 -99 | 12 1.8 15 27 4.6 1.6 17 0 -99 3.6 0 2.1 11 0 | 1 0 4.1 0 8.9 2.5 5 0 -99 4.6 0 0.4 11.1 | 0 15.3 0 0 0 0 -99 0 0 10.7 3.2 0 |
| Dec | 9036002 9036025 9036034 9036072 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.25 | 16.3 25.7 0 18.3 102 10.3 12.2 30.2 -99 42.6 7 8.2 -99 18.6 | 2.1 3.6 0 6 3.3 0 1.4 0.5 -99 0 0 3.5 -99 0 0 0 3.5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 0 0 -99 0 0 0 0 0 0 0 0 0 0 0 0 0 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 6.7 11 52 14 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 10.8 41.6 22 32.2 40 51.5 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 0 0 0 | 3.4 2 0 94.4 7.4 -99 9.7 5.5 34 7.7 26.4 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 25 40.9 0 | 3.3 3 0 3 68 1.1 3.2 -99 0 0 36 0 11 0 | 49 46 51 83 -99 33 32 72 27 27 19 61 -99 55 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 111 -99 16 | 34 29 16 53 59 -99 51 44 42 36 0 43 -99 7.6 24 | 12 1.8 15 27 4.6 1.6 17 0 -99 3.6 0 2.1 11 0 | 1 0 4.1 0 8.9 2.5 5 0 -99 4.6 0 0.4 11.1 | 0 15.3 0 0 0 0 -99 0 0 0 10.7 3.2 0 -99 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 9036252 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 | -0.72 -0.58 -0.50 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.25 -0.92 | 16.3 25.7 0 18.3 102 10.3 12.2 30.2 -99 42.6 7 8.2 -99 18.6 2.5 -99 | 2.1 3.6 0 6 3.3 0 1.4 0.5 -99 0 0 3.5 -99 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 0 0 -99 0 0 0 0 0 0 0 0 0 0 0 0 0 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 6.7 11 52 44 -99 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 10.8 41.6 22 32.2 40 51.5 44.5 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 0 0 0 99 | 3.4 2 0 94.4 7.4 -99 9.7 5.5 34 7.7 26.4 0 -99 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 25 40.9 0 0 0 | 3.3 3 0 3 68 1.1 3.2 -99 0 0 36 0 11 0 | 49 46 51 83 -99 33 32 72 27 27 19 61 -99 55 46 -99 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 111 -99 16 5.2 | 34 29 16 53 59 -99 51 44 42 36 0 43 -99 7.6 24 -99 | 12 1.8 15 27 4.6 1.6 17 0 -99 3.6 0 2.1 11 11 0 -99 -99 -99 | 1 0 4.1 2.5 5 0 -99 4.6 0 0.4 11.1 0 -99 | 0 15.3 0 0 0 0 -99 0 0 0 10.7 3.2 0 -99 -99 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 9036252 9036257 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 | -0.72 -0.58 -0.50 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.25 -0.92 | 16.3 25.7 0 18.3 102 10.3 12.2 30.2 -99 42.6 7 8.2 -99 18.6 2.5 -99 18.6 | 2.1 3.6 0 6 3.3 0 1.4 0.5 -99 0 0 3.5 -99 0 0 0 0 0 -99 11.7 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 0 -99 0 0 0 0 -99 | -99 -99 6.5 13 -99 29 6.5 7.2 20 5.2 6.7 11 52 6.7 11 52 14 -99 23 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 10.8 41.6 22 32.2 40 51.5 44.5 -99 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 0 0 0 99 | 3.4 2 0 94.4 7.4 -99 9.7 5.5 34 7.7 26.4 0 -99 45.2 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 25 40.9 0 0 0 -99 28.4 | 3.3 3 0 3 68 1.1 3.2 13 -99 0 0 0 36 0 11 0 -99 | 49 46 51 83 -99 33 32 72 27 19 61 -99 55 46 -99 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 111 -99 16 5.2 -99 | 34 29 16 53 59 -99 51 44 42 36 0 43 -99 7.6 24 -99 | 12 1.8 15 27 4.6 1.6 1.7 0 -99 3.6 0 2.1 11 0 -99 -99 -99 4.2 | 1 0 4.1 0 8.9 2.5 5 0 -99 4.6 0 0.4 11.1 0 0.4 11.1 | 0 15.3 0 0 0 0 -99 0 0 0 10.7 3.2 0 -99 -99 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 9036252 9036257 9036259 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.25 -0.92 -0.72 -0.72 | 16.3 25.7 0 18.3 102 10.3 12.2 30.2 -99 42.6 7 8.2 -99 18.6 2.5 -99 102 7.7 | 2.1 3.6 0 6 3.3 0 1.4 0.5 -99 0 0 3.5 -99 0 0 0 0 -99 11.7 0 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 -99 0 0 0 -99 0 0 0 -99 2.9 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 6.7 11 52 6.7 11 52 14 -99 23 13 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 10.8 41.6 22 32.2 40 51.5 44.5 -99 87.2 27.3 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 0 0 0 -99 4.7 | 3.4 2 0 94.4 7.4 -99 9.7 5.5 34 7.7 26.4 0 -99 45.2 2.8 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 25 40.9 0 0 0 -99 28.4 1.6 | 3.3 3 0 3 68 1.1 3.2 13 -99 0 0 36 0 11 0 -99 0 0 0 0 0 0 0 0 0 0 0 0 0 | 49 46 51 83 -99 33 22 72 27 19 61 -99 55 46 -99 156 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 111 -99 16 5.2 -99 56 | 34 29 16 53 59 -99 51 44 42 36 0 43 -99 7.6 24 -99 136 | 12 1.8 15 27 4.6 1.6 1.7 0 -99 3.6 0 2.1 11 0 -99 -99 -99 4.2 | 1 0 4.1 0 8.9 2.5 5 0 -99 4.6 0 0.4 11.1 0 -99 -99 20.9 | 0 15.3 0 0 0 0 -99 0 10.7 3.2 0 -99 -99 25.8 2.6 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 9036252 9036257 9036259 9036261 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.45 | -0.72 -0.58 -0.50 -0.98 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.92 -0.72 -0.72 -0.72 -0.5 | 16.3 25.7 0 18.3 102 10.3 12.2 30.2 -99 42.6 7 8.2 -99 18.6 2.5 -99 102 7.7 7.7 | 2.1 3.6 0 6 3.3 0 1.4 0.5 -99 0 0 3.5 -99 0 0 0 -99 11.7 0 0.5 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 -99 0 0 -99 0 0 -99 0 0 0 0 -99 0 0 0 0 -99 0 0 0 -99 0 0 -99 0 0 -99 0 0 -99 0 -99 0 0 -99 0 0 -99 0 0 -99 0 0 -99 0 0 -99 0 0 -99 0 0 -99 0 0 0 -99 0 0 0 0 0 0 0 0 0 0 0 0 0 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 6.7 11 52 14 -99 23 13 6.3 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 10.8 41.6 22 32.2 40 51.5 44.5 -99 87.2 27.3 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 0 0 0 9 9 9 4.7 3.6 | 3.4 2 0 94.4 7.4 -99 9.7 5.5 34 7.7 26.4 0 -99 45.2 2.8 3.9 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 25 40.9 0 0 -99 28.4 1.6 7.6 | 3.3 3 0 3 68 1.1 3.2 13 -99 0 0 366 0 111 0 -99 0 0 2.6 | 49 46 51 83 -99 33 22 72 27 19 61 -99 55 46 -99 156 43 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 111 -99 16 5.2 -99 56 4.7 | 34 29 16 53 59 -99 51 44 42 36 43 -99 7.6 24 -99 136 15 23 | 12 1.8 15 27 4.6 1.6 17 0 -99 3.6 0 2.1 11 0 -99 -99 4.2 1.4 | 1 0 4.1 0 8.9 2.5 5 0 -99 4.6 0 0.4 11.1 0 -99 -99 20.9 20.9 0.3 | 0 15.3 0 0 0 0 -99 0 10.7 3.2 0 -99 -99 25.8 2.6 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036109 9036147 9036151 9036152 9036164 9036243 9036252 9036257 9036259 9036261 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.45 | -0.72 -0.58 -0.50 -0.98 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.25 -0.27 -0.50 | $\begin{array}{c} 16.3\\ 25.7\\ 0\\ 18.3\\ 102\\ 10.3\\ 12.2\\ 30.2\\ -99\\ 42.6\\ 7\\ 8.2\\ -99\\ 18.6\\ 2.5\\ -99\\ 102\\ 7.7\\ 7.7\\ 0\\ \end{array}$ | 2.1 3.6 0 6 3.3 0 1.4 0.5 -99 0 0 0 3.5 -99 0 0 0 -99 11.7 0 0.5 0 0 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 -99 0 0 0 -99 0 0 0 -99 0 0 0 0 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 6.7 11 52 14 -99 23 13 6.3 8.5 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 10.8 41.6 22 32.2 40 51.5 44.5 -99 87.2 27.3 7.2 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 0 0 -99 4.7 3.6 6.5 28.5 | 3.4 2 0 94.4 7.4 -99 9.7 5.5 34 7.7 26.4 0 -99 45.2 2.8 3.9 | $\begin{array}{c} 0\\ 7.4\\ 7.2\\ 0\\ 31.6\\ 2.4\\ 10.8\\ 0.2\\ -99\\ 0\\ 0\\ 25\\ 40.9\\ 0\\ 0\\ -99\\ 28.4\\ 1.6\\ 7.6\\ 0\\ \end{array}$ | 3.3 3 0 3 68 1.1 3.2 13 -99 0 0 36 0 11 0 -99 0 0 2.6 2 | 49 46 51 83 83 -99 33 22 72 27 19 61 -99 55 46 -99 156 43 46 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 111 -99 16 5.2 -99 56 4.7 24 | 34 29 16 53 59 -99 51 44 42 36 43 -99 7.6 24 -99 136 15 23 | 12 1.8 15 27 4.6 1.6 17 0 -99 3.6 0 2.1 11 0 -99 -99 4.2 1.4 0 | 1 0 4.1 0 8.9 2.5 5 0 -99 4.6 0 0.4 11.1 0 -99 -99 20.9 0.3 3.4 | 0 15.3 0 0 0 0 -99 0 0 10.7 3.2 0 -99 -99 25.8 2.6 0 3 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036081 9036181 9036147 9036151 9036152 9036164 9036243 9036257 9036257 9036251 9036261 9036264 | 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.77 36.10 36.45 36.52 36.63 | -0.72 -0.58 -0.50 -0.98 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.92 -0.72 -0.72 -0.50 -0.50 -0.48 | 16.3 25.7 0 18.3 102 10.3 12.2 30.2 -99 42.6 7 8.2 -99 18.6 2.5 -99 102 7.7 7.7 0 14.1 | 2.1 3.6 0 6 3.3 0 1.4 0.5 -99 0 0 3.5 -99 0 0 0 -99 11.7 0 0.5 0 8.8 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 -99 0 0 0 -99 0 0 0 -99 0 0 0 0 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 6.7 11 52 14 -99 23 13 6.3 8.5 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 10.8 41.6 22 32.2 40 51.5 44.5 -99 87.2 27.3 7.2 9.2 38.5 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 0 0 -99 4.7 3.6 6.5 28.5 5.8 | 3.4 2 0 94.4 7.4 -99 9.7 5.5 34 7.7 26.4 0 -99 45.2 2.8 3.9 7.3 | $\begin{array}{c} 0 \\ 7.4 \\ 7.2 \\ 0 \\ 31.6 \\ 2.4 \\ 10.8 \\ 0.2 \\ -99 \\ 0 \\ 0 \\ 25 \\ 40.9 \\ 0 \\ 0 \\ -99 \\ 28.4 \\ 1.6 \\ 7.6 \\ 0 \\ 20 \end{array}$ | 3.3 3 0 3 68 1.1 3.2 13 -99 0 0 36 0 11 0 -99 0 0 2.6 2 2 2 | 49 46 51 83 83 -99 33 27 27 27 19 61 -99 55 46 -99 156 43 46 -99 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 111 -99 16 5.2 -99 56 4.7 24 -99 | 34 29 16 53 59 99 51 44 42 36 43 -99 7.6 24 -99 136 15 23 -99 | 12 1.8 15 27 4.6 1.6 1.7 0 -99 3.6 0 2.1 11 11 0 -99 -99 4.2 1.4 0 0 | 1 0 4.1 0 8.9 2.5 5 0 -99 4.6 0 0.4 11.1 0 -99 -99 20.9 0.3 3.4 1 | 0 15.3 0 0 0 0 0 -99 0 0 0 10.7 3.2 0 -99 -99 25.8 2.6 0 3 3 2 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036081 9036187 9036151 9036152 9036164 9036243 9036252 9036257 9036251 9036261 9036264 9036272 9036281 | 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.77 36.10 36.45 36.52 36.63 36.45 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.25 -0.92 -0.72 -0.72 -0.50 -0.50 -0.50 -0.48 -0.73 | $\begin{array}{c} 16.3\\ 25.7\\ 0\\ 18.3\\ 102\\ 10.3\\ 12.2\\ 30.2\\ -99\\ 42.6\\ 7\\ 8.2\\ -99\\ 18.6\\ 2.5\\ -99\\ 102\\ 7.7\\ 7.7\\ 0\\ 102\\ 7.7\\ 7.7\\ 0\\ 14.1\\ 12.7 \end{array}$ | 2.1 3.6 0 6 3.3 0 1.4 0.5 -99 0 0 0 3.5 -99 0 0 0 -99 11.7 0 0.5 0 8.8 1.5 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 -99 0 0 0 -99 0 0 0 -99 0 0 0 0 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 6.7 11 52 14 -99 23 13 6.3 8.5 18 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 10.8 41.6 222 32.2 40 51.5 44.5 -99 87.2 27.3 7.2 9.2 38.5 8.1 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 0 0 -99 4.7 3.6 6.5 28.5 5.8 5.1 | 3.4 2 0 94.4 7.4 -99 9.7 5.5 34 7.7 26.4 0 -99 45.2 2.8 3.9 7.3 55.8 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 25 40.9 0 0 -99 28.4 1.6 7.6 0 20 1.8 | 3.3 3 0 3 68 1.1 3.2 13 -99 0 0 36 0 11 0 -99 0 0 2.6 2 2 2 | 49 46 51 83 83 -99 33 32 72 27 19 61 -99 55 46 -99 156 43 46 -99 52 63 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 111 -99 16 5.2 -99 56 4.7 24 -99 39 | 34 29 16 53 59 99 51 44 42 36 0 43 -99 7.6 24 -99 136 15 23 -99 34 28 | 12 1.8 15 27 4.6 1.6 1.7 0 -99 3.6 0 2.1 11 0 -99 -99 4.2 1.4 0 0 0 0 0 | 1 0 4.1 0 8.9 2.5 5 0 -99 4.6 0 0.4 11.1 0 -99 -99 20.9 0.3 3.4 1 8 0 | 0 15.3 0 0 0 0 0 0 -99 0 0 0 10.7 3.2 0 -99 -99 25.8 2.6 0 3 3 2 2 0 0 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036085 9036104 9036151 9036152 9036164 9036243 9036252 9036257 9036261 9036264 9036272 | 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.77 36.10 36.45 36.52 36.63 36.45 36.90 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.92 -0.72 -0.25 -0.92 -0.72 -0.50 -0.50 -0.48 -0.50 -0.48 -0.73 -0.92 | 16.3 25.7 0 18.3 102 10.3 12.2 30.2 -99 42.6 7 8.2 -99 18.6 2.5 -99 102 7.7 7.7 0 14.1 12.7 84.4 | 2.1 3.6 0 6 3.3 -99 0 0 3.5 -99 0 0 0 -99 11.7 0 0.5 0 8.8 1.5 0 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 -99 0 0 0 -99 2.9 0 0 0 0.3 8.9 1.6 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 6.7 11 52 14 -99 23 13 6.3 8.5 18 13 38 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 10.8 41.6 22 32.2 40 51.5 44.5 -99 87.2 27.3 7.2 9.2 38.5 8.1 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 0 0 -99 4.7 3.6 6.5 28.5 5.8 5.1 | 3.4 2 0 94.4 7.4 -99 9.7 5.5 34 7.7 26.4 0 -99 45.2 2.8 3.9 7.3 55.8 9.1 48.7 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 0 25 40.9 0 0 -99 28.4 1.6 7.6 0 20 1.8 15 | 3.3 3 0 3 68 1.1 3.2 13 -99 0 0 366 0 111 0 -99 0 0 2.6 2 2 0.8 0 0 0 0 0 0 0 0 0 0 0 0 0 | 49 46 51 83 83 -99 33 32 72 27 19 61 -99 55 46 -99 156 43 46 -99 52 63 | $ \begin{array}{c} 15\\ 42\\ 8.4\\ 104\\ 28\\ -99\\ 13\\ 0\\ 16\\ 6.1\\ 3.5\\ 111\\ -99\\ 16\\ 5.2\\ -99\\ 56\\ 4.7\\ 24\\ -99\\ 39\\ 21\\ \end{array} $ | 34 29 16 53 59 99 51 44 42 36 0 43 -99 7.6 24 -99 136 15 23 -99 34 28 | 12 1.8 15 27 4.6 1.6 1.7 0 -99 3.6 0 2.1 11 0 -99 4.2 1.4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 1 0 4.1 0 8.9 2.5 5 0 -99 4.6 0 0.4 11.1 0 -99 -99 20.9 0.3 3.4 1 8 | 0 15.3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036081 9036185 9036147 9036151 9036152 9036164 9036252 9036257 9036257 9036261 9036262 9036264 9036272 9036281 9036308 | 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.77 36.10 36.45 36.52 36.63 36.45 36.90 36.03 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.25 -0.92 -0.72 -0.25 -0.92 -0.72 -0.50 -0.50 -0.48 -0.50 -0.48 -0.73 -0.92 | $\begin{array}{c} 16.3\\ 25.7\\ 0\\ 18.3\\ 102\\ 10.3\\ 12.2\\ 30.2\\ -99\\ 42.6\\ 7\\ 8.2\\ -99\\ 18.6\\ 2.5\\ -99\\ 102\\ 7.7\\ 7.7\\ 0\\ 102\\ 7.7\\ 7.7\\ 0\\ 14.1\\ 12.7\\ 84.4\\ 4.5\\ \end{array}$ | 2.1 3.6 0 6 3.3 -99 0 0 0 3.5 -99 0 0 0 -99 11.7 0 0.5 0 8.8 1.5 0 0 0 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 -99 0 0 0 -99 2.9 0 0 0 0.3 8.9 1.6 0 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 6.7 11 52 14 -99 23 13 6.3 8.5 18 13 38 | -99 -99 36.4 49.9 52.66 -99 3.1 36.4 10.8 41.6 222 32.2 40 51.5 44.5 -99 87.2 27.3 7.2 9.2 38.5 8.1 144 16 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 0 0 -99 4.7 3.6 6.5 28.5 5.8 5.1 5.4 | 3.4 2 0 94.4 7.4 -99 9.7 5.5 34 7.7 26.4 0 -99 45.2 2.8 3.9 7.3 55.8 9.1 48.7 0 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 0 25 40.9 0 0 -99 28.4 1.6 7.6 0 20 1.8 15 0 | 3.3 3 0 3 68 1.1 3.2 13 -99 0 0 0 366 0 111 0 -99 0 0 2.6 2 2 0.8 0 4.5 | 49 46 51 83 83 -99 33 32 72 27 19 61 -99 55 46 -99 156 43 46 -99 52 63 161 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 111 -99 16 5.2 -99 56 4.7 24 -99 39 21 28 | 34 29 16 53 59 99 51 44 42 36 0 43 -99 7.6 24 -99 136 15 23 -99 34 28 116 | 12 1.8 15 27 4.6 1.6 17 0 -99 3.6 0 2.1 11 0 -99 4.2 1.4 0 0 0 0 1.4 0 0 0 1.5 1.6 0 0 2.1 1.1 0 0 0 2.1 1.1 0 0 0 0 2.1 1.1 0 0 0 0 0 0 0 0 0 0 0 0 0 | 1 0 4.1 0 8.9 2.5 5 0 -99 4.6 0 0.4 11.1 0 -99 20.9 0.3 3.4 1 8 0 0 33.3 | 0 15.3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036081 9036185 9036164 9036152 9036152 9036252 9036257 9036252 9036261 9036262 9036264 9036272 9036281 9036308 9036310 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.77 36.10 36.45 36.52 36.63 36.45 36.90 36.03 36.53 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.92 -0.72 -0.25 -0.92 -0.50 -0.48 -0.50 -0.48 -0.73 -0.92 -0.35 -0.20 | $\begin{array}{c} 16.3\\ 25.7\\ 0\\ 18.3\\ 102\\ 10.3\\ 12.2\\ 30.2\\ -99\\ 42.6\\ 7\\ 8.2\\ -99\\ 18.6\\ 2.5\\ -99\\ 102\\ 7.7\\ 7.7\\ 0\\ 102\\ 7.7\\ 7.7\\ 0\\ 14.1\\ 12.7\\ 84.4\\ 4.5\\ 43.6 \end{array}$ | 2.1 3.6 0 6 3.3 -99 0 0 0 3.5 -99 0 0 0 -99 11.7 0 0.5 0 8.8 1.5 0 0 22.7 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 -99 0 0 0 -99 0 0 0 0.3 8.9 1.6 0 5.5 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 6.7 11 52 6.7 11 52 14 -99 23 13 6.3 8.5 18 13 8.5 | -99 -99 36.4 49.9 52.69 -99 3.1 36.4 10.8 41.6 22 32.2 40 51.5 44.5 -99 87.2 27.3 7.2 9.2 38.5 8.1 144 16 16 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 0 -99 4.7 3.6 6.5 28.5 5.8 5.1 5.4 0.7 23.6 | 3.4 2 0 94.4 7.4 -99 9.7 5.5 34 7.7 26.4 0 -99 45.2 2.8 3.9 7.3 55.8 9.1 48.7 0 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 0 25 40.9 0 0 -99 28.4 1.6 7.6 0 20 1.8 15 0 0 | 3.3 3 0 3 68 1.1 3.2 13 -99 0 0 0 366 0 11 0 -99 0 0 2.6 2 2 0.8 0 4.5 0 0 | 49 46 51 83 83 -99 33 32 72 27 19 61 -99 55 46 -99 156 43 46 -99 52 63 161 52 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 111 -99 16 5.2 -99 56 4.7 24 -99 39 21 28 3.7 | 34 29 16 53 59 99 51 44 42 36 0 43 -99 136 15 23 -99 34 28 116 5 | 12 1.8 15 27 4.6 1.6 1.7 0 -99 3.6 0 2.1 11 0 -99 4.2 1.4 0 0 0 0 1.4 0 0 0 2.5 | 1 0 4.1 0 8.9 2.5 5 0 -99 4.6 0 0.4 11.1 0 -99 20.9 0.3 3.4 1 8 0 0.3 3.3 0 | 0 15.3 0 0 0 0 0 -99 0 0 0 10.7 3.2 0 -99 -99 25.8 2.6 0 3 3 2 2 0 0 2.2 0 0 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036076 9036081 9036081 9036185 9036169 9036147 9036151 9036152 9036252 9036257 9036257 9036261 9036262 9036264 9036272 9036281 9036308 9036310 | 36.43 36.63 36.33 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.77 36.10 36.45 36.52 36.63 36.45 36.90 36.03 36.53 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.92 -0.72 -0.25 -0.92 -0.72 -0.50 -0.48 -0.50 -0.48 -0.73 -0.92 -0.35 -0.20 -0.20 -0.77 | $\begin{array}{c} 16.3\\ 25.7\\ 0\\ 18.3\\ 102\\ 10.3\\ 12.2\\ 30.2\\ -99\\ 42.6\\ 7\\ 8.2\\ -99\\ 18.6\\ 2.5\\ -99\\ 102\\ 7.7\\ 7.7\\ 0\\ 102\\ 7.7\\ 7.7\\ 0\\ 14.1\\ 12.7\\ 84.4\\ 4.5\\ 43.6\\ 26.4 \end{array}$ | 2.1 3.6 0 6 3.3 -99 0 0 0 -99 0 0 0 -99 11.7 0 0.5 0 8.8 1.5 0 0 8.2 7 0 0 22.7 0 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 -99 0 0 0 -99 2.9 0 0 0 0.3 8.9 1.6 0 5.5 5 11.9 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 6.7 11 52 14 -99 23 13 6.3 8.5 18 13 38 5.2 9.5 | -99 -99 36.4 49.9 52.60 -99 3.1 36.4 10.8 41.6 222 32.2 40 51.5 44.5 -999 87.2 27.3 7.2 9.2 38.5 8.1 144 166 6.9 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 0 0 -99 4.7 3.6 6.5 28.5 5.8 5.1 5.4 0.7 23.6 5.1 | 3.4 2 0 94.4 7.4 0 24 -99 9.7 5.5 34 7.7 26.4 0 -99 45.2 2.8 3.9 7.3 55.8 9.1 48.7 0 8 8 6.1 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 0 25 40.9 0 0 -99 28.4 1.6 7.6 0 20 1.8 15 0 0 | 3.3 3 0 3 68 1.1 3.2 13 -99 0 0 0 366 0 11 0 -99 0 0 2.6 2 2 0.8 0 4.5 0 0 | 49 46 51 83 83 -99 33 32 72 27 19 61 -99 55 46 -99 55 46 -99 52 63 161 52 65 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 111 -99 16 5.2 -99 56 4.7 24 -99 39 21 28 3.7 21 | 34 29 65 59 99 51 44 42 36 0 43 -99 7.6 24 -99 136 15 23 -99 34 28 116 5 29 14 | 12 1.8 15 27 4.6 1.6 17 0 -99 3.6 0 2.1 11 0 -99 4.2 1.4 0 0 0 0 0 0 0 1.0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 1 0 4.1 0 8.9 2.5 5 0 -99 4.6 0 0.4 11.1 0 -99 -99 20.9 0.3 3.4 1 8 8 0 33.3 0 9 | 0 15.3 0 0 0 0 0 -99 0 0 0 10.7 3.2 0 -99 25.8 2.6 0 3 3 2 2 0 0 2.2 0 0 2.5 0 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036072 9036076 9036081 9036085 9036187 9036151 9036152 9036152 9036252 9036257 9036257 9036252 9036261 9036262 9036264 9036272 9036281 9036308 9036310 9036312 | 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.45 36.52 36.63 36.45 36.52 36.63 36.45 36.53 36.32 36.32 36.32 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.92 -0.72 -0.25 -0.92 -0.72 -0.50 -0.48 -0.50 -0.48 -0.73 -0.50 -0.48 -0.73 -0.20 -0.77 -0.20 -0.77 -0.20 -0.77 -0.20 -0.77 -0.20 -0.77 -0.20 -0.20 -0.77 -0.20 | $\begin{array}{c} 16.3\\ 25.7\\ 0\\ 18.3\\ 102\\ 10.3\\ 12.2\\ 30.2\\ -99\\ 42.6\\ 7\\ 8.2\\ -99\\ 18.6\\ 2.5\\ -99\\ 102\\ 7.7\\ 7.7\\ 0\\ 102\\ 7.7\\ 7.7\\ 0\\ 14.1\\ 12.7\\ 84.4\\ 4.5\\ 43.6\\ 26.4\\ 103\\ \end{array}$ | 2.1 3.6 0 6 3.3 -99 0 0 0 -99 0 0 0 -99 11.7 0 0.5 0 8.8 1.5 0 0 8.8 1.5 0 0 22.7 0 29 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 -99 0 0 0 -99 2.9 0 0 0.3 8.9 1.6 0 5.5 5 11.9 4.1 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 6.7 11 52 6.7 11 52 14 -99 23 13 6.3 8.5 18 13 38.5 18 13 38 0.5 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 10.8 41.6 222 32.2 40 51.5 44.5 -99 87.2 27.3 7.2 9.2 38.5 8.1 144 166 6.9 126 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 0 0 -99 4.7 3.6 6.5 28.5 5.8 5.1 5.4 0.7 23.6 5.1 | 3.4 2 0 94.4 7.4 -99 9.7 5.5 34 7.7 26.4 0 -99 45.2 2.8 3.9 7.3 55.8 9.1 48.7 0 8 55.7 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 0 25 40.9 0 0 0 -99 28.4 1.6 7.6 0 20 1.8 15 0 0 29.2 | 3.3 3 0 3 68 1.1 3.2 13 -99 0 0 0 366 0 11 0 -99 0 0 2.6 2 2 0.8 0 4.5 0 0 0 0 0 0 0 0 0 0 0 0 0 | 49 46 51 83 83 -99 33 32 72 27 19 61 -99 55 46 -99 156 43 46 -99 52 63 46 -99 52 63 161 52 58 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 111 -99 16 5.2 -99 56 4.7 24 -99 39 21 28 3.7 21 28 3.7 21 25 | 34 29 65 59 99 51 44 42 36 0 43 -99 7.6 24 -99 136 15 23 -99 34 28 116 5 29 14 | 12 1.8 15 27 4.6 1.6 17 0 -99 3.6 0 2.1 11 0 -99 4.2 1.4 0 0 0 0 0 0 0 1.0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 1 0 4.1 0 8.9 2.5 5 0 -99 4.6 0 0.4 11.1 0 -99 -99 20.9 0.3 3.4 1 8 0 0.3 3.3 0 9 9 0 0 | 0 15.3 0 0 0 0 0 -99 0 0 10.7 3.2 0 -99 25.8 2.6 0 3 3 2 2 0 0 2.2 0 0 2.5 0 0 -99 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036072 9036076 9036081 9036085 9036151 9036152 9036152 9036152 9036252 9036257 9036257 9036261 9036262 9036264 9036272 9036281 9036308 9036310 9036312 9036323 | 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.45 36.52 36.63 36.45 36.52 36.63 36.45 36.53 36.32 36.32 36.32 36.32 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.92 -0.72 -0.25 -0.92 -0.72 -0.50 -0.48 -0.50 -0.48 -0.73 -0.50 -0.48 -0.73 -0.20 -0.77 -0.20 -0.77 -0.20 -0.77 -0.20 -0.77 -0.20 -0.27 | $\begin{array}{c} 16.3\\ 25.7\\ 0\\ 18.3\\ 102\\ 10.3\\ 12.2\\ 30.2\\ -99\\ 42.6\\ 7\\ 8.2\\ -99\\ 18.6\\ 2.5\\ -99\\ 102\\ 7.7\\ 7.7\\ 0\\ 102\\ 7.7\\ 7.7\\ 0\\ 14.1\\ 12.7\\ 84.4\\ 4.5\\ 43.6\\ 26.4\\ 103\\ -99\end{array}$ | 2.1 3.6 0 6 3.3 -99 0 0 0 -99 0 0 3.5 -99 0 0 0 3.5 -99 0 0 0 5 0 0 8.8 8 1.5 0 0 22.7 0 29 -99 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 -99 0 0 0 0 -99 0 0 0 0.3 8.9 1.6 0 0.5.5 11.9 4.1 11.5 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 6.7 11 52 14 -99 23 13 6.3 8.5 18 13 38.5 18 13 38 5.2 6.7 0 26 -99 | -99 -99 36.4 49.9 52.6 -99 3.1 36.4 10.8 41.6 222 32.2 40 51.5 44.5 -99 87.2 27.3 7.2 9.2 38.5 8.1 144 166 6.9 126 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 0 -99 4.7 3.6 6.5 28.5 5.8 5.1 5.4 0.7 23.6 5.1 16.6 | 3.4 2 0 94.4 7.4 -99 9.7 5.5 34 7.7 26.4 0 -99 45.2 2.8 3.9 7.3 55.8 9.1 48.7 0 8 6.1 55.7 0 0 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 25 40.9 0 0 -99 28.4 1.6 7.6 0 20 1.8 15 0 0 0 29.2 0 0 | 3.3 3 0 3 68 1.1 3.2 13 -99 0 0 0 366 0 11 0 -99 0 0 2.6 2 2 0.8 0 4.5 0 0 0 0 0 0 0 0 0 0 0 0 0 | 49 46 51 83 83 -99 33 22 72 27 19 61 -99 55 46 -99 55 46 -99 52 63 46 -99 52 63 161 52 65 58 98 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 111 -99 16 5.2 -99 56 4.7 24 -99 39 21 28 3.7 21 28 3.7 21 25 33 | 34 29 16 53 59 99 51 44 42 36 0 43 -99 7.6 24 -99 136 15 23 -99 34 28 116 5 29 14 102 | 12 1.8 15 27 4.6 1.6 1.7 0 -99 3.6 0 2.1 11 0 -99 4.2 1.4 0 0 0 0 0 0 0 1.0 0 0 -99 9.5 0.5 0 -99 | 1 0 4.1 0 8.9 2.5 5 0 -99 4.6 0 0.4 11.1 0 -99 20.9 0.3 3.4 1 8 0 0.3 3.3 0 9 9 0 0 -99 | 0 15.3 0 0 0 0 0 -99 0 0 10.7 3.2 0 -99 25.8 2.6 0 3 3 2 2 0 0 2.2 0 0 2.5 0 0 -99 |
| Dec | 9036002 9036025 9036034 9036061 9036072 9036072 9036076 9036081 9036185 9036185 9036152 9036152 9036152 9036257 9036257 9036257 9036261 9036262 9036264 9036272 9036281 9036308 9036310 9036312 9036323 9036336 | 36.43 36.63 36.63 36.25 36.02 36.42 36.77 36.38 36.20 36.17 36.65 36.68 36.20 36.17 36.65 36.68 36.23 36.08 36.70 36.77 36.10 36.45 36.52 36.63 36.45 36.52 36.63 36.45 36.90 36.53 36.53 36.32 36.82 36.28 36.28 36.03 | -0.72 -0.58 -0.50 -0.98 -0.35 -0.30 -0.65 -0.13 -0.65 -0.47 -0.03 -0.72 -0.72 -0.72 -0.25 -0.92 -0.72 -0.25 -0.92 -0.72 -0.50 -0.48 -0.50 -0.48 -0.73 -0.50 -0.48 -0.73 -0.20 -0.77 -0.55 -0.20 -0.77 -0.58 | $\begin{array}{c} 16.3\\ 25.7\\ 0\\ 18.3\\ 102\\ 10.3\\ 12.2\\ 30.2\\ -99\\ 42.6\\ 7\\ 8.2\\ -99\\ 42.6\\ 7\\ 8.2\\ -99\\ 102\\ 7.7\\ 7.7\\ 0\\ 102\\ 7.7\\ 7.7\\ 0\\ 14.1\\ 12.7\\ 84.4\\ 4.5\\ 43.6\\ 26.4\\ 103\\ -99\\ -99\\ -99\\ -99\\ \end{array}$ | 2.1 3.6 0 6 3.3 -99 0 0 0 3.5 -99 0 0 0 3.5 -99 0 0 0 -99 11.7 0 0.5 0 0 8.88 1.5 0 0 0 22.7 0 299 -99 -99 | 0 0 2.4 10 9.9 0 3.4 0.7 -99 0 0 0 -99 0 0 0 -99 2.9 0 0 0.3 8.9 1.6 0 0.3 8.9 1.6 1.9 9 1.5 5.5 11.9 4.1 11.5 -99 | -99 -99 6.5 13 16 -99 29 6.5 7.2 20 5.2 6.7 11 52 14 -99 23 13 6.3 8.5 18 13 38.5 18 13 38 5.2 6.7 9.9 23 13 6.3 8.5 18 10 9.5 0 26 5.3 10 5.2 10 10 5.2 10 10 10 5.2 10 10 10 10 10 10 10 10 10 10 10 10 10 | -99 -99 36.4 49.9 52.69 3.1 36.4 10.8 41.6 222 32.2 40 51.5 44.5 -999 87.2 27.3 7.2 9.2 38.5 8.1 144 166 6.9 1266 -999 | -99 -99 19.2 4 6.2 -99 0 5 0 3.2 2.8 5.1 10 0 0 -99 4.7 3.6 6.5 28.5 5.8 5.1 5.4 0.7 23.6 5.1 16.6 -99 7.3 | 3.4 2 0 94.4 7.4 0 24 -99 9.7 5.5 34 7.7 26.4 0 -99 45.2 2.8 3.9 7.3 55.8 9.1 48.7 0 8 55.7 0 0 8 6.1 55.7 | 0 7.4 7.2 0 31.6 2.4 10.8 0.2 -99 0 0 25 40.9 0 0 -99 28.4 1.6 7.6 0 20 1.8 15 0 0 0 29.2 0 0 | 3.3 3 0 3 68 1.1 3.2 13 -99 0 0 0 36 0 0 11 0 -99 0 0 2.6 2 2 0.8 0 4.5 0 0 0 0 0 0 0 0 0 0 0 0 0 | 49 46 51 83 83 -99 33 22 72 27 19 61 -99 55 46 -99 55 46 -99 52 63 46 -99 52 63 161 52 65 58 98 33 | 15 42 8.4 104 28 -99 13 0 16 6.1 3.5 111 -99 16 5.2 -99 56 4.7 24 -99 56 4.7 24 -99 39 21 28 3.7 21 28 3.7 21 25 33 4 | 34 29 16 53 59 -99 51 44 42 36 0 43 -99 7.6 24 -99 136 15 23 -99 34 28 116 55 29 14 102 55 31 | 12 1.8 15 27 4.6 1.7 0 -99 3.6 0 2.1 11 0 -99 4.2 1.4 0 0 0 0 0 0 0 0 0 0 0 0 0 | 1 0 4.1 0 8.9 2.5 5 0 -99 4.6 0 0.4 11.1 0 -99 20.9 0.3 3.4 1 8 0 0.3 3.3 4 0 0 33.3 0 0 9 9 0.99 1.8 | 0 15.3 0 0 0 0 -99 0 0 10.7 3.2 0 -99 25.8 2.6 0 3 2 2.5 0 -99 0.6 1 1 |

International Institute For Aerospace Survey and Earth Sciences

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APPENDIX C Determination of optimum threshold Tt (daily and decadal data) including contingency table

| CCDU | | | | | | | | | | | | | |
|------|------|------|-------|------|------|------|------|------|------|-------|------|------|------|
| | | | March | | | | | | | April | | | |
| | | | Ir=0 | Ir=1 | | | | | | Ir=0 | Ir=1 | | |
| | | IC=0 | 2551 | 597 | | | | | Ic=0 | 1275 | 658 | | |
| R > | 0mm | Ic=1 | 596 | 586 | | | R > | Omm | Ic=1 | 346 | 837 | | |
| h = | 0 | 2 | 4 | 6 | 8 | 10 | h= | 0 | 2 | 4 | 6 | 8 | 10 |
| PC | 0.72 | 0.74 | 0.75 | 0.75 | 0.74 | 0.74 | PC | 0.68 | 0.66 | 0.64 | 0.62 | 0.59 | 0.60 |
| Bias | 1.00 | 0.74 | 0.55 | 0.46 | 0.37 | 0.31 | Bias | 0.79 | 0.61 | 0.49 | 0.40 | 0.32 | 0.27 |
| HR | 0.50 | 0.39 | 0.31 | 0.27 | 0.22 | 0.19 | HR | 0.56 | 0.45 | 0.36 | 0.31 | 0.25 | 0.22 |
| FAR | 0.19 | 0.13 | 0.09 | 0.07 | 0.06 | 0.05 | FAR | 0.21 | 0.14 | 0.11 | 0.09 | 0.06 | 0.05 |
| KSS | 0.31 | 0.26 | 0.22 | 0.20 | 0.16 | 0.14 | KSS | 0.35 | 0.31 | 0.25 | 0.22 | 0.19 | 0.17 |

| | | | May | | | | | | | June | | | |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| | | | Ir=0 | Ir=1 | | | | | | Ir=0 | Ir=1 | | |
| | | Ic=0 | 2063 | 1124 | | | | | Ic=0 | 2015 | 846 | | |
| R > | 0mm | Ic=1 | 431 | 753 | | | R > | 0mm | Ic=1 | 321 | 466 | | |
| h= | 0 | 2 | 4 | 6 | 8 | 10 | h = | 0 | 2 | 4 | 6 | 8 | 10 |
| PC | 0.64 | 0.64 | 0.63 | 0.62 | 0.60 | 0.60 | PC | 0.68 | 0.68 | 0.68 | 0.67 | 0.65 | 0.65 |
| Bias | 0.63 | 0.44 | 0.32 | 0.24 | 0.17 | 0.13 | Bias | 0.60 | 0.44 | 0.32 | 0.21 | 0.13 | 0.09 |
| HR | 0.40 | 0.30 | 0.23 | 0.18 | 0.14 | 0.10 | HR | 0.36 | 0.28 | 0.21 | 0.14 | 0.09 | 0.06 |
| FAR | 0.17 | 0.10 | 0.06 | 0.05 | 0.03 | 0.02 | FAR | 0.14 | 0.09 | 0.06 | 0.04 | 0.02 | 0.01 |
| KSS | 0.23 | 0.20 | 0.17 | 0.14 | 0.11 | 0.08 | KSS | 0.22 | 0.19 | 0.15 | 0.10 | 0.07 | 0.05 |

| | | | October | 1 | | | | | | November | 1 | | |
|------|------|------|---------|------|------|------|------|------|------|----------|------|------|------|
| | | | Ir=0 | Ir=1 | | | | | | Ir=0 | Ir=1 | | |
| | | IC=0 | 1614 | 789 | | | | | IC=0 | 1458 | 1282 | | |
| R > | 0mm | Ic=1 | 267 | 289 | | | R > | 0mm | IC=1 | 396 | 794 | | |
| h= | 0 | 2 | 4 | 6 | 8 | 10 | h = | 0 | 2 | 4 | 6 | 8 | 10 |
| PC | 0.64 | 0.65 | 0.65 | 0.64 | 0.64 | 0.64 | PC | 0.57 | 0.55 | 0.53 | 0.52 | 0.49 | 0.50 |
| Bias | 0.52 | 0.28 | 0.14 | 0.07 | 0.04 | 0.02 | Bias | 0.57 | 0.41 | 0.29 | 0.21 | 0.15 | 0.10 |
| HR | 0.27 | 0.15 | 0.08 | 0.05 | 0.03 | 0.01 | HR | 0.38 | 0.28 | 0.20 | 0.15 | 0.11 | 0.08 |
| FAR | 0.14 | 0.07 | 0.03 | 0.01 | 0.01 | 0.00 | FAR | 0.21 | 0.15 | 0.09 | 0.07 | 0.04 | 0.03 |
| KSS | 0.13 | 0.08 | 0.05 | 0.03 | 0.02 | 0.01 | KSS | 0.17 | 0.13 | 0.11 | 0.08 | 0.06 | 0.05 |

| | | | December | | | |
|------|------|------|----------|------|------|------|
| | | | Ir=0 | Ir=1 | | |
| | | IC=0 | 2752 | 712 | | |
| R > | Omm | Ic=1 | 174 | 258 | | |
| h= | 0 | 2 | 4 | 6 | 8 | 10 |
| PC | 0.77 | 0.78 | 0.77 | 0.76 | 0.75 | 0.75 |
| Bias | 0.45 | 0.24 | 0.13 | 0.08 | 0.06 | 0.04 |
| HR | 0.27 | 0.17 | 0.10 | 0.06 | 0.04 | 0.02 |
| FAR | 0.06 | 0.02 | 0.01 | 0.01 | 0.00 | 0.00 |
| KSS | 0.21 | 0.15 | 0.09 | 0.06 | 0.04 | 0.02 |

1.Daily data.

| | | | March |] | | | | | | April |] | | |
|------|------|------|-------|------|------|------|------|------|------|-------|------|------|------|
| | | | Ir=0 | Ir=1 | | | | | | Ir=0 | Ir=1 | | |
| | | Ic=0 | 14 | 20 | | | | | Ic=0 | 4 | 17 | | |
| R > | Omm | Ic=1 | 56 | 263 | | | R > | 0mm | Ic=1 | 8 | 143 | | |
| h = | 0 | 2 | 4 | 6 | 8 | 10 | h = | 0 | 2 | 4 | 6 | 8 | 10 |
| PC | 0.78 | 0.78 | 0.67 | 0.59 | 0.50 | 0.50 | PC | 0.85 | 0.87 | 0.78 | 0.65 | 0.48 | 0.48 |
| Bias | 1.13 | 0.86 | 0.67 | 0.55 | 0.46 | 0.42 | Bias | 0.94 | 0.89 | 0.78 | 0.63 | 0.53 | 0.44 |
| HR | 0.93 | 0.79 | 0.63 | 0.52 | 0.44 | 0.40 | HR | 0.89 | 0.88 | 0.77 | 0.63 | 0.53 | 0.44 |
| FAR | 0.80 | 0.27 | 0.16 | 0.11 | 0.09 | 0.09 | FAR | 0.67 | 0.25 | 0.08 | 0.00 | 0.00 | 0.00 |
| KSS | 0.13 | 0.52 | 0.48 | 0.41 | 0.35 | 0.31 | KSS | 0.23 | 0.63 | 0.69 | 0.63 | 0.53 | 0.44 |

| | | | Мау | 1 | | | | | | June | 1 | | |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| | | | Ir=0 | Ir=1 | | | | | | Ir=0 | Ir=1 | | |
| | | Ic=0 | 13 | 68 | | | | | Ic=0 | 15 | 58 | | |
| R > | 0mm | Ic=1 | 10 | 332 | | | R > | 0mm | Ic=1 | 9 | 238 | | |
| h= | 0 | 2 | 4 | 6 | 8 | 10 | h= | 0 | 2 | 4 | 6 | 8 | 10 |
| PC | 0.82 | 0.69 | 0.52 | 0.42 | 0.34 | 0.34 | PC | 0.79 | 0.61 | 0.53 | 0.43 | 0.30 | 0.30 |
| Bias | 0.86 | 0.69 | 0.49 | 0.39 | 0.33 | 0.31 | Bias | 0.83 | 0.59 | 0.50 | 0.40 | 0.28 | 0.25 |
| HR | 0.83 | 0.68 | 0.49 | 0.39 | 0.33 | 0.31 | HR | 0.80 | 0.58 | 0.50 | 0.39 | 0.28 | 0.25 |
| FAR | 0.43 | 0.13 | 0.00 | 0.00 | 0.00 | 0.00 | FAR | 0.38 | 0.08 | 0.04 | 0.04 | 0.04 | 0.04 |
| KSS | 0.40 | 0.55 | 0.49 | 0.39 | 0.33 | 0.31 | KSS | 0.43 | 0.50 | 0.45 | 0.35 | 0.24 | 0.21 |

| | | | October |] | | | | | | November |] | | |
|------|------|------|---------|------|------|------|------|------|------|----------|------|------|------|
| | | | Ir=0 | Ir=1 | | | | | | Ir=0 | Ir=1 | | |
| | | Ic=0 | 8 | 30 | | | | | Ic=0 | 9 | 68 | | |
| R > | Omm | Ic=1 | 17 | 162 | | | R > | 0mm | Ic=1 | 5 | 310 | - | |
| h= | 0 | 2 | 4 | 6 | 8 | 10 | h= | 0 | 2 | 4 | 6 | 8 | 10 |
| PC | 0.78 | 0.58 | 0.41 | 0.34 | 0.23 | 0.24 | PC | 0.81 | 0.73 | 0.61 | 0.51 | 0.31 | 0.31 |
| Bias | 0.93 | 0.61 | 0.37 | 0.28 | 0.20 | 0.14 | Bias | 0.83 | 0.73 | 0.62 | 0.51 | 0.39 | 0.29 |
| HR | 0.84 | 0.57 | 0.35 | 0.27 | 0.19 | 0.14 | HR | 0.82 | 0.72 | 0.61 | 0.50 | 0.39 | 0.29 |
| FAR | 0.68 | 0.32 | 0.16 | 0.08 | 0.08 | 0.00 | FAR | 0.36 | 0.21 | 0.21 | 0.21 | 0.14 | 0.07 |
| KSS | 0.16 | 0.25 | 0.19 | 0.19 | 0.11 | 0.14 | KSS | 0.46 | 0.51 | 0.39 | 0.29 | 0.24 | 0.22 |

| | | | December | | | |
|------|------|------|----------|------|------|------|
| | | | Ir=0 | Ir=1 | | |
| | | Ic=0 | 48 | 98 | | |
| R > | 0mm | Ic=1 | 28 | 163 | | |
| h= | 0 | 2 | 4 | 6 | 8 | 10 |
| PC | 0.63 | 0.49 | 0.42 | 0.40 | 0.36 | 0.36 |
| Bias | 0.73 | 0.39 | 0.27 | 0.23 | 0.20 | 0.18 |
| HR | 0.62 | 0.36 | 0.26 | 0.23 | 0.20 | 0.18 |
| FAR | 0.37 | 0.08 | 0.03 | 0.01 | 0.01 | 0.01 |
| KSS | 0.26 | 0.29 | 0.23 | 0.21 | 0.19 | 0.16 |

2.decadal data.

CCD40

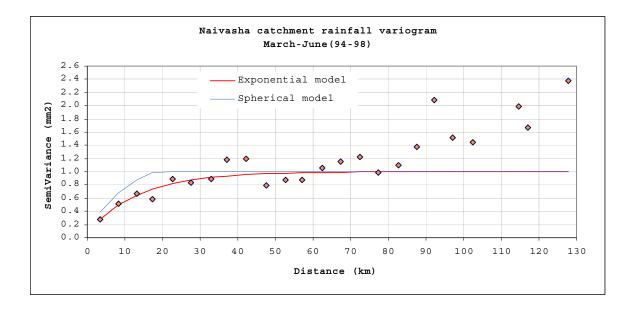
| | | | March | | | | | | | April |] | | |
|------|------|------|-------|------|------|------|------|------|------|-------|------|------|------|
| | | | Ir=0 | Ir=1 | | | | | | Ir=0 | Ir=1 | | |
| | | Ic=0 | 26 | 68 | | | | | Ic=0 | 11 | 38 | | |
| R > | 0mm | Ic=1 | 48 | 240 | | | R > | 0 mm | Ic=1 | 1 | 122 | | |
| h= | 0 | 2 | 4 | 6 | 8 | 10 | h= | 0 | 2 | 4 | 6 | 8 | 10 |
| PC | 0.70 | 0.57 | 0.50 | 0.46 | 0.45 | 0.45 | PC | 0.77 | 0.59 | 0.51 | 0.45 | 0.40 | 0.40 |
| Bias | 0.94 | 0.55 | 0.43 | 0.38 | 0.36 | 0.35 | Bias | 0.77 | 0.58 | 0.47 | 0.41 | 0.39 | 0.35 |
| HR | 0.78 | 0.51 | 0.41 | 0.36 | 0.34 | 0.34 | HR | 0.76 | 0.57 | 0.47 | 0.41 | 0.39 | 0.35 |
| FAR | 0.65 | 0.16 | 0.11 | 0.09 | 0.08 | 0.07 | FAR | 0.08 | 0.08 | 0.00 | 0.00 | 0.00 | 0.00 |
| KSS | 0.13 | 0.35 | 0.30 | 0.26 | 0.26 | 0.27 | KSS | 0.68 | 0.49 | 0.47 | 0.41 | 0.39 | 0.35 |

| | | | Мау | 1 | | | | | | June | 1 | | |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| | | | Ir=0 | Ir=1 | | | | | | Ir=0 | Ir=1 | | |
| | | IC=0 | 18 | 112 | | | | | IC=0 | 22 | 109 | | |
| R > | 0mm | Ic=1 | 5 | 288 | | | R > | 0 mm | Ic=1 | 2 | 187 | | |
| h= | 0 | 2 | 4 | 6 | 8 | 10 | h= | 0 | 2 | 4 | 6 | 8 | 10 |
| PC | 0.72 | 0.51 | 0.38 | 0.33 | 0.28 | 0.28 | PC | 0.65 | 0.49 | 0.37 | 0.28 | 0.14 | 0.14 |
| Bias | 0.73 | 0.48 | 0.34 | 0.29 | 0.25 | 0.24 | Bias | 0.64 | 0.47 | 0.32 | 0.23 | 0.16 | 0.08 |
| HR | 0.72 | 0.48 | 0.34 | 0.29 | 0.25 | 0.24 | HR | 0.63 | 0.46 | 0.32 | 0.22 | 0.15 | 0.08 |
| FAR | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | FAR | 0.08 | 0.08 | 0.04 | 0.04 | 0.04 | 0.04 |
| KSS | 0.50 | 0.48 | 0.34 | 0.29 | 0.25 | 0.24 | KSS | 0.55 | 0.38 | 0.28 | 0.18 | 0.11 | 0.04 |

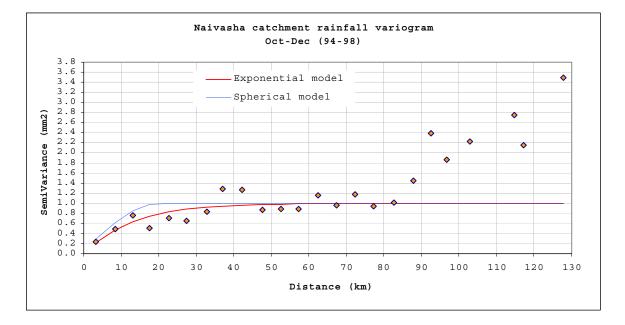
| | | | October | | | | | | | November | | | |
|------|------|------|---------|------|------|------|------|------|------|----------|------|------|------|
| | | | Ir=0 | Ir=1 | | | | | | Ir=0 | Ir=1 | | |
| | | Ic=0 | 18 | 91 | | | | | IC=0 | 10 | 107 | | |
| R > | 0mm | Ic=1 | 7 | 101 | | | R > | 0 mm | Ic=1 | 4 | 272 | - | |
| h = | 0 | 2 | 4 | 6 | 8 | 10 | h= | 0 | 2 | 4 | 6 | 8 | 10 |
| PC | 0.55 | 0.31 | 0.24 | 0.18 | 0.14 | 0.14 | PC | 0.72 | 0.44 | 0.30 | 0.20 | 0.12 | 0.12 |
| Bias | 0.56 | 0.24 | 0.17 | 0.07 | 0.04 | 0.03 | Bias | 0.73 | 0.43 | 0.27 | 0.17 | 0.13 | 0.09 |
| HR | 0.53 | 0.23 | 0.16 | 0.07 | 0.04 | 0.03 | HR | 0.72 | 0.43 | 0.27 | 0.17 | 0.13 | 0.09 |
| FAR | 0.28 | 0.08 | 0.08 | 0.00 | 0.00 | 0.00 | FAR | 0.29 | 0.14 | 0.00 | 0.00 | 0.00 | 0.00 |
| KSS | 0.25 | 0.15 | 0.08 | 0.07 | 0.04 | 0.03 | KSS | 0.43 | 0.28 | 0.27 | 0.17 | 0.13 | 0.09 |

| | | | December | | | |
|------|------|------|----------|------|------|------|
| | | | Ir=0 | Ir=1 | | |
| | | Ic=0 | 67 | 156 | | |
| R > | Omm | Ic=1 | 9 | 105 | | |
| h= | 0 | 2 | 4 | 6 | 8 | 10 |
| PC | 0.51 | 0.38 | 0.36 | 0.31 | 0.23 | 0.23 |
| Bias | 0.44 | 0.21 | 0.18 | 0.11 | 0.04 | 0.00 |
| HR | 0.40 | 0.20 | 0.18 | 0.11 | 0.04 | 0.00 |
| FAR | 0.12 | 0.01 | 0.01 | 0.00 | 0.00 | 0.00 |
| KSS | 0.28 | 0.19 | 0.16 | 0.11 | 0.04 | 0.00 |

1.Decadal data.







Monthly variogram, decadl data for the year 94 to 98 with lag spacing 5km, for long (march to june) and short (october to November) rainy season.

| | P= | 0.21 | 1 | 1 | | | 1 | P | 0.35 | est | | |
|------------|--------------|---------|------|----------------|--------------|--------------|----------------|--------------|--------------|--------------|-------|-----------------|
| Date | | Box cox | Fc | KR | Sgrtrai | estsqr | EstR | - Residua | box- | box-cox | EstR | Residuals |
| | t | | - | | n | t | | ls | cox | | | |
| НЗҮ | 2.55 | 1.03 | 0.91 | 14.23 | 3.77 | 4.79 | 22.93 | 8.70 | 4.38 | 5.55 | 21.83 | 7.60 |
| H3Z | 21.48 | 4.31 | 1.00 | 31.52 | 5.61 | 6.11 | 37.38 | 5.85 | 6.70 | 8.37 | 49.94 | 18.42 |
| H4X | 5.58 | 2.07 | 1.00 | 29.70 | 5.45 | 5.00 | 25.00 | -4.69 | 6.51 | 6.44 | 29.13 | -0.56 |
| H4Y | 5.60 | 2.07 | 0.99 | 22.06 | 4.70 | 5.00 | 25.02 | 2.96 | 5.58 | 6.45 | 29.18 | 7.12 |
| H4Z | 27.40 | 4.78 | 1.00 | 96.06 | 9.80 | 6.53 | 42.61 | -53.44 | 11.26 | | 55.33 | -40.73 |
| H5X | 2.56 | 1.04 | 0.93 | 38.86 | 6.23 | 4.79 | 22.93 | -15.93 | 7.43 | 5.55 | | -17.01 |
| H5Y | 2.22 | 0.87 | 0.61 | 31.72 | 5.63 | 4.77 | 22.71 | -9.01 | 6.72 | 5.40 | | -10.94 |
| H5Z | 0.61 | -0.46 | 0.43 | 41.28 | 6.42 | 4.65 | 21.65 | -19.63 | 7.65 | 4.26 | | -27.73 |
| H6X | 6.75 | 2.35 | 1.00 | 26.42 | 5.14 | 5.08 | 25.83 | -0.60 | 6.13 | | 31.34 | 4.92 |
| H6Y | 6.91 | 2.38 | 0.97 | 52.38 | 7.24 | 5.09 | 25.94 | -26.44 | 8.56 | 6.71 | | -20.75 |
| H6Z | 6.17 | 2.22 | 1.00 | 21.38 | 4.62 | 5.04 | 25.42 | 4.04 | 5.49 | 6.57 | 30.28 | 8.90 |
| HAZ | 1.50 | 0.42 | | 36.66 | 6.05 | 4.71 | 22.23 | -14.43 | 7.22 | | 18.14 | -18.52 |
| HBX | 12.76 | 3.37 | 1.00 | 70.99 | 8.43 | 5.50 | 30.29 | -40.70 | 9.84 | | 40.32 | -30.67 |
| HBY | 9.81 | 2.93 | 1.00 | 60.90 | 7.80 | 5.30 | 28.06 | -32.85 | 9.18 | | 36.29 | -24.62 |
| HBZ | 10.01 | 2.96 | 1.00 | 42.99 | 6.56 | 5.31 | 28.20 | -14.79 | 7.80 | 7.21 | 36.58 | -6.42 |
| HCX | 1.80 | 0.63 | 0.86 | 22.30 | 4.72 | 4.74 | 22.43 | 0.13 | 5.61 | | 19.32 | -2.98 |
| HCZ | 0.09 | -1.86 | 0.09 | 3.54 59.99 | 1.88 | 4.62 | 21.31 | 17.78 | 1.59 9.12 | 3.05 | 7.96 | 4.43 |
| I3X | 31.42 | 5.06 | | | 7.75 | 6.81 | 46.36 | -13.63 | | 9.02 | 58.65 | |
| I5X | 5.30 | 2.00 | 0.99 | 47.61 | 6.90 5.45 | 4.98 | 24.81 | -22.80 | 8.19 | | 28.59 | -19.03 |
| I5Y | 11.63 | 3.21 | 1.00 | 29.68 | | 5.42 | 29.42 | -0.26 | 6.50 | | 38.84 | 9.16 |
| I5Z | 1.72 5.94 | 0.57 | | 15.78 | 3.97 | 4.73 | 22.38 25.26 | 6.60 | 4.65 | 5.15 6.52 | | 3.23 |
| 16Y 16Z | 1.38 | 2.16 | 0.98 | 30.61 31.33 | 5.53 | 5.03 4.71 | 25.26 | -5.35 | 6.61 6.68 | | 29.85 | -0.76 -13.71 |
| IBX | 0.56 | -0.55 | 0.88 | 28.99 | 5.80 | 4.71 | 22.15 | -9.18 | 6.43 | | 13.13 | -13.71 |
| IBX | 6.24 | 2.23 | 1.00 | 50.49 | 7.11 | 4.65 | 25.47 | -25.02 | 8.42 | 4.10 | | -15.85 |
| IBI | 5.09 | 1.94 | 1.00 | 11.24 | 3.35 | 4.97 | 25.47 | | 3.81 | 6.33 | | -20.08 |
| ICX | 0.12 | -1.70 | 0.12 | 11.51 | 3.39 | 4.62 | 21.33 | 9.82 | 3.86 | 3.19 | 8.53 | -2.98 |
| ICY | 2.30 | 0.91 | 0.63 | 22.64 | 4.76 | 4.77 | 22.76 | 0.12 | 5.66 | 5.44 | | -1.59 |
| ICZ | 1.20 | 0.18 | 0.74 | 9.64 | 3.10 | 4.69 | 22.03 | 12.39 | 3.46 | 4.82 | | 7.18 |
| J3X | 4.44 | 1.75 | 1.00 | 7.89 | 2.81 | 4.92 | 24.22 | 16.32 | 3.03 | | 26.74 | 18.85 |
| J3Y | 3.37 | 1.38 | 0.82 | 20.45 | 4.52 | 4.85 | 23.48 | 3.03 | 5.36 | 5.85 | | 3.69 |
| J3Z | 34.48 | 5.25 | | 54.95 | 7.41 | 7.02 | 49.33 | -5.62 | 8.76 | 9.19 | | 6.09 |
| J4Z | 0.45 | -0.73 | 0.25 | 8.07 | 2.84 | 4.64 | 21.54 | 13.48 | 3.08 | 4.03 | 12.33 | 4.27 |
| J5X | 4.12 | 1.65 | 1.00 | 13.73 | 3.71 | 4.90 | 24.00 | 10.27 | 4.29 | | 26.01 | 12.28 |
| J5Y | 10.65 | 3.06 | 1.00 | 45.10 | 6.72 | 5.36 | 28.68 | -16.41 | 7.98 | | 37.49 | -7.60 |
| J5Z | 0.76 | -0.27 | 0.34 | 22.42 | 4.74 | 4.66 | 21.74 | -0.68 | 5.63 | | 14.47 | -7.95 |
| J6X | 4.80 | 1.86 | 0.77 | 73.63 | 8.58 | 4.95 | 24.47 | -49.17 | 10.01 | 6.26 | 27.54 | -46.09 |
| JGY | 12.19 | 3.29 | 1.00 | 36.01 | 6.00 | 5.46 | 29.85 | -6.16 | 7.16 | | 39.58 | 3.57 |
| JAX | 6.14 | 2.21 | 1.00 | 12.30 | 3.51 | 5.04 | 25.40 | 13.10 | 4.02 | 6.56 | 30.23 | 17.93 |
| JAY | 1.48 | 0.41 | 0.69 | 21.81 | 4.67 | 4.71 | 22.22 | 0.41 | 5.55 | 5.01 | 18.07 | -3.74 |
| JAZ | 0.56 | -0.55 | 0.42 | 21.40 | 4.63 | 4.65 | 21.61 | 0.21 | 5.49 | 4.18 | 13.14 | -8.26 |
| JBX | 5.38 | 2.02 | 1.00 | 23.91 | 4.89 | 4.99 | 24.86 | 0.95 | 5.82 | 6.40 | 28.74 | 4.82 |
| JBY | 0.16 | -1.52 | 0.16 | 8.96 | 2.99 | 4.62 | 21.36 | 12.40 | 3.30 | 3.34 | 9.15 | 0.19 |
| JBZ | 6.90 | 2.38 | 1.00 | 43.08 | 6.56 | 5.09 | 25.94 | -17.15 | 7.81 | 6.71 | 31.61 | -11.47 |
| JCX | 1.45 | 0.39 | 0.75 | 15.39 | 3.92 | 4.71 | 22.20 | 6.81 | 4.58 | 4.99 | 17.94 | 2.55 |
| JCY | 0.89 | -0.12 | 0.73 | 7.53 | 2.74 | 4.67 | 21.83 | 14.30 | 2.93 | 4.55 | 15.23 | 7.70 |
| JCZ | 0.70 | -0.35 | 0.54 | 8.18 | 2.86 | 4.66 | 21.71 | 13.52 | 3.11 | 4.36 | 14.11 | 5.93 |
| K3X | 1.02 | 0.02 | 1.00 | 0.86 | 0.93 | 4.68 | 21.91 | 21.05 | -0.14 | 4.67 | 15.94 | 15.08 |
| КЗҮ | 1.34 | 0.30 | 0.76 | 1.85 | 1.36 | 4.70 | 22.13 | 20.28 | 0.69 | | 17.46 | 15.61 |
| K3Z | 60.84 | 6.52 | | 31.90 | 5.65 | 8.87 | 78.66 | 46.76 | 6.74 | | 78.26 | 46.36 |
| K4X | 106.60 | 7.93 | | 84.40 | 9.19 | 12.07 | 145.74 | 61.34 | 10.64 | 11.50 | ##### | 16.40 |
| K5X | 27.20 | 4.77 | | 35.37 | 5.95 | 6.51 | 42.43 | 7.06 | 7.10 | | 55.16 | 19.79 |
| K5Y | 2.58 | 1.05 | | 14.97 | 3.87 | 4.79 | 22.95 | 7.98 | 4.51 | | 21.91 | 6.94 |
| K5Z | 0.10 | -1.86 | | 4.71 | 2.17 | 4.62 | 21.31 | 16.61 | 2.06 | 3.05 | | 3.28 |
| K6X | 0.86 | -0.15 | | 5.90 | 2.43 | 4.67 | 21.81 | 15.92 | 2.46 | | 15.08 | 9.18 |
| КбҮ | 4.79 | 1.85 | | 33.69 | 5.80 | 4.94 | 24.45 | -9.24 | 6.93 | | 27.50 | -6.19 |
| K6Z | 8.25 | 2.65 | 1.00 | 20.02 | 4.47 | 5.19 | 26.91 | 6.89 | 5.30 | 6.95 | 33.88 | 13.87 |

APPENDIX E Calibration plot calculation for decadal data

| KAX | 3.74 | 1.52 | 0.98 | 30.74 | 5.54 | 4.87 | 23.73 | -7.01 | 6.62 | 5.97 | 25.08 | -5.66 |
|-----|-------|-------|------|--------|-------|------|-------|--------|-------|-------|-------|--------|
| KAY | 2.34 | 0.93 | 0.85 | 59.41 | 7.71 | 4.77 | 22.79 | -36.62 | 9.08 | 5.46 | 21.18 | -38.23 |
| KBX | 9.77 | 2.92 | 1.00 | 82.88 | 9.10 | 5.29 | 28.03 | -54.85 | 10.55 | 7.18 | 36.23 | -46.64 |
| KBY | 70.64 | 6.88 | 1.00 | 72.29 | 8.50 | 9.55 | 91.30 | 19.01 | 9.93 | 10.60 | 83.66 | 11.37 |
| KBZ | 9.68 | 2.91 | 1.00 | 45.45 | 6.74 | 5.29 | 27.96 | -17.50 | 8.01 | 7.17 | 36.09 | -9.36 |
| KCX | 12.51 | 3.33 | 1.00 | 58.81 | 7.67 | 5.49 | 30.09 | -28.72 | 9.03 | 7.53 | 39.99 | -18.82 |
| KCY | 15.55 | 3.71 | 1.00 | 31.02 | 5.57 | 5.70 | 32.47 | 1.45 | 6.65 | 7.86 | 43.69 | 12.67 |
| KCZ | 3.54 | 1.45 | 0.97 | 30.66 | 5.54 | 4.86 | 23.60 | -7.07 | 6.61 | 5.91 | 24.58 | -6.08 |
| L3X | 7.95 | 2.60 | 1.00 | 20.00 | 4.47 | 5.17 | 26.69 | 6.69 | 5.30 | 6.90 | 33.41 | 13.41 |
| L3Y | 0.76 | -0.26 | 0.48 | 10.16 | 3.19 | 4.66 | 21.75 | 11.58 | 3.58 | 4.43 | 14.52 | 4.36 |
| L3Z | 4.14 | 1.66 | 1.00 | 15.13 | 3.89 | 4.90 | 24.01 | 8.88 | 4.54 | 6.09 | 26.05 | 10.92 |
| L4Z | 6.82 | 2.37 | 0.99 | 31.65 | 5.63 | 5.09 | 25.88 | -5.76 | 6.72 | 6.70 | 31.48 | -0.16 |
| L5X | 29.70 | 4.94 | 1.00 | 136.14 | 11.67 | 6.69 | 44.74 | -91.40 | 13.10 | 8.92 | 57.26 | -78.88 |
| L5Y | 32.27 | 5.12 | 1.00 | 60.43 | 7.77 | 6.87 | 47.19 | -13.24 | 9.15 | 9.07 | 59.33 | -1.09 |
| L5Z | 3.08 | 1.27 | 0.97 | 43.44 | 6.59 | 4.83 | 23.28 | -20.15 | 7.84 | 5.75 | 23.36 | -20.08 |
| L6Y | 1.30 | 0.27 | 0.70 | 30.85 | 5.55 | 4.70 | 22.10 | -8.75 | 6.63 | 4.89 | 17.29 | -13.55 |
| LAX | 5.05 | 1.93 | 1.00 | 17.21 | 4.15 | 4.96 | 24.63 | 7.43 | 4.88 | 6.32 | 28.06 | 10.85 |
| LAY | 8.23 | 2.65 | 1.00 | 31.10 | 5.58 | 5.19 | 26.89 | -4.21 | 6.66 | 6.94 | 33.85 | 2.75 |
| LBX | 5.59 | 2.07 | 1.00 | 27.41 | 5.24 | 5.00 | 25.02 | -2.39 | 6.25 | 6.45 | 29.17 | 1.76 |
| LBY | 0.58 | -0.52 | 0.48 | 27.25 | 5.22 | 4.65 | 21.63 | -5.62 | 6.23 | 4.21 | 13.28 | -13.97 |
| LBZ | 0.30 | -1.06 | 0.28 | 13.62 | 3.69 | 4.63 | 21.45 | 7.83 | 4.27 | 3.74 | 10.94 | -2.68 |
| LCZ | 1.32 | 0.29 | 0.54 | 2.41 | 1.55 | 4.70 | 22.11 | 19.71 | 1.03 | 4.90 | 17.38 | 14.98 |

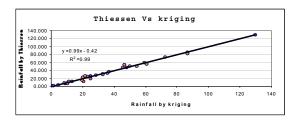
APPENDIX F Deviation assessment for decadal data

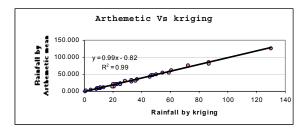
| Data | EstR | Act.rain | Frrlatu | AbaBoa | Err Ratio |
|--------------------|----------------|----------------|--------------|----------------|----------------|
| Date H3Y | 21.82 | 14.23 | 1.78 | 7.59 | 4.27 |
| H3Z | 49.70 | 31.52 | 5.76 | 18.18 | 3.16 |
| H4X | 29.09 | 29.70 | 4.77 | 0.61 | 0.13 |
| H4Y | 29.13 | 22.06 | 2.66 | 7.08 | 2.66 |
| H4Z | 55.02 | 96.06 | 3.66 | 41.04 | 11.21 |
| H5X | 21.84 | 38.86 | 5.66 | 17.02 | 3.01 |
| Н5Ү | 20.77 | 31.72 | 6.37 | 10.95 | 1.72 |
| H5Z | 13.54 | 41.28 | 7.80 | 27.73 | 3.56 |
| H6X | 31.28 | 26.42 | 4.90 | 4.86 | 0.99 |
| НбҮ | 31.57 | 52.38 | 5.09 | 20.81 | 4.09 |
| H6Z | 30.23 | 21.38 | 2.26 | 8.85 | 3.92 |
| HAZ | 18.14 | 36.66 | 3.58 | 18.52 | 5.17 |
| HBX | 40.19 | 70.99 | 6.48 | 30.81 | 4.76 |
| HBY | 36.19 | 60.90 | 5.85 | 24.71 | 4.22 |
| HBZ | 36.48 | 42.99 | 5.33 | 6.52 | 1.22 |
| HCX | 19.32 | 22.30 | 5.98 | 2.98 | 0.50 |
| HCZ | 7.94 | 3.54 | 0.97 | 4.41 | 4.57 |
| I3X | 58.30 | 59.99 | 7.17 | 1.70 | 0.24 |
| I5X | 28.55 | 47.61 | 5.75 | 19.07 | 3.31 |
| 15Y | 38.72 | 29.68 | 6.18 | 9.04 | 1.46 |
| I5Z | 19.01 | 15.78 | 3.73 | 3.23 | 0.87 |
| I6Y | 29.80 | 30.61 | 5.32 | 0.81 | 0.15 |
| I6Z | 17.62 | 31.33 | 5.00 | 13.71 | 2.74 |
| IBX | 13.13 | 28.99 | 8.68 | 15.85 | 1.83 |
| IBY | 30.36 28.12 | 50.49 | 6.66 | 20.14 | 3.02 11.80 |
| IBZ ICX | 8.52 | 11.24 11.51 | 1.43 5.92 | 16.87 3.00 | 0.51 |
| ICX | 21.05 | 22.64 | 2.27 | 1.60 | 0.70 |
| ICZ | 16.82 | 9.64 | 4.20 | 7.18 | 1.71 |
| J3X | 26.71 | 7.89 | 1.71 | 18.82 | 10.98 |
| J3Y | 24.13 | 20.45 | 2.73 | 3.67 | 1.34 |
| J3Z | 60.66 | 54.95 | 7.88 | 5.70 | 0.72 |
| J4Z | 12.33 | 8.07 | 2.20 | 4.26 | 1.94 |
| J5X | 25.98 | 13.73 | 2.77 | 12.25 | 4.43 |
| J5Y | 37.39 | 45.10 | 5.69 | 7.71 | 1.35 |
| J5Z | 14.47 | 22.42 | 3.93 | 7.96 | 2.03 |
| J6X | 27.50 | 73.63 | 6.25 | 46.13 | 7.38 |
| JGY | 39.45 | 36.01 | 6.11 | 3.44 | 0.56 |
| JAX | 30.18 | 12.30 | 1.99 | 17.88 | 9.01 |
| JAY | 18.07 | 21.81 | 5.17 | 3.74 | 0.72 |
| JAZ | 13.14 | 21.40 | 4.28 | 8.27 | 1.93 |
| JBX | 28.69 | 23.91 | 2.34 | 4.78 | 2.04 |
| JBY | 9.14 | 8.96 | 4.05 | 0.18 | 0.04 |
| JBZ | 31.55 | 43.08 | 4.76 | 11.53 | 2.42 |
| JCX | 17.94 | 15.39 | 5.92 | 2.55 | 0.43 |
| JCY | 15.23 | 7.53 | 2.27 | 7.70 | 3.39 |
| JCZ | 14.11 | 8.18 | 4.20 | 5.93 | 1.41 |
| КЗХ КЗҮ | 15.94 17.46 | 0.86 1.85 | 0.58 0.93 | 15.08 15.61 | 26.04 16.73 |
| K31 K3Z | 17.46 | 31.90 | 5.96 | 45.70 | 7.66 |
| K4X | 99.69 | 84.40 | 10.04 | 15.29 | 1.52 |
| K5X | 54.85 | 35.37 | 4.36 | 19.49 | 4.47 |
| K5Y | 21.90 | 14.97 | 3.28 | 6.93 | 2.11 |
| K5Z | 7.96 | 4.71 | 1.76 | 3.26 | 1.85 |
| K6X | 15.08 | 5.90 | 2.16 | 9.18 | 4.25 |
| KGY | 27.46 | 33.69 | 5.75 | 6.23 | 1.08 |
| K6Z | 33.81 | 20.02 | 1.98 | 13.79 | 6.96 |
| KAX | 25.06 | 30.74 | 4.31 | 5.68 | 1.32 |
| KAY | 21.17 | 59.41 | 7.66 | 38.24 | 4.99 |
| KBX | 36.14 | 82.88 | 8.55 | 46.74 | 5.47 |
| KBY | 82.89 | 72.29 | 6.24 | 10.60 | 1.70 |
| KBZ | 36.00 | 45.45 | 3.32 | 9.46 | 2.85 |
| KCX | 39.86 | 58.81 | 3.39 | 18.95 | 5.59 |

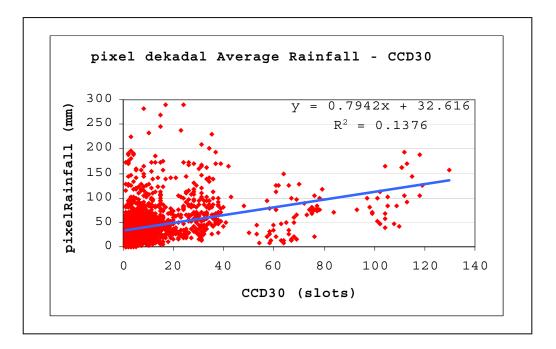
| KCY | 43.52 | 31.02 | 5.86 | 12.50 | 2.13 |
|-----|-------|--------|-------|-------|-------|
| KCZ | 24.56 | 30.66 | 3.37 | 6.10 | 1.81 |
| L3X | 33.34 | 20.00 | 3.60 | 13.34 | 3.70 |
| L3Y | 14.52 | 10.16 | 2.26 | 4.35 | 1.93 |
| L3Z | 26.03 | 15.13 | 3.28 | 10.89 | 3.32 |
| L4Z | 31.42 | 31.65 | 6.39 | 0.22 | 0.04 |
| L5X | 56.93 | 136.14 | 13.60 | 79.21 | 5.82 |
| L5Y | 58.97 | 60.43 | 7.60 | 1.46 | 0.19 |
| L5Z | 23.34 | 43.44 | 4.59 | 20.09 | 4.38 |
| L6Y | 17.29 | 30.85 | 6.40 | 13.55 | 2.12 |
| LAX | 28.02 | 17.21 | 5.45 | 10.81 | 1.98 |
| LAY | 33.78 | 31.10 | 4.73 | 2.67 | 0.57 |
| LBX | 29.13 | 27.41 | 4.36 | 1.72 | 0.39 |
| LBY | 13.27 | 27.25 | 3.88 | 13.97 | 3.60 |
| LBZ | 10.93 | 13.62 | 3.46 | 2.69 | 0.78 |
| LCZ | 17.38 | 2.41 | 1.07 | 14.97 | 13.98 |
| | | | | | |

| Dekade | CCD30 | Kriging | Thiessen | Arthemetic |
|--------|---------|---------|----------|------------|
| J3X | 4.443 | 8.777 | 7.798 | 9.753 |
| J3Y | 3.369 | 20.299 | 21.031 | 20.024 |
| J3Z | 34.481 | 54.578 | 51.210 | 54.959 |
| КЗХ | 1.019 | 0.777 | 1.582 | 1.018 |
| КЗҮ | 1.339 | 1.320 | 1.264 | 1.812 |
| K3Z | 60.840 | 32.994 | 31.199 | 29.100 |
| L3X | 7.953 | 25.193 | 18.925 | 20.659 |
| L3Y | 0.764 | 10.976 | 9.737 | 9.947 |
| L3Z | 4.142 | 20.705 | 12.600 | 14.241 |
| J4Z | 0.452 | 8.361 | 9.601 | 7.824 |
| K4X | 106.604 | 86.868 | 86.305 | 86.324 |
| L4Z | 6.824 | 35.803 | 33.002 | 30.241 |
| K5X | 27.198 | 36.797 | 35.999 | 35.741 |
| K5Y | 2.575 | 19.386 | 15.129 | 14.265 |
| K5Z | 0.095 | 4.496 | 4.012 | 5.535 |
| L5X | 29.698 | 129.795 | 128.966 | 126.465 |
| L5Y | 32.274 | 59.127 | 60.147 | 54.635 |
| L5Z | 3.076 | 45.462 | 47.844 | 42.041 |
| H6X | 6.745 | 25.041 | 26.749 | 23.594 |
| H6Y | 6.908 | 46.619 | 55.041 | 48.112 |
| H6Z | 6.170 | 22.808 | 24.266 | 21.194 |
| JAX | 6.142 | 11.123 | 13.115 | 10.941 |
| JAY | 1.482 | 20.131 | 22.196 | 20.741 |
| JAZ | 0.557 | 21.757 | 27.084 | 22.529 |
| KAX | 3.736 | 32.642 | 29.925 | 33.806 |
| KAY | 2.340 | 60.458 | 55.621 | 61.641 |
| IBX | 0.556 | 28.515 | 27.913 | 31.171 |
| IBY | 6.236 | 50.024 | 51.141 | 49.676 |
| IBZ | 5.094 | 13.394 | 11.419 | 11.100 |
| JBX | 5.377 | 24.904 | 24.814 | 21.359 |
| JBY | 0.160 | 10.263 | 6.734 | 10.065 |
| KBX | 9.774 | 86.432 | 81.420 | 81.859 |
| KBY | 70.642 | 72.403 | 73.681 | 77.235 |
| KBZ | 9.679 | 47.822 | 47.803 | 47.882 |
| | | | | |

APPENDIX G Comparison of kriged rainfall estimate with arthemetic mean and Thiessen polygon method

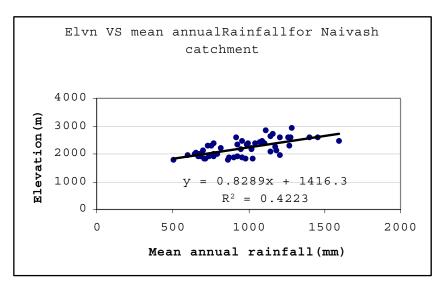






APPENDIX H Pixel calibration for decadal data

pixel calibration for the dekadal data.



APPENDIX I Annual rainfall and altitude relationship

Graph, which shows the relation between elevation and mean annual rainfall for Naivasha catchment (source: thesis report by Kwacha).

APENDIX J Listing of the program

Windowing:

AWK.

```
BEGIN{
REGION = "Na"
MET COORDS = "-565 1378 -309 1122"
LL COORDS = "32 5 42 -5"
af file = substr(\$1,1,8)
metfile = REGION substr(af_file,3,6)
llfile = substr(metfile,1,4) "1" substr(metfile,6,3)
print "c:\\idrisi\\window x", af_file, metfile, "2", MET_COORDS
print "c:\\bin\\met2ll", metfile, "templl 0.05"
print "c:\\idrisi\\window x templl", llfile, "2", LL_COORDS
print "del templl.*"
print ""
bat
dir %1.img /on/b > list.txt
c:\bin\gawk -fmyprog.awk list.txt > job.bat
call job.bat
del job.bat
del list.txt
Unzip file
AWK
BEGIN{
       REGION = "Na"
       MET_COORDS = "-565 1378 -309 1122"
       LL COORDS = "32 5 42 -5"
       ZIPDRIVE = "c: \\"
}
{
       this program
#
       af file = substr($1,1,3) "3" substr($1,5,4)
       metfile = REGION substr(af file,3,6)
       llfile = substr(metfile,1,4) "1" substr(metfile,6,3)
       print "c:\\bin\\pkunzip", ZIPDRIVE $1, af_file".*"
       print "c:\\idrisi\\window x", af_file, metfile, "2", MET_COORDS
       print "c:\\bin\\met2ll", metfile, "templl 0.05"
       print "c:\\idrisi\\window x templl", llfile, "2", LL_COORDS
       print "del", af_file".*"
       print "del templl.*"
       print ""
}
```

bat

```
rem dir %1.zip /on/b > list.txt
```

c:\bin\gawk -fafzip2ll.awk list.txt > jobwin.bat call jobwin.bat del jobwin.bat del list.txt

Spliting the data

Splitds.awk

```
# AWK script to split a table file in "row-date/column-station" format into
# as many individual time step files as exist. The output name is derived
\# from the rwo header which is a date in DD/MM/YY
BEGIN{
       EXT = ".TXT"
       NHEAD = 1
                        # Number of row headers, usually 1
                        # First data column is (NHEAD+1)th column.
}
{
       if (NR==1) {
               nstatn = $1
                             # first row of file has this quantity
               region = substr(FILENAME,1,2)
               param = substr(FILENAME,3,2)
      geog
             = substr(FILENAME, 5, 1)
       }
       else if (NR == 2){
               for (i = 1; i <= nstatn+NHEAD; i++) id[i] = $i</pre>
       }
       else if (NR == 3){
               for (i = 1; i <= nstatn+NHEAD; i++) lon[i] = $i</pre>
       }
       else if (NR == 4) {
               for (i = 1; i <= nstatn+NHEAD; i++) lat[i] = $i</pre>
       }
       else{
               DATE = ZAMIS date($1)
            outfile = region param geog DATE EXT
               print "1", nstatn > outfile
               for (i = 1; i <= nstatn+NHEAD; i++) {</pre>
                       print id[i], " ", lon[i], " ", lat[i], " ", $i >> outfile
               }
               print "generated file", outfile
       }
```

}

```
function ZAMIS date(date) {
        # date is in the date format DD/MM/YY
        # alphabetic date code
        date_code = "123456789ABCDEFGHIJKLMNOPQRSTUVWXYZ"
        # extraction of year - subtract 77 from year so 87=10, 88=11, ...
        # then retrieve the year code from the date code string
       yy = substr(date, 7, 2) - 77
       year = substr(date_code, yy, 1)
        # extraction of month - subtract 0 for MM to become a number (1-12)
        # then retrieve the month code from the date code string
             = substr(date, 4, 2) - 0
       mm
       month = substr(date code,mm,1)
        # extraction of day - subtract 0 for DD to become a number (1-31)
        # then retrieve the day code from the date code string
             = substr(date, 1, 2) - 0
        dd
        day = substr(date_code,dd,1)
       zamis date = year month day
       return zamis date
}
```

Splitds.bat

@echo off
rem Runs the table splitting awk script. Output files generated within the script
\bin\gawk -fsplitds.awk %1

Variogram Derivation:

glsvario.bat

rem NOTE : Amend the data table name and the vario .dat files before using !!!!!
rem runs VARIOT to derive the experimental variogram
\bin\variot -s -t -z Nargp0%31.txt %2 > vg_%3%2.txt

```
rem converts to format used by EP GLS program AVAMCP
\bin\gawk -fvg2ls.awk vg_%3%2.txt > vtemp
rem prepares input file to AVAMCP and runs it
echo vtemp > infile
echo %1 >> infile
echo 1 >> infile
echo 1 >> infile
echo 2 >> infile
echo coeff1 >> infile
```

```
echo coeff2 >> infile
\bin\avamcp < infile
del infile
rem converts the output coefficient file from AVAMCP into
rem TAMSAT standard variogram coefficients format
\bin\gawk -fgls2dat.awk coeff2 > Navcl0%31.dat
rem clean up
del vtemp
del coeff1
del coeff2
```

Kriging (KRIGOPOL):

AWK

```
BEGIN {
    area = "Namask"
    output = "krig.txt"
}
{
    Rfile = $1
    region = substr(Rfile,1,2)
    month = substr(Rfile,7,1)
    if (NR==1) to = "> "
    else to = ">>"
     varfile = region "vcl0" month "1.dat"
    print "c:\\bin\\krigopol",Rfile,varfile,area,to,output
}
```

}

bat

```
@echo off
dir %1.txt /on/b > kr.txt
c:\bin\gawk -fkrig1.awk kr.txt > assign.bat
call assign.bat
rem del assign.bat
rem del kr.txt
```

Merging of satellite and gauge data (GET_STN):

AWK

```
BEGIN{ PATH = "c:\\bin\\"
    height = "8"
    output = "stn.txt"
}
{
    gauge = $1
```

```
ccd = substr(gauge,1,2) "c3M" substr(gauge,6,3)
if(NR==1) to = ">"
else to = ">>"
print PATH"get_stn -m -p", height, gauge, ccd, to, output
}
```

bat

```
@echo off
dir %1.txt /on/b > mes.txt
c:\bin\gawk -fgetstn.awk mes.txt > jobstn.bat
call jobstn.bat
del jobstn.bat
del mes.txt
Where :
-m convert the rain gauge stn (lon, lat) to meteosat co-ordinate
-p parallax correction
8 is height of cloud in parallax correction
```

Derivation average CCD over the catchment (MEANPOL)

AWK

```
BEGIN{
```

```
PATH = "c:\\bin\\"
       mask = "Namask2"
       thresh["a"] = 0
       thresh["b"] = 0
       thresh["c"] = 0
       thresh["3"] = 1
       thresh["4"] = 0
       thresh["5"] = 0
       thresh["6"] = 0
       if (output == "") output = "outmpol"
       output = output ".txt"
}
{
       image = substr($1,1,8)
       month = tolower(substr(image,7,1))
         t = thresh[month]
       if (NR==1) to = "> "
       else
                  to = ">>"
       print PATH"meanpol -x", t, mask, image, to, output
}
```

bat

@echo off

rem USAGE : MEANPOL IMGSPEC OUTPUT
rem where OUTPUT is the name of the output text file
dir %1.img /on/b > datalist
\bin\gawk -fmeanpolk.awk -voutput=%2 datalist > jobmean.bat
call jobmean.bat
del jobmean.bat
del datalist

APPENDIX K Naming convention for files (data+image)

1. The file should have eight characters and three-file extension (idrisi extension)

2. The characters should be in the form of RRTTGYMT.

Where: RR: Region code

TT: Type codes (data type)

G: Geography code

YMT: Date code (Y=year, M=month and T= time step)

For the year the METEOSAT data archive starts at 1987, it is agreed to have:

| Year | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 2000 |
|------|----|----|----|----|----|----|----|----|----|----|----|----|----|------|
| Code | А | В | С | D | Е | F | G | Н | Ι | J | К | L | Μ | Ν |

Month

| Month | Jan | Feb | March | Apr | May | June | July | Aug | Sept | Oct | Nov | Dec |
|-------|-----|-----|-------|-----|-----|------|------|-----|------|-----|-----|-----|
| Code | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | А | В | С |

Decade

| Decade | First | Second | Third |
|--------|--------|--------|--------|
| | decade | decade | decade |
| Code | Х | Y | Ζ |

Time step (day)

| Day | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | | 25 | | 27 | | 29 | 30 | 31 |
|------|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|---|----|---|----|---|----|----|----|
| Code | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | А | | С | D | Е | F | G | Н | Ι | J | Κ | L | Μ | Ν | 0 | Р | Q | R | S | Т | U | V |

APPENDIX L File locations

| Data type | Data location | Description | | | | | | | | |
|--------------------|----------------------------|--|--|--|--|--|--|--|--|--|
| | | CCD images with threshold -30°C (Latitude-Longitude | | | | | | | | |
| | C:\Kenya\Data\kec3l | coordinate | | | | | | | | |
| 0.00 | C:\Kenya\Data\kec3t | CCD images with threshold -30°C (METEOSAT coordinate) | | | | | | | | |
| CCD images | C:\Kenya\Data\kec4l | CCD images with threshold -40°C (Latitude-Longitude coordinate | | | | | | | | |
| | C:\Kenya\Data\kec4t | CCD images with threshold -40°C (METEOSAT coordinate) | | | | | | | | |
| Rain gauge data | C:\Kenya\Data\Kergp | Rain gauge station location and row data | | | | | | | | |
| | C:\Kenya\Result\Daily | Data arrangement, variogram derivation, calibaeration | | | | | | | | |
| | | plot,regression and deviation assessement | | | | | | | | |
| | C:\Kenya\Result\dekadal | Data arrangement, variogram derivation, calibaeration | | | | | | | | |
| XLS data | | plot, regression pixel caliberation, deviation | | | | | | | | |
| | | assessement and comparison of CCD to Thiessen | | | | | | | | |
| | | polygon and arthemetic mean. | | | | | | | | |
| | C:\Kenya\Result\Comparison | Discharge row data and Discharge Response to event | | | | | | | | |
| | | CCD and kriged rainfal | | | | | | | | |
| Program file | C:\bin | All the program that are used in this thesis | | | | | | | | |
| Word | C:\Kenya\Document | Thesis reporat | | | | | | | | |
| document | | | | | | | | | | |
| ILWIS | C:\Kenya\Process | Selected CCD image imported from IDRISI to evaluate | | | | | | | | |
| image | | discharge response | | | | | | | | |
| IDRISI | C:\Kenya\Process | Mask image of Naivasha and Malewa which are used | | | | | | | | |
| Mask | | for kriging and determination of average CCD over the | | | | | | | | |
| Image | | catchment | | | | | | | | |

The following table refers to the location of file used in the report.

Estimation of rainfall using METEOSAT TIR data for the Naivasha catchment (Kenya)